City of Fairfax Chesapeake Bay Total Maximum Daily Load (TMDL) Action Plan

Phase III



Prepared for:
City of Fairfax

Department of Public Works
10455 Armstrong Street
Fairfax, VA 22030

August 27, 2024

Updated by:



4229 Lafayette Center Drive, Suite 1850 Chantilly, Virginia 20151 703-870-7000



Table of Contents

Repo	oort Certification	ii
Acro	onyms	iv
Defi	initions	
1.0	Executive Summary	1
2.0	Chesapeake Bay TMDL and Virginia MS4s	
3.0	City of Fairfax MS4	2
	3.1 Analysis of Legal Authorities	3
	3.2 City's Intended Use of Nutrient Credits Via Private Nutrient Exchange to Months Load Reductions	
4.0	City MS4 POC Loads	5
5.0	City MS4 POC Reductions	8
6.0	City Implementation of Phase I and Phase II Chesapeake Bay TMDL Action Plans	g
	6.1 Phase II Chesapeake Bay TMDL Action Plan Compliance Assessment	13
7.0	City Phase III Chesapeake Bay TMDL Action Plan	14
	7.1 Phase III Chesapeake Bay TMDL Action Plan Pollutant Additional Strategies	17
	7.2 Phase III Chesapeake Bay TMDL Action Plan Compliance Assessment	19
8.0	Progress Tracking and Documentation	21
9.0	Opportunity for Public Comment Summary	24



Appendice(s)

Appendix A – City/NCPCP Water Quality Agreement for Chesapeake Bay TMDL Implementation

Appendix B. Updated Land Cover Analysis

Appendix C. Daniels Run Stream Restoration Calculations

Appendix D. City Hall Pond Retrofit Calculations

Appendix E. Lion Run Outfall Restoration POC Reduction Calculations

Appendix F. Pickett Road Outfall Restoration POC Reduction Calculations

Appendix G. Shiloh Street Outfall Restoration POC Reduction Calculations

Appendix H. Westmore Elementary School/Dog Park Bioretention Calculations

Appendix I. University Drive Traffic Calming Calculations

Appendix J. Calculating VSMP Pollutant Reductions Creditable to Chesapeake Bay Existing Source Load Reductions

Appendix K. VSMP Implementation - Redevelopment Credits on Prior Developed Land

Appendix L. NPS Nutrient Credit Purchase: Whispering Hills

Appendix M. DEQ MS4 Nutrient Credit Acquisition Form

Appendix N. Stafford Drive Stream and Outfall Restoration Calculations

Appendix O. Ashley Pond Conservancy Wet Pond Enhancement Calculations

Appendix P. Van Dyck Park Outfall Restoration Calculations

Appendix Q. Traveler Street Outfall Restoration Calculations

Appendix R. Providence Park Providence Park Outfall Restoration Calculations

Appendix S. Mathy Park Retrofit Calculations

Appendix T. Lions Run BMP Retrofit Concept Calculations

Appendix U. Storm Drain Cleaning Assessment and Procedures

Appendix V. Chesapeake Bay POC Reduction and Crediting Associated with Leaf Litter Collection and Disposal Discussion

Appendix W. Summary of Public Comments Received During the Public Comment Period and City Responses



Report Certification

As required by the MS4 General Permit, Part III. K. 4.

"I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations."

Name: Satoshi Eto
Date: 2024.09.09
14:34:21 -04'00'

Title: Public Works Program Manager
Date: 09-09-2024



Acronyms

Blvd. Boulevard

BMP Best Management Practice
CBP EPA's Chesapeake Bay Program
CBPA Chesapeake Bay Preservation Act

CCTV Closed-Circuit Television
CIP Capital Improvement Plan
City City of Fairfax, Virginia
CWA Federal Clean Water Act

DEQ Virginia Department of Environmental Quality

EPA Environmental Protection Agency

FY Fiscal Year

GIS Geographic Information System

GM Guidance Memo
IC Impervious Cover
I&I Inflow and Infiltration

L2 Run Chesapeake Bay Model 5.2 Level 2 Scoping Run

Lat. Latitude
Lbs. Pounds
Long. Longitude

MGD Million Gallons per Day

Mi. Miles

MS4 Municipal Separate Storm Sewer System

MS4 General Permit VPDES General Permit for Discharges of Stormwater from Small MS4s

NCPCP Noman Cole Jr. Pollution Control Plant

NMP Nutrient Management Plan

No. Number

NPS Nonpoint Source

POC Pollutants of Concern (Nitrogen and Phosphorus)

Rd. Road

SDC Storm Drain Cleaning

SLAF Virginia Stormwater Local Assistance Fund

St. Street

SWM Stormwater Management Facility

TMDL Total Maximum Daily Load

VA WIP Virginia Chesapeake Bay Watershed Implementation Plan

VESCP Virginia Erosion and Sediment Control Program

VESMP Virginia Erosion and Stormwater Management Program

VNCEA Virginia Nutrient Credit Exchange Association
VPDES Virginia Pollutant Discharge Elimination System

VRRM Virginia Runoff Reduction Method

VSMP Virginia Stormwater Management Program

WLA Wasteload Allocation

Yr. Year



Definitions

Existing Sources	Pervious and impervious urban land uses served by the MS4 as of June 30,
	2009.
Impaired Water Body	A water body that does not meet water quality standards because it will not support one or more of its designated uses.
New Sources	Pervious and impervious urban land uses served by the MS4 developed or redeveloped on or after July 1, 2009.
Phase I Chesapeake Bay TMDL Action Plan	The first phase of a three-phase approach provided to small MS4 operators to implement the total reductions required of MS4s as established by the Chesapeake Bay Model 5.2 Level 2 Scoping Run. Small MS4 operators were required to reduce the Existing Source POC (and applicable New Source) loads by 5% of the total required reductions as calculated in the 2013 MS4 General Permit.
Phase II Chesapeake Bay TMDL Action Plan	The second phase of a three-phase approach provided to small MS4 operators to implement the total reductions required of MS4s as established by the Chesapeake Bay Model 5.2 Level 2 Scoping Run. Small MS4 operators were required to reduce the Existing Source (and applicable New Source) POC loads by 40% of the total required reductions as calculated in the 2018 MS4 General Permit.
Phase III Chesapeake Bay TMDL Action Plan	The third phase of a three-phase approach provided to small MS4 operators to implement the total reductions required of MS4s as established by the Chesapeake Bay Model 5.2 Level 2 Scoping Run. Small MS4 operators were required to reduce the Existing Source (and applicable New Source) POC loads by 100% of the total required reductions as calculated in the 2023 MS4 General Permit.
Transitional Sources	Regulated land disturbing activities that are temporary in nature and discharge through the MS4.
Wasteload Allocation	The portion of the TMDL allocated to VPDES permitted discharges.



1.0 Executive Summary

The City of Fairfax (City) operates a Municipal Separate Storm Sewer System (MS4) regulated under the Virginia Pollutant Discharge Elimination System (VPDES) and discharges into the tributaries of the Chesapeake Bay. The Chesapeake Bay is impaired due to excess nutrients (phosphorus and nitrogen) and sediment. As a regulated VPDES discharger, the City must implement pollutants of concern (POC) minimization strategies to address loads from Transitional Sources and New Sources. The City also has three (3) VPDES permit cycles to meet the required POC load reductions from Existing Sources defined as 100% of the cumulative reduction required by the Chesapeake Bay Watershed Model Progress Run Level 2 (L2) Run. This Action Plan is the third and final Chesapeake Bay TMDL Action Plan. It documents the City's intended means and methods for achieving 100% of the required Existing Source cumulative POC load reductions.

The Phase III Chesapeake Bay TMDL Action Plan documents the City of Fairfax's commitment to complete a minimum of 22 pollutant reduction strategies by October 31, 2028, which will result in the annual reduction of 1,276 lbs. of nitrogen and 651 lbs. of phosphorus. The City has entered into an agreement with Fairfax County to secure sufficient point source credits from the Noman Cole Jr. Pollution Control Plant (NCPCP) to guarantee pollutant loads will have been reduced to meet the required L2 Run.

2.0 Chesapeake Bay TMDL and Virginia MS4s

The Chesapeake Bay watershed encompasses over 64,000 mi.² of land in Delaware, Maryland, New York, Pennsylvania, Virginia, West Virginia, and the District of Columbia. Portions of the Bay and its tidal tributaries were identified as impaired for not meeting federal Clean Water Act (CWA) water quality standards in 1998. The United States Environmental Protection Agency published a TMDL on December 29, 2010, which identified nutrients (nitrogen and phosphorus) and sediment as the causes of the impairment. The TMDL also established the maximum quantity of POCs that can be discharged into the Bay and its tributaries and still allow it to meet water quality standards. The Commonwealth of Virginia developed the Virginia Chesapeake Bay Watershed Implementation Plan (VA WIP) in response to the federal action. The VA WIP outlined Virginia's strategies for implementing POC load reductions in Virginia waterways to meet the conditions of the TMDL from both point source and nonpoint source dischargers. The VA WIP outlined the Commonwealth's intention to regulate POC reductions from MS4s in the Chesapeake Bay watershed under the VPDES permitting program. Under VPDES permit conditions, the Commonwealth requires MS4 operators to implement both a Virginia Erosion and Sediment Control Program (VESCP) and a Virginia Stormwater Management Program (VSMP) consistent with State statutes and regulations. MS4 operators were also required to implement Nutrient Management Plans (NMPs) on municipal properties if fertilizers are applied to a contiguous area of one (1) acre or greater as a means to control POC discharges from New Sources (increases in impervious cover (IC) after July 1, 2009) and Transitional Sources (sources generating POC during land use transitions). The VA WIP also enumerated the reductions in POC loads from Existing Sources (land use identified as impervious and pervious urban served by the MS4 prior to July 1, 2009) that MS4 operators would need to implement to meet the Chesapeake Bay Watershed Model Progress L2 Run (Table 1).



Table 1. Chesapeake Bay Watershed Model Progress L2 Run Existing Source Reduction Requirements

Land Use	POC Reductions				
Land Ose	Nitrogen	Phosphorus	Sediment		
Impervious Regulated Lands	9%	16%	20%		
Pervious Regulated Lands	6%	7.25%	8.75%		

Additionally, the L2 Run assumed that POC discharges from New Sources disturbing one acre or greater of land provided stormwater quality treatment based on the pre-2014 VSMP Baywide design criteria equivalent of 16% impervious cover (0.45 lbs./ac./year). The VA WIP required MS4 operators to offset any increases in POC loads from New Sources constructed after July 1, 2009, that were implemented based on a design other than the 16% Baywide design criteria.

The VA WIP describes Virginia's compliance strategy in which MS4 operators have three five-year VPDES permit cycles to implement the required Existing Source POC reductions and offset the increased POC loads from New Sources. The POC reduction requirements would be prorated among the three VPDES permit cycles to require 5% of the L2 Run reductions to be met by the end of the first permit cycle, 40% of the cumulative L2 Run reductions to be met by the end of the second permit cycle, and 100% of the cumulative L2 Run reductions to be met by the end of the third. For small MS4 operators covered under the VPDES General Permit for Stormwater Discharges from Small MS4s (MS4 General Permit), the three (3) permit cycles correspond with the following dates:

- Permit Cycle 1 July 1, 2013 October 31, 2018
- Permit Cycle 2 November 1, 2018 October 31, 2023
- Permit Cycle 3 November 1, 2023 October 31, 2028

On November 22, 2022, the Virginia Department of Environmental Quality (DEQ) notified the Environmental Protection Agency (EPA) of its decision to remove the specific sediment reduction requirements from MS4 General Permits to be consistent with the Chesapeake Bay Program Principals' Staff Committee's August 12, 2019, final decision. As a result, small MS4 operators will only need to meet 100% of the cumulative L2 Run reductions for nutrients and not sediment as required in the first two (2) MS4 General Permit cycles.

3.0 City of Fairfax MS4

The City of Fairfax is a 154-year-old, independent city of approximately 24,000 residents in the heart of Northern Virginia. The City encompasses 6.24 mi.2 of land, of which approximately 45% is impervious. The City operates a small MS4 approximately 14 miles west of Washington, D.C. Discharges from its MS4 are authorized to enter the Chesapeake Bay via the Potomac River under the MS4 General Permit. The City has previously developed and implemented both Phase I and Phase II Chesapeake Bay TMDL Action Plans. The City manages POC sources from Transitional Sources and New Sources through the implementation of the following programs:

- A DEQ-authorized VESCP ¹
- A DEQ-authorized VSMP
- NMPs on 21.24 acres at the six (6) City properties listed in Table 2.

¹ As of July 1, 2024, the City will operate a Virginia Erosion and Stormwater Management Program (VESMP) consistent with the consolidated Virginia Erosion and Sediment Control and Stormwater Management Regulations.



Table 2. City of Fairfax Nutrient Management Plans for Application of Nutrients on One (1) Contiguous Acre or Greater

Facility Name	NMP Acreage	NMP Effective Date
Kutner Park	1.68	1/1/2021
Lanier Middle School	5.31	1/1/2021
Providence Elementary School	4.70	1/1/2021
Daniels Run Elementary School	2.96	1/1/2021
Green Acres Center	3.68	1/1/2021
Pat Rodio Park	2.91	1/1/2021

Virginia Code § 62.1-44.15:68 defines the City as located in Tidewater, Virginia, under the Chesapeake Bay Preservation Act (CBPA). As such, the City has implemented stormwater requirements on land disturbance projects 2,500 ft² and larger.

3.1 Analysis of Legal Authorities

- 12. Chesapeake Bay TMDL action plan requirements.
 - b. For permittees previously covered under the General VPDES Permit for the Discharge of Stormwater from MS4 effective November 1, 2018, no later than 12 months after the permit effective date, the permittee shall submit a third phase Chesapeake Bay TMDL action plan for the reductions required in Part II A 3, A 4, and A 5 that includes the following information:
 - 1) Any new or modified legal authorities, such as ordinances, permits, policy, specific contract language, orders, and interjurisdictional agreements, implemented or needing to be implemented to meet the requirements of Part II A3, A4, & A5.

The MS4 General Permit requires that the City identify any new or modified legal authorities necessary to meet the General Permit Special Condition for the Chesapeake Bay TMDL. The City believes it has sufficient legal authority to implement the Chesapeake Bay Special Condition with the following caveat.

The City believes it has the legal authority to include necessary language in any future contracts, orders, or inter-jurisdictional agreements that may be required but have not been implemented during the development of this plan. As a locality in a Dillon Rule state, the City reserves the right to identify where the Commonwealth of Virginia has not provided adequate legal authority to implement any future legal agreements and documents.

3.2 City's Intended Use of Nutrient Credits Via Private Nutrient Exchange to Meet L2 Pollutant Load Reductions

Fairfax County operates the NCPCP (VPDES # VA0025364). The 2003 General Services Agreement between the City of Fairfax and Fairfax County reserves 4.2 million gallons/day (MGD) (6.27%) of the 67.00 MGD treatment capacity for the City's use. The City and the County have entered into a Water Quality Credit Agreement, dated October 6, 2020 (Appendix A). This agreement designates nutrient credits towards the City's MS4 Chesapeake Bay TMDL Action Plan as follows:

- Sufficient nutrient credits for the City to achieve a nutrient load reduction equivalent to 40% of the L2 Run nutrient load reductions through October 31, 2028.
- Sufficient nutrient credits for the City to achieve a nutrient load reduction equivalent to 100% of the L2 Run nutrient load reductions beginning October 31, 2028. The current agreement will expire after Compliance Year 2030 and must be renewed if the City wishes to continue utilizing point source credit trades to maintain compliance.



The NCPCP was designed and constructed to treat 67.00 million MGD of sanitary sewage to an average daily nitrogen concentration of 3.0 milligrams/Liter. The Chesapeake Bay TMDL allocated the NCPCP a nitrogen wasteload of 612,158 lbs./yr. based on this design. Based on the Virginia Nutrient Credit Exchange Association's (VNCEA) Compliance Plan 2023 Update, sufficient credits will be allocated to the City to ensure it maintains the minimum required reductions equivalent to 40% of the L2 Run during the current MS4 General Permit cycle (Table 3) and the total required L2 Run reductions by October 31, 2028 (Table 4). While the City's agreement with the County secures sufficient credits based on the City not achieving pollutant reductions by any other means, as demonstrated in this action plan, the City will not solely rely on nutrient credits from the NCPCP.

Table 3. City of Fairfax MS4 40% L2 Run Pollutant Load Reduction Compliance Security Via Private Exchange with NCPCP

Nutrient	NCPCP WLA	NCPCP Expected Credits (2023)	City Allocated Portion (6.27%)	40% City's MS4 L2 Run Required Reductions	Phase II Compliance Secured
Nitrogen	612,158	206,329	12,937	1,465	✓
Phosphorus	36,729	12,570	788	180	✓

Table 4. City of Fairfax MS4 100% L2 Run Pollutant Load Reduction Compliance Security Via Private Exchange with NCPCP

Nutrient	NCPCP WLA	NCPCP Expected Credits (2028)	City Allocated Portion (6.27%)	100% City's MS4 L2 Run Required Reductions	Phase III Compliance Secured
Nitrogen	612,158	143,912	9,023	3,662	✓
Phosphorus	36,729	8,771	550	449	✓

The City recognizes the potential impact on available wastewater treatment capacity caused by using wastewater credits to meet stormwater requirements and has continued to strive to maximize the pollutant reductions through traditional stormwater management practices during the three phases of its Chesapeake Bay TMDL Action Plan. To maximize the availability of future credits, the City intends to continue its long-term sanitary sewer flow monitoring program to identify, prioritize, and minimize inflow and infiltration (I&I). Between 2010 and August 2022, the City's I&I reduction efforts have resulted in the closed-circuit television (CCTV) evaluation of approximately 25% (127,600 feet) and the lining of approximately 17% (87,600 feet) of the City's sanitary sewer; thus, significantly reducing the amount of non-sanitary sewage being sent to NCPCP. The City will also continue to enforce City ordinances that require maintenance of privately-owned sanitary sewer laterals while providing aid in offsetting the costs through programs such as the City's current sanitary sewer lateral repair and replacement program. As I&I programs continue to eliminate non-sewage flows from entering the sanitary sewer, reduced sanitary sewage treatment needs will offset the City's use of nitrogen credits to meet MS4 POC load reduction requirements.

Additionally, the City's efforts to eliminate I&I continue to reduce sewage exfiltration from the sanitary sewer into the City's MS4 and nearby receiving waters. DEQ's current Guidance Memo GM20-2003 does not recognize a method for calculating POC reductions for MS4s associated with this activity; however, the City understands that the Chesapeake Bay Urban Working Group Expert Panel published an October

² https://www.deg.virginia.gov/home/showpublisheddocument/6987/638417913809370000



22, 2014 panel report - "Recommendations of the Expert Panel to Define Removal Rates for the Elimination of Discovered Nutrient Discharges from Grey Infrastructure" — that recognizes nutrient loads (nitrogen and phosphorus) can enter the MS4 as a result of exfiltration of sewage from cracks and leaks in the sanitary sewer. The City hopes that DEQ publishes an economically and technically viable method for quantifying these reductions so that the City can account for the nitrogen reductions associated with its extensive activities.

4.0 City MS4 POC Loads

- 12. Chesapeake Bay TMDL action plan requirements....
 - b. For permittees previously covered under the General VPDES Permit for the Discharge of Stormwater from MS4 effective November 1, 2018, no later than 12 months after the permit effective date, the permittee shall submit a third phase Chesapeake Bay TMDL action plan for the reductions required in Part II A 3, A 4, and A 5 that includes the following information:
 - 2) The load calculations for each river basin calculated in accordance with Part II A 3, A 4, and A 5.

In estimating its Existing Source acreage for Phase I and Phase II of its Chesapeake Bay Action Plan, the City used a conservative jurisdictional approach in which aerial imagery was used to manually digitize four (4) land coverage types to estimate land use changes between July 1, 2009 and June 30, 2014. In 2021, the City completed the Updated Land Cover Analysis to refine its Existing Source acreages by analyzing Geographic Information System (GIS) datasets, aerial imagery, and field verification (Appendix B). As a result, the updated acreages associated with Existing Sources as of June 30, 2009, are:

- Impervious Urban Acres 1,570 acres
- Pervious Urban Acres 2,046 acres

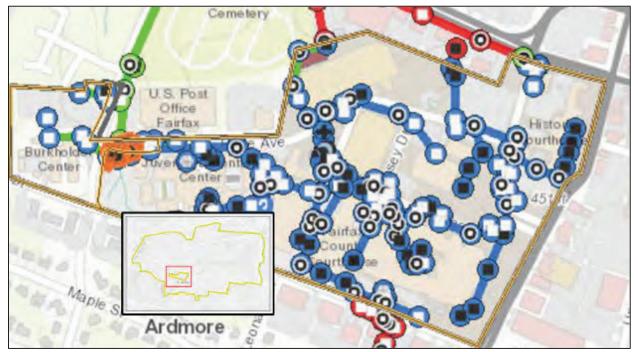


Figure 1. Fairfax County Stormwater Infrastructure Physically Interconnected to the City's MS4 (Fairfax County Jade)



The City further defined the MS4 Service Area by eliminating a 48.92-acre unincorporated segment of Fairfax County surrounded by the City. As shown in Figure 1, the County stormwater infrastructure (blue) associated with this property is physically interconnected with the City's MS4.

The City also identified and eliminated 90.41 acres of properties located in the City whose stormwater discharges are regulated under either individual VPDES permits or the VPDES General Permit for Discharges from Industrial Activities. The final adjusted MS4 Service Area for the City and for which the Chesapeake Bay TMDL Action Plan Existing Source Loads are based, is as follows:

- 1,508 Impervious Acres
- 1,968 Pervious Acres

Table 5 provides the calculations for adjusting the MS4 Service Area.

Table 5. MS4 Service Area Adjustment for Unincorporated County Property and VPDES Permitted Facilities

Acreage Adjustment	Impervious, acres	Pervious, acres
Land Use (City of Fairfax 2021 GIS Analysis)	1,570	2,046
Unincorporated County Property (48.92 acres)	30.35	18.57
VPDES Industrial – Individual and VA05 General Permit	31.36	59.05
Motiva (58 3 02 026) - VA002283	4.92	11.18
Joint Basin Corporation (58 1 02 029; 58 1 02 029a; 58 1 02 030; 58 3 02 025) - VA001872	17	42.27
Fairfax County Jermantown Maintenance Facility (47 3 02 005) - VAR051770	9.44	5.6
Final REVISED Phase III TMDL Action Plan MS4 Service Area Acres	1,508	1,968

The Existing Source POC loads attributed to the City's Adjusted MS4 Service Area are as follows:

- Nitrogen 45,243 lbs./yr.
- Phosphorus 3,250 lbs./yr.

Table 6 provides the calculations for the existing source loads.

Table 6. City of Fairfax Existing Source POC Loads

POC	Existing Source (Land Use)	Loading Rate, lbs./ac./yr.	Acres Served as of July 1, 2009	Existing Source Load, Ibs./yr.	Total Existing Source Load, Ibs./yr.3	
Niterra	Regulated Impervious	16.86	1,508	25,425	45,243	
Nitrogen	Regulated Pervious	10.07	1,968	19,818		
Dhasabasus	Regulated Impervious	1.62	1,508	2,443	2.250	
Phosphorus	Regulated Pervious	0.41	1,968	807	3,250	

The City also updated its previously calculated New Source loads. As a CBPA locality in place prior to the TMDL, the City had implemented a stormwater water quality design criteria based on local watershed impervious cover (45% impervious cover equivalent to 1.27 lbs./ac./yr. phosphorus) rather than the Baywide impervious cover assumption of 16%. As a result, the City reviewed previously approved plans

³ Loading and reduction values greater than or equal to 10 lbs. must be calculated and reported to the nearest pound without regard to mathematical rules of precision. Those less than 10 lbs. must be calculated and reported to two significant digits.



to identify and mitigate the POC load difference between the City's water quality design criteria and the watershed water quality design criteria for projects that disturb one acre or greater and:

- Initiated construction between July 1, 2009, and June 30, 2019, in accordance with approved plans using the City's water quality technical criteria; or
- Initiated construction after July 1, 2014, using grandfathered plans using the City's water quality technical criteria.

Additionally, the City identified eight (8) projects that resulted in increased POC loads from New Sources because of the City's use of water quality criteria based on local impervious cover (Table 7). For these projects, the City revisited the previously City-approved stormwater plans and calculated the applicable increases in POC loads from New Sources using the following assumptions:

- Increases in New Source POC loads were identified when:
 - A land disturbing project utilized the design criteria associated with new development:
 - Increased loads were calculated based on the City design requirements, the 16% impervious cover, the site's acreage, and POC reductions associated with best management practice (BMP) implementation acreage identified in the site plan calculations.
 - A land disturbing project utilized the design criteria associated with redevelopment, and there
 was an increase in impervious cover.
 - Increased loads were calculated based on the predevelopment impervious cover and post-development impervious cover. Once BMP POC reductions were applied, increased loads were deducted from the credit associated with the 10% POC reduction requirement associated with the redevelopment design criteria.
- Decreases in New Source POC loads were identified when:
 - A land disturbing project utilized the design criteria associated with redevelopment and was required to reduce the POC load by the required 10%.
 - A land disturbing project resulted in a decrease in impervious cover from the predevelopment condition.

Table 7. New Source Loads from Projects Initiating Construction Between July 1, 2009 and June 30, 2014

Activity Name	Activity Address	New or Redevelopment	New Nitrogen Load, lbs./yr. (Total P lbs. x 6.9 lbs. N) ⁴	New Phosphorus Load, lbs./yr.
Fairfax Nursing Center - Commercial Addition to an Existing Building	10701 Main St.	Redevelopment < 1 Acre	-14	-1.97-
Farrish Dodge/Jeep - Commercial Building with Associated Parking	9610 Fairfax Blvd.	Redevelopment	-12	-1.71
Madison Mews at Old Town Village	3915 Chain Bridge Rd.	Redevelopment	-7.66	-1.11
Marriott Residence Inn - Hotel	3565 Chain Bridge Rd.	Redevelopment	-13	1.93

⁴ Negative pollutant loads represents a decrease in the pollutant load as a result of the redevelopment project.



Activity Name	Activity Address	New or Redevelopment	New Nitrogen Load, lbs./yr. (Total P lbs. x 6.9 lbs. N) ⁴	New Phosphorus Load, lbs./yr.
Providence Elementary Baseball Field - Providence Elementary School	3616 Jermantown Rd.	Redevelopment Final Design < 16% Impervious cover	N/A	N/A
Providence Park Tennis Courts - Recreational Facility	10615 Canfield St.	Redevelopment < 1 Acre	N/A	N/A
Lowrey Property (Clarks Corner)	Lowery Property	Redevelopment	2.39	0.5
Royal Legacy	Royal Legacy	New	72	10
The Army Navy Country Club	3315 Old Lee Highway	Redevelopment Final Design < 16% Impervious cover	N/A	N/A
Walgreens - Store #11570 - 10980 Fairfax Blvd.		Redevelopment	-8.90	-1.29
Yorktown Phase 1 - Jaguar			-36	-5.24
Yorktown Phase 2 - Cameron Glen	Yorktown Phase 2 - Cameron Glen	New	202	29.24
		Total New	185	27

5.0 City MS4 POC Reductions

The City utilized the revised acreages associated with Existing Sources to calculate L2 Run reduction requirements associated with Existing Sources (Table 8).

Table 8. Existing Source POC Load Reductions Necessary to Comply with the L2 Run

POC	Existing Source (Land Use)	Existing Source Load, lbs./yr.	Percent Reduction	Existing Source L2 Run Reductions Required, lbs./yr.	
Nitrogen	Regulated Impervious	25,425	9%	3,477	
	Regulated Pervious	19,818	6%		
Phosphorus	Regulated Impervious	2,443	16%	449	
	Regulated Pervious	807	7.25%		

As a result of the City's efforts, the cumulative 100% POC reductions from Existing Sources and increases in New Sources required to meet the L2 Run by October 31, 2028, are:

- Nitrogen 3,662 lbs./yr. (Existing Source 3,477 lbs./yr. + New Source 185 lbs./yr.)
- Phosphorus 476 lbs./yr. (Existing Source 449 lbs./yr. + New Source 27 lbs./yr.)



6.0 City Implementation of Phase I and Phase II Chesapeake Bay TMDL Action Plans

- 12. Chesapeake Bay TMDL action plan requirements....
 - b. For permittees previously covered under the 2018 GP...
 (4) A list of BMPs implemented prior to November 1, 2023, to achieve reductions associated with the Chesapeake Bay TMDL, including:
 - (a) The date of implementation; and
 - (b) The reductions achieved.

As of October 31, 2023, the City completed ten (10) POC reduction projects under Phase I and Phase II of the Chesapeake Bay TMDL Action Plans, including three (3) stream restoration projects, three (3) outfall and gully stabilization projects, three (3) BMP retrofits and one (1) Land Use Conversion.

- 1. Stream Restoration Daniels Run
- 2. Stream Restoration Tusico Creek Phase I
- 3. Stream Restoration Tusico Creek Phase II
- 4. BMP Retrofit City Pond
- 5. Outfall Restoration 3501 Lion Run
- 6. Outfall Restoration 3410 Pickett Road
- 7. Outfall Restoration 10400 Shiloh Street
- 8. Land Use Conversion Westmore Elementary
- 9. BMP Retrofit Westmore Elementary/Dog Park
- 10. BMP Retrofit University Drive Traffic Calming

In addition to the projects completed by the City, the City has:

- Achieved 10.10 lbs. of annual phosphorus reductions and 27.83 lbs. of annual nitrogen reduction as a condition of redevelopment
- Purchased 30 lbs. of phosphorus and 81 lbs. of nitrogen nonpoint source nutrient credits from the open market

The pollutant load reductions achieved by these are summarized in Table 9.



Table 9. City of Fairfax Chesapeake Bay TMDL Action Plan Projects Completed by October 31, 2023

	Loca	ition		Nitrogo	en, lbs./yr.	Phosphorus, lbs./yr.	
Project	Lat	Long	Implementation Date	Project Reduction	Remaining L2 Run Required Reduction	Project Reduction	Remaining L2 Run Required Reduction
		Requi	ed POC Load Reducti	ons Remaining	3,662		476
Stream Restoration: Daniels Run	38.8515	-77.2939	FY2016	57.38	3,605	52.02	424
Stream Restoration: Tusico Creek Phase I & Phase II	38.852	-77.3105	FY2023	141.38	3,463	128.18	296
BMP Retrofit: City Pond	38.8402	-77.2075	FY2023	7.36	3,456	0.40	295
Outfall Restoration: 3501 Lion Run	38.8625	-77.2894	FY2023	36.06	3,420	14.97	280
Outfall Restoration: 3410 Pickett Road	38.86042	-77.2743	FY2023	18.51	3,401	3.70	277
Outfall Restoration: 10400 Shiloh Street	38.86337	-77.3028	FY2023	17.09	3,384	9.25	267
Land Use Conversion: Westmore Elementary	38.8483	-77.3278	FY2012	4.44	3,380	0.00	267
BMP Retrofit: Westmore Elementary	38.8483	-77.3278	FY2019	4.39	3,375	0.60	267
BMP Retrofit: University Drive Traffic Calming	38.8569	-77.3019	FY2021	4.26	3,371	0.20	267
VSMP Implementation: Redevelopment Reductions from Existing Sources	-	-	FY19-FY2023	27.83	3,343	10.10	257
NPS Nutrient Credit Purchase: Whispering Hills	-	-	FY2023	81.00	3,262	30.00	227
Total Reductions, lbs./yr.				400 10.9 %		249	
	Percent of L2 Run Met, %					52.4%	

Summary discussions of each project identified in Table 9 are provided below.



Stream Restoration - Daniels Run

This project is a stream restoration of 765 linear feet of Daniels Run, located in the Accotink Creek watershed. The City received \$285,000 in Virginia Stormwater Local Assistance Fund (SLAF) funding to assist with this project, which was completed in FY2016. The Daniels Run Stream Restoration Project resulted in the annual reduction of 57.38 lbs. of nitrogen and 52.02 lbs. of phosphorus. Final calculations are provided in Appendix C.

Stream Restoration - Tusico Branch (Two Phases)

Tusico Creek Stream Restoration resulted in the restoration of 1,885 linear feet of stream in two phases. The first phase was completed in FY2021, and the second phase was completed in FY2023. The City received \$650,000 in SLAF funding to assist with financing this project. Pollutant removal calculations were based on the interim rates and calculated as follows:

- Nitrogen Removed 1,885 linear feet x 0.0375 lbs. of Nitrogen per linear foot = 141.38 lbs.
- Phosphorus Removed 1,885 linear feet x 0.068 lbs. of Phosphorus per linear foot = 128.18 lbs.

BMP Retrofit - City Hall Pond

This project is a retrofit of the pond on City Hall property, which converted an existing dry pond used for water quantity control to an extended detention pond. This retrofit installed a forebay located at the inflow and aquatic plantings and benches throughout the pond. This retrofit also slightly increased the total pond volume. The City completed the pond restoration in May 2023. The calculated POC removal provided was 9.05 lbs. total nitrogen per year and 0.66 lbs. total phosphorus per year. Calculations are provided in Appendix D.

Outfall Restoration - 3501 Lion Run Outfall and Gully Restoration Project

The Lion Run Outfall and Gully Restoration Project consists of the stabilization of approximately 375 linear feet of an actively eroding outfall channel that discharges into Accotink Creek. Completion of this project in FY2023 resulted in the annual reduction of POC totaling 36.06 lbs. of nitrogen and 14.97 lbs. of phosphorus. The final design calculations are provided in Appendix E.

Outfall Restoration - 3410 Pickett Road Outfall and Gully Restoration Project

The Pickett Road Outfall and Gully Restoration Project consists of stabilizing approximately 150 linear feet of an actively eroding outfall channel that discharges into Accotink Creek. Completion of this project in FY2023 resulted in the annual reduction of POC totaling 18.51 lbs. of nitrogen and 3.70 lbs. of phosphorus. The final design calculations are provided in Appendix F.

Outfall Restoration - 10400 Shiloh Street Outfall and Gully Restoration Project

The Shiloh Street Outfall and Gully Restoration Project consists of stabilizing approximately 250 linear feet of an actively eroding outfall channel that discharges into Accotink Creek. Completion of this project in FY2023 resulted in an annual reduction of POC totaling 17.09 lbs. of nitrogen and 9.25 lbs. of phosphorus. The final design calculations are provided in Appendix G.

Land Use Conversion & BMP Retrofit - Westmore Elementary School/Dog Park

This project was a redevelopment project that occurred in two phases. In FY2012, the Westmore Elementary School was demolished. In FY2019, the City constructed a dog park and level 2 bioretention stormwater management (SWM) facility within the school's original footprint. Combined, the two phases resulted in a net decrease of impervious cover of 1.04 acres (Figures 2 and 3). The level 2 bioretention SWM facility receives stormwater runoff from 0.24 acres of previously untreated impervious area and



0.27 acres of previously untreated pervious area, resulting in an annual pollutant load reduction of 8.82 lbs. of nitrogen/year and 0.59 lbs. of phosphorus/year.





2024

(Aerial Imagery Courtesy of Fairfax County Jade)

Figure 2. Westmore Elementary School Land Use in 2011 Figure 3. Westmore Elementary School Land Use in 2024 (Aerial Imagery Courtesy of Fairfax County Jade)

Table 10 provides the calculations for determining the nutrient load reductions for the Westmore Elementary School redevelopment based on the reduction in impervious cover. Appendix H provides the calculations for determining the nutrient load reductions for treating 0.24 acres of previously untreated impervious land use and 0.27 acres of previously untreated pervious urban land use with the level 2 bioretention SWM facility.

Table 10. Westmore Elementary School Pollutant Load Reductions Resulting from Land Use Conversion

Pollutant	Impervious Area Prior to Westmore Elementary School Demolition, acres	Impervious Area After Westmore Dog Park, acres	Net Reduction of Impervious Area, acres	Land Use Conversion Efficiency Table V.H.1. (Impervious to Turf)	Annual Pollutant Load Reduction
Nitrogen	3.37	2.33	1.04	(4.27)	(4.44)
Phosphorus	3.37	2.33	1.04	-	-

BMP Retrofit - University Drive Traffic Calming

This University Drive Traffic Calming Project resulted in the FY2021 installation of bioretention facilities as part of a larger overall project designed to reduce traffic and speeding on University Drive. The bioretention facilities provide stormwater management for 0.63 acres (0.20 acres of managed turf and 0.43 acres of impervious cover) of previously untreated developed urban land in the Accotink Creek watershed. The annual POC reduced from installing these bioretention facilities totals 4.26 lbs. of nitrogen and 0.20 lbs. of phosphorous. The final calculations are provided in Appendix I.

VSMP Implementation - Redevelopment on Prior Developed Lands

The City operates a DEQ-approved VSMP Program through which it requires pollutant reductions on prior developed lands as part of the redevelopment process. Between FY2019 and FY2023, the City approved 48 plans where new developments were required to reduce pollutant loads to meet the VSMP



design standard for new development, and redevelopments were required to reduce the existing pollutant load by either 10% or 20%, based on the size of the land disturbance. The City developed and utilized the Calculating VSMP POC Reductions Creditable to Chesapeake Bay Existing Source Load Reductions SOPs (Appendix J) to identify the portion of the pollutant load reduction achieved that could be credited towards the existing load reduction requirements. The implementation of the VSMP program resulted in the pollutant load reduction of 227.83 lbs./year of nitrogen and 10.10 lbs./year of phosphorus. The location and applicable pollutant load associated with each redevelopment project are provided in Appendix K.

NPS Nutrient Credit Purchase: Whispering Hills

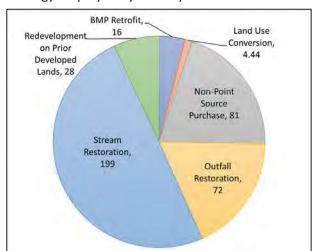
The City purchased 30 lbs. of phosphorous credits and 81 lbs. of nitrogen credits on November 2, 2022, from the Whispering Hills nonpoint nutrient credit bank, located in the Accotink Creek watershed. The MS4 Nutrient Credit Acquisition Form for this purchase can be found in Appendix L.

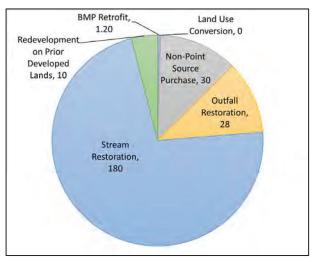
6.1 Phase II Chesapeake Bay TMDL Action Plan Compliance Assessment

Projects completed throughout the implementation of the City's Phase II Chesapeake Bay TMDL Action Plan have resulted in the annual reduction of:

- 400 lbs./yr. of nitrogen (10.9% of the cumulative 100% L2 Run required nitrogen reduction)
- 249 lbs./yr. of phosphorus (52.4% of the cumulative 100% L2 Run required phosphorus reduction)

Figures 4 and 5 provide a breakdown of the pollutant reductions by the type of pollutant reduction strategy employed by the City.





per Year Completed Through Phase II

Figure 4. Annual Nitrogen Load Reductions in Pounds Figure 5. Annual Nitrogen Load Reductions in Pounds per Year Completed Through Phase II

The City will rely on its Water Quality Credit Agreement with Fairfax County for the acquisition of annual nutrient credits from the NCPCP to maintain the minimum of a 40% compliance requirement of 40% of the L2 Run while implementing Phase III of the Chesapeake Bay TMDL Action Plan.

The City will submit copies of the DEQ MS4 Nutrient Credit Acquisition Form as part of the Chesapeake Bay TMDL Implementation Annual Status Report, as required by the MS4 General Permit. A copy of the 2023 DEQ MS4 Nutrient Credit Acquisition Form is included in Appendix M.



7.0 City Phase III Chesapeake Bay TMDL Action Plan

- 12. Chesapeake Bay TMDL action plan requirements....
 - b. For permittees previously covered under the 2018 GP...
 - 5) The BMPs to be implemented by the permittee within 60 months of the effective date of this permit to meet the cumulative reductions calculated in Part II A 3, A 4, and A 5, including as applicable:
 - (a) Type of BMP;
 - (b) Project name;
 - (c) Location;
 - (d) Percent removal efficiency for each pollutant of concern; and
 - (e) Calculation of the reduction expected to be achieved by the BMP calculated and reported in accordance with the methodologies established in Part II A 9 for each pollutant of concern; and
 - (f) A preliminary schedule for implementation of the BMPs included in the Chesapeake Bay TMDL action plan.

The City has eleven (11) projects in various stages of design or construction that will be completed during the Phase III Chesapeake Bay TMDL Action Plan, including one (1) stream restoration project, six (6) outfall restoration projects, one (1) Land Cover Conversion, and three (3) BMP Retrofits:

- 1. Stream Restoration Stafford Drive
- 2. Outfall Restoration #1 3300 Stafford Drive
- 3. Outfall Restoration #2 3300 Stafford Drive
- 4. BMP Retrofit Ashby Pond Wet Pond
- 5. Land Cover Conversion Van Dyck Park
- 6. Outfall Restoration Van Dyck Park (Outfall #4)
- 7. Outfall Restoration Traveler Street #1
- 8. Outfall Restoration Traveler Street #2
- 9. Outfall Restoration Providence Park
- 10. BMP Retrofit Mathy Park
- 11. BMP Retrofit Lion Run

The pollutant load reductions achieved by these are summarized in Table 11.



Table 11. City of Fairfax Phase III Chesapeake Bay TMDL Action Plan Projects

Location		tion	Anticipated	Nitrogen	Nitrogen, lbs./yr.		Phosphorus, lbs./yr.	
Project	Lat	Long	Anticipated Completion Date	Project Reduction	Remaining L2 Run Reductions Required	Project Reduction	Remaining L2 Run Reductions Required	
			Remaining P	OC Load Reductions	3,262		227	
Stream Restoration: Stafford Drive	38.8648	-77.2919	FY26	323.66	2,939	181.04	46	
Outfall Restoration #1: 3300 Stafford Drive	38.86354	-77.2943	FY26	3.38	2,935	9.76	36	
Outfall Restoration #2: 3300 Stafford Drive	38.86342	-77.2942	FY26	9.41	2,926	23.68	12	
BMP Retrofit: Ashby Pond Wet Pond	38.8479	-77.2861	FY26	351.54	2,574	87.52	-75 ⁵	
Land Cover Conversion: Van Dyck Park	38.8547	-77.2989	FY26	0.95	2,573	0.25	-76	
Outfall Restoration: Van Dyck Park	38.8547	-77.2989	FY27	134.27	2,439	81.47	-157	
Outfall Restoration: Traveler Street #1	38.86	-77.2929	FY27	10.59	2,429	4.30	-161	
Outfall Restoration: Traveler Street #2	38.8684	-77.2933	FY27	5.56	2,423	1.70	-163	
Outfall Restoration: Providence Park	38.8397	-77.3145	FY27	24.16	2,399	10.89	-174	
BMP Retrofit: Mathy Park	38.8397	-77.3145	FY27	5.63	2,417	0.40	-174	
BMP Retrofit: Lion Run	38.8626	-77.2894	FY27	7.60	2,391	0.64	-175	
Phase III Total Reductions, lbs./yr. Nitrogen 877 Phosphorus 401						401		

Summary discussions of each project identified in Table 10 are provided below.

 $^{^{\}rm 5}$ 100% of L2 Run Phosphorus Load Reductions Achieved



Stream Restoration - Stafford Drive Stream Restoration

The Stafford Drive Stream Restoration Project is a combination of 2,300 linear feet of restoration of the North Fork of Accotink Creek and the restoration of two actively eroding outfalls on Stafford Park property. The City received \$1,175,000 in SLAF funding for the Stafford stream and outfall restoration projects and anticipates completing the stream restoration in FY2026. The City calculates the annual POC removed by the stream restoration portion of the project as 323.66 lbs. of nitrogen and 181.04 lbs. of phosphorus. The stream restoration calculations are provided in Appendix N.

Outfall Restoration - 3300 Stafford Drive Outfall #1

The Stafford Drive Outfall #1 Restoration Project will result in the restoration of a 90-foot reach of an actively eroding outfall channel. Once completed, this project's calculated annual pollutant load reductions are 3.38 lbs. of nitrogen and 9.76 lbs. of phosphorus. Calculations are provided in Appendix N with the Stafford Stream Restoration.

Outfall Restoration - 3300 Stafford Drive Outfall #2

The Stafford Drive Outfall #2 Restoration Project will restore a 48.57-foot reach of an actively eroding outfall channel. Once completed, this project's calculated annual pollutant load reductions are 9.41 lbs. of nitrogen and 23.68 lbs. of phosphorus. Calculations are provided in Appendix N with the Stafford Stream Restoration.

BMP Retrofit - Ashby Pond Wet Pond

This project is an enhancement of an existing wet pond located in the Accotink Creek watershed to meet the current BMP Specification 14 (Wet Pond) Design Standards. This project involves the restoration and stabilization of both inflows and the outfall channel, the installation of two large forebays at the inflows, the addition of aquatic plantings/benches, and conducting a complete dredging of the pond. The anticipated completion date of this stream restoration is FY2026. The calculated annual POC load removed through the Ashby Pond Conservancy Project is 351.54 lbs. of nitrogen and 87.52 lbs. of phosphorous. Calculations for this project are provided in Appendix O.

Land Cover Conversion - Van Dyck Park

The Van Dyck Park Land Cover Conversion Project converts 0.17 acres of turf in Van Dyck Park to forest with an anticipated completion date of FY2026. The calculated annual pollutant removal associated with the Van Dyck Land Cover Conversion project is calculated to total 0.95 lbs. of nitrogen and 0.25 lbs. of phosphorous. Calculations for this land cover conversion project are provided in Table 12.

Table 12. Van Dyck Park Pollutant Load Reductions Resulting from Land Use Conversion

Pollutant	Area Converted from Turf to Forest, acres	Land Use Conversion Efficiency Table V.H.1. (Turf to Forest)	Annual Pollutant Load Reduction
Nitrogen	0.17	(5.58)	(0.95)
Phosphorus	0.17	(1.46)	(0.25)

Outfall Restoration - Van Dyck Park (Outfall #4)

The Van Dyck Park Outfall Restoration Project will result in the restoration of approximately 329 linear feet of actively eroding outfall channel in the Accotink Creek watershed, resulting in a calculated annual reduction of 134.27 lbs. of nitrogen and 81.47 lbs. of phosphorus. The City received \$362,720 in SLAF



funding and anticipates completing this project in FY2027. The calculated pollutant load reductions for this project are provided in Appendix P.

Outfall Restoration - Traveler Street #1

The Traveler Street Outfall Restoration Project will result in the the restoration of two currently eroding outfalls that discharge to the Dale Lestina tributary of Accotink Creek. Restoration of Channel #1 will result in the restoration of approximately 60 feet of actively eroding outfall channel, resulting in the calculated annual reduction of 10.59 lbs. of nitrogen and 4.30 lbs. of phosphorus. The City received \$137,902 in SLAF funding and anticipates completion of this project in FY2027. The pollutant load reduction calculations are combined with the Outfall #2 calculations in Appendix Q.

Outfall Restoration - Traveler Street #2

The second outfall of the Traveler Street Outfall Restoration Project will result in restoration of approximately 90 feet of actively eroding outfall channel, resulting in a calculated annual reduction of 5.56 lbs. of nitrogen and 1.70 lbs. of phosphorus. Pollutant load reduction calculations are combined with the Outfall #1 calculations in Appendix Q.

Outfall Restoration - Providence Park

The Providence Park Outfall Restoration Project will result in the restoration of approximately 200 feet of actively eroding outfall channel in the Popes Head Run watershed, resulting in a calculated annual reduction of 24.16 lbs. of nitrogen and 10.89 lbs. of phosphorus. The City received \$186,017 in SLAF funding and anticipates completion of this project in FY2027. The calculated estimated pollutant load reductions for this project are provided in Appendix R.

BMP Retrofit - Mathy Park

The Mathy Park Stormwater Retrofit Project redirects stormwater from three locations in Mathy Park so that it discharges via Sheet Flow into Open Space, with an anticipated completion date of FY2027. Upon completion, the Mathy Park BMP retrofit will treat stormwater from 0.37 acres of previously untreated urban impervious acres and 0.50 acres of previously untreated urban pervious acres, resulting in the calculated annual reduction of an estimated 5.63 lbs. of nitrogen and 0.40 lbs. of phosphorous. The calculated pollutant load reductions for this project are provided in Appendix S.

BMP Retrofit - Lion Run

The Lion Run BMP Retrofit Project will upgrade an existing dry pond at Fairfax High School to meet the Level 1 Extended Detention Pond design standards. The City will construct a forebay and aquatic benches and will install micropools while increasing the pond's overall storage capacity. When completed in FY2027, the Lion Run BMP Retrofit will result in a calculated annual reduction of 7.60 lbs. of nitrogen and 0.64 lbs. of phosphorous in the Accotink Creek watershed. The calculated pollutant load reductions for this project are provided in Appendix T.

7.1 Phase III Chesapeake Bay TMDL Action Plan Pollutant Additional Strategies

The City will also continue to identify and implement pollutant load reductions associated with the following strategies to further reduce its reliance on acquiring nutrients through annual private nutrient exchanges with the NCPCP.



Reductions Associated with Nonpoint Source Nutrient Credit Purchases

The City will consider the purchase of additional nonpoint source nutrient credits from a DEQ-accredited nutrient bank if it is in the City's best interest. Future purchases will be reported in the appropriate City's Chesapeake Bay TMDL Implementation Annual Status Report.

Reductions Associated with Capital Improvement Projects

The City maintains an updated Capital Improvement Plan (CIP) as part of its annual budget process. The City's CIP currently contains numerous future projects, including those identified specifically as drainage and flood relief projects. As these CIP projects progress through the design phase, the City will evaluate them for potential opportunities to implement pollutant reductions. The City will update its Chesapeake Bay TMDL Action Plan as warranted when opportunities are identified for implementation.

Reductions Associated with VESMP Implementation on Redevelopment

Through the implementation of its VESMP, the City requires phosphorus load reductions of 10% from redevelopment projects with a land disturbance between 2,500 ft.² and one acre and 20% from redevelopment projects with land disturbances of one acre or greater. The City will utilize the Virginia Runoff Reduction Method (VRRM) Compliance Spreadsheets to obtain the pollutant load reduction equivalent to the phosphorus load reduction associated with existing impervious cover and any POC reduction implemented that is greater than the reduction required for new development. BMPs, including on-site stormwater management facilities and off-site nonpoint nutrient credits, will be reported to DEQ through the BMP Warehouse but will represent the BMP load reductions as applied to the entire redevelopment project and not be divided between POC load reductions assigned to new development or redevelopment of existing impervious cover.

Pollutant load reductions associated with both private and public redevelopment projects to comply with VSMP redevelopment criteria will be credited toward the Existing Source load reductions. Creditable pollutant load reductions will be calculated using the Calculating VSMP POC Reductions Creditable to Chesapeake Bay Existing Source Load Reductions SOPs.

Reductions Associated with Local TMDL Action Plan Projects

As of November 1, 2023, the City is required to develop and implement local TMDL Action Plans to address the following local TMDLs:

- Chloride TMDLs for the Accotink Creek Watershed, Fairfax County, Virginia
- Sediment TMDLs for the Accotink Creek Watershed, Fairfax County, Virginia
- Benthic TMDL Development for Bull Run, Virginia
- Benthic TMDL Development for Popes Head Creek, Virginia
- Benthic TMDL Development for Difficult Run, Virginia
- Fecal Coliform TMDL for Accotink Creek, Fairfax County, Virginia
- Bacteria TMDL for the Difficult Run Watershed, Virginia
- Bacteria TMDLs for Popes Head Creek, Broad Run, Kettle Run, South Run, Little Bull Run, Bull Run, and the Occoquan River, Virginia

The City will evaluate its POC reduction strategies implemented as part of Local TMDL Action Plans for equivalent pollutant reductions applicable to the Chesapeake Bay TMDL pollutant reduction requirements. Equivalent pollutant load reductions implemented through the implementation of local TMDL Action Plans will be credited toward the Existing Source load reductions.



Reductions Associated with Storm Drain Cleaning (Annual Reduction)

With the February 6, 2021 publication of Guidance Memo No. 20-2003 (GM #20-2003), DEQ adopted the EPA Chesapeake Bay Program's (CBP) "Recommendations of the Expert Panel to Define Removal Rates for Street and Storm Drain Cleaning (SDC) Practices, Final Report, May 19, 2016, (CBP Final Report) as the sole acceptable methodology to quantify associated Chesapeake Bay TMDL POC reduction credits in Virginia after June 30, 2022. GM #20-2003 defines the requirements and expectations SDC programs must implement for associated POC reductions to be credited towards meeting Existing Source load reductions.

In response, the City assessed the potential for the City to obtain annual Existing Source POC load reductions for credit against the Existing Source pollutant loads (Appendix U - Storm Drain Cleaning Assessment and Procedures). Concurrent with its assessment, the City developed procedures consistent with the CBP Final Report designed to quantify the POC reductions associated with the City initiatives. The City has yet to implement these procedures at this time; however, it retains the possibility of implementing them in the future should the need become warranted.

Reductions Associated with Leaf Litter Collection and Disposal (Annual Reduction)

The City has completed a desktop analysis regarding the potential of achieving Existing Load POC load reductions through the City's Leaf Litter Collection and Disposal Program (Appendix V - Chesapeake Bay POC Reduction and Crediting Associated with Leaf Litter Collection and Disposal Discussion). Although the City has not approached DEQ for approval of this non-traditional POC reduction strategy as a means of achieving the necessary pollutant reductions, the City retains the possibility of seeking DEQ approval in the future should the need become warranted. Future pollutant load reductions associated with leaf litter collection and disposal will be calculated and credited towards the Existing Source load reductions on an annual basis upon future DEQ approval conditions.

7.2 Phase III Chesapeake Bay TMDL Action Plan Compliance Assessment

Based on the achieved pollutant load reductions completed through Phase II of the Chesapeake Bay TMDL Action Plan and the anticipated pollutant load reductions that will be completed through Phase III, the City estimates that it will have implemented annual pollutant load reductions of:

- 1,276 lbs./yr. of nitrogen (35% of the required 100% L2 Reduction)
- 651 lbs./yr. of phosphorus (137% of the required 100% L2 Reduction)

Figure 6, in combination with Table 13, provides a geographic record of the locations at which the City will have completed Chesapeake Bay TMDL Action Plan pollutant load reduction projects by October 31, 2028. Figures 7 and 8 provide a record of the types of pollutant load reduction projects employed by the City.



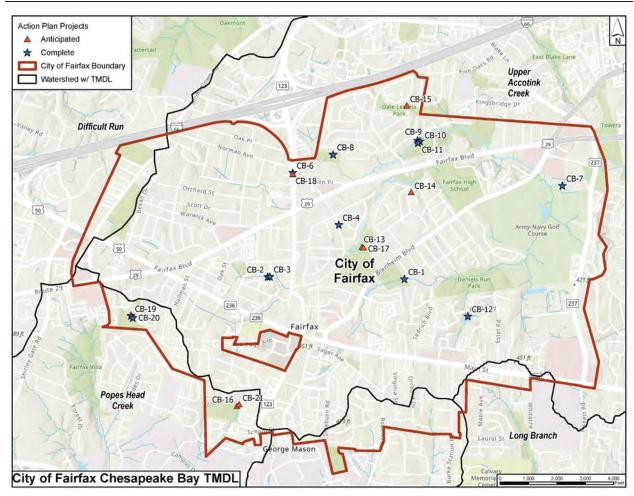


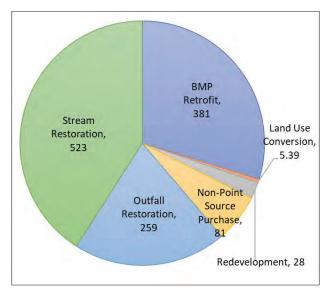
Figure 6. Locations of Completed and Anticipated Chesapeake Bay TMDL Pollutant Load Reductions in the City of Fairfax, VA

Table 13. BMP Identification in Figure 6

BMP	Location	Description	ВМР Туре
CB-1	Daniels Run Stream Restoration Project	Complete	Stream Restoration
CB-2	Tusico Creek Restoration, Phase I	Complete	Stream Restoration
CB-3	Tusico Creek Restoration, Phase II	Complete	Stream Restoration
CB-4	University Drive Traffic Calming Retrofit	Complete	SWM Retrofit
CB-5	City Pond Retrofit	Complete	SWM Retrofit
CB-6	Outfall Restoration - Lion Run Site	Complete	Outfall Restoration
CB-7	Outfall Restoration - Pickett Road Site	Complete	Outfall Restoration
CB-8	Outfall Restoration - Shiloh Street Site	Complete	Outfall Restoration
CB-9	Stafford Drive Stream Restoration	Complete	Stream Restoration
CB-10	Stafford Drive Outfall Restoration 1	Complete	Outfall Restoration
CB-11	Stafford Drive Outfall Restoration 2	Complete	Outfall Restoration
CB-12	Ashby Pond Wet Pond Enhancement	Complete	SWM Retrofit
CB-13	Van Dyck Park Outfall Restoration	Anticipated	Outfall Restoration
CB-14	Traveler Street Outfall Restoration 1	Anticipated	Outfall Restoration
CB-15	Traveler Street Outfall Restoration 2	Anticipated	Outfall Restoration
CB-16	Mathy Park/FFX HS	Anticipated	SWM Retrofit
CB-17	Van Dyck Land Cover Conversion	Anticipated	Land Cover Conversion
CB-18	BMP Retrofit at Lion Run (FFX HS)	Anticipated	SWM Retrofit



ВМР	Location	Description	ВМР Туре
CB-19	Westmore Dog Park	Complete	Land Cover Conversion
CB-20	Westmore Dog Park	Complete	SWM Retrofit
CB-21	Providence Park Outfall	Anticipated	Outfall Restoration



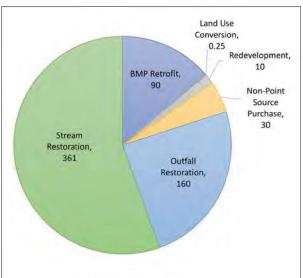


Figure 7. Anticipated Total Annual Nitrogen Load Reductions Achieved Through Phase III TMDL Action Plan – 1,276 lbs./yr.

Figure 8. Anticipated Total Annual Phosphorus Load Reductions Achieved Through Phase III TMDL Action Plans - 651 lbs./yr.

Upon the completion of these projects, the City is estimated to still be responsible for these additional POC reductions by October 31, 2028:

- Nitrogen reductions totaling 2,386 lbs./yr.
- Phosphorus 0 additional phosphorus reductions are required. The L2 Run requirements will be met.

The City's estimated responsibility does not include any of the identified strategies for which pollutant load reductions were not available. The City will rely on its MOU with Fairfax County to acquire annual nutrient credits from the NCPCP to attain the compliance requirement of 100% of the L2 Run by October 31, 2028. The City will submit copies of the DEQ MS4 Nutrient Credit Acquisition Form as part of the Chesapeake Bay TMDL Implementation Annual Status Report, as required by the MS4 General Permit.

8.0 Progress Tracking and Documentation

The MS4 General Permit, Chesapeake Bay TMDL Special Condition, requires tracking and documenting specific to implementing the TMDL Action Plan. Table 14 provides the City with an annual checklist of required tracking and documenting Chesapeake Bay TMDL Action Implementation, which must be submitted to DEQ when the City obtains nutrient credits that it intends to apply towards MS4 Existing Source load reductions.

Progress made annually between July 1 and June 30 must be reported in a stand-alone Chesapeake Bay TMDL Action Plan Annual Status Report that includes:



- A list of Chesapeake Bay TMDL Action Plan BMPs, not including annual practices implemented prior to the reporting period, that includes the following information for reported BMPs:
 - The number of BMPs for each BMP type.
 - The estimated reduction of POC achieved by each BMP type and reported in pounds of POC reduction per year.
 - A confirmation statement that the City electronically reported Chesapeake Bay TMDL Action Plan BMPs inspected using the DEQ BMP Warehouse.
 - A list of newly implemented BMPs, including annual practices implemented during the reporting period that includes the following information for each reported BMP or a statement that no BMPs were implemented during the reporting period:
 - The BMP type and a description of the location for each BMP.
 - The estimated reduction of POC achieved by each BMP and reported in pounds of POC reduction per year.
 - A confirmation statement that the City electronically reported the BMPs using the DEQ BMP warehouse.
 - If the City acquires credits during the reporting period to meet some or all of the POC reductions, a statement that credits were acquired.
 - The progress, using the final design efficiency of the BMPs, towards meeting the required cumulative reductions for the POC.
 - Any revisions made to the Chesapeake Bay TMDL Action Plan.
 - A list of BMPs planned to be implemented during the next reporting period.



Table 14. City of Fairfax Chesapeake Bay TMDL Action Plan Annual Compliance Checklist

B	Schedule /	Complete		
Requirement	Due Date	Yes	No	N/A
VESCP implementation compliant with the MS4 General Permit	Continuous, until 6/30/2024			
VSMP implementation compliant with the MS4 General Permit	Continuous, until 6/30/2024			
VESMP implementation compliant with MS4 General Permit	Continuous, after 7/1/2024			
CBPA implementation compliant with the MS4 General Permit	Continuous			
Nutrient Management Plan implementation compliant with the MS4 General Permit	Continuous			
Development and electronic submittal of a Chesapeake Bay TMDL Implementation Annual Status Report covering activities of the previous permit year (July 1 through June 30)	Annually, no later than November 1			
Provide the public a minimum of 15 days to comment on the Phase III Chesapeake Bay TMDL Action Plan prior to its submittal to DEQ	Prior to October 31, 2024			
Submit a Phase III Chesapeake Bay TMDL Action Plan to DEQ	October 31, 2024			
Summary of Comments and Responses to Public Comments in Year 2 Chesapeake Bay TMDL Action Plan Implementation Annual Status Report	October 31, 2025			
Maintain a Minimum POC Reduction Equivalent to 40% of the L2 Run POC Reduction Requirements	Annually through October 31, 2028			
Utilize the MS4 Nutrient Credit Acquisition Form to certify the nitrogen credits that were obtained for the previous calendar year	Annually, no later than June 1			
Report all BMPs newly installed between July 1 and June 30 of each permit year in which POC reductions are credited towards Chesapeake Bay TMDL POC load reduction compliance	Annually, no later than October 1			
Inspect City owned or operated SWM facilities. Verify that the SWM facilities are functioning as designed and constructed	Annually			
Inspect privately owned SWM facilities	No less than once per five years			
Inspect ecosystem restoration projects (e.g., stream restoration)	At least once every 60 months			
Update the latest inspection date of all BMPs in which POC reductions are credited towards Chesapeake Bay TMDL POC load reduction compliance using the DEQ BMP warehouse	Annually, no later than October 1			
Attain a POC Reduction Equivalent to 100% of the L2 Run POC Load Reduction Requirements	October 31, 2028			
Maintain a Minimum POC Reduction Equivalent to 100% of the L2 Run POC Reduction Requirements	After October 31, 2028			



9.0 Opportunity for Public Comment Summary

13. Prior to submittal of the action plan required in Part II A 12 a and b, permittees shall provide an opportunity for public comment for no fewer than 15 days on the additional BMPs proposed in

The MS4 General Permit requires the City to allow the public to comment on the additional BMPs proposed as part of the Phase III Chesapeake Bay TMDL Action Plan. The City must provide an opportunity that is no less than 15 days. The opportunity to comment on the City of Fairfax's Phase II Chesapeake Bay Action was provided as documented below.

The public was notified of the opportunity to comment on 9/16/2024

Check Applicable Box(es)					
☑ Publication on the City Website	☐ Publication in Local Newspapers	☐ Social Media			
www.fairfaxva.gov					
☐ Publication in a City Publication	□ Other	☐ Other			

Public Comments were received between September 16, 2024 and October 1, 2024. A summary of the comments received, and the City's responses are included in Appendix W.



Appendix A – City/NCPCP Water Quality Agreement for Chesapeake Bay TMDL Implementation



County of Fairfax, Virginia

To protect and enrich the quality of life for the people, neighborhoods and diverse communities of Fairfax

October 19, 2020

Mr. Satoshi Eto Stormwater Resource Engineer City of Fairfax Department of Public Works 10455 Armstrong Street City Hall Annex, Suite 200 Fairfax, VA 22030

Reference: Water Quality Credit Agreement for Chesapeake Bay Total Maximum Daily Loads Implementation

Dear Mr. Eto:

Enclosed for your files is a fully executed original of the subject agreement for Chesapeake Bay Total Maximum Daily Loads (TMDL) Implementation.

Thank you for your assistance during the negotiation of this agreement. If you have any questions regarding this matter, please do not hesitate to contact me at 703-324-5026.

Sincerely.

Shahram Mohsenin, P.E.

Director

Encl: Water Quality Credit Agreement for Chesapeake Bay TMDL Implementation

cc: Michael McGrath, Director, Department of Public Works and Environmental Services (DPWES), Wastewater Treatment Division

Anand Goutam, Financial Manager, DPWES, Wastewater Planning and Monitoring Division





www.fairfaxcounty.gov/publicworks

WATER QUALITY CREDIT AGREEMENT FOR CHESAPEAKE BAY TMDL IMPLEMENTATION

BACKGROUND

- The County's Wastewater Treatment Plant. The County owns and operates an A. advanced wastewater treatment plant known as the Noman M. Cole, Jr., Pollution Control Plant ("NCPCP"), which is authorized to discharge the nutrients total nitrogen ("TN") and total phosphorus ("TP") as well as sediment expressed as total suspended solids ("TSS") within the Chesapeake Bay watershed in accordance with (a) certain water quality plans or regulations including the Chesapeake Bay Total Maximum Daily Load ("TMDL") issued by the U.S. Environmental Protection Agency ("EPA"), the related Virginia Chesapeake Bay TMDL Watershed Implementation Plan ("WIP") issued by the Commonwealth of Virginia, and the Water Quality Management Planning Regulation, 9 VAC 25-720, issued by the State Water Control Board and Virginia Department of Environmental Quality (jointly, "DEQ"), and (b) the General Virginia Pollutant Discharge Elimination System ("VPDES") Watershed Permit Regulation for TN and TP Discharges and Nutrient Trading in the Chesapeake Bay Watershed in Virginia, 9 VAC 25-820, most recently reissued by DEQ effective February 8, 2017, as hereafter modified or reissued from time to time (the "Watershed General Permit"). Due to exceptional performance and current operating conditions, NCPCP currently discharges less TN, TP and TSS than authorized under the Watershed General Permit and Chesapeake Bay TMDL while protecting Chesapeake Bay water quality and, therefore, the County has the ability to generate and supply TN, TP and TSS credits on at least a temporary basis. The rated capacity of NCPCP is 67 million gallons per day ("MGD") and, pursuant to the Appendix IV of the General Services Agreement of 2003 (the "General Services Agreement"), the County has reserved 4.2 MGD of treatment capacity for the City's use.
- B. The City's Stormwater System. The City owns and operates a municipal separate stormwater sewer system ("MS4") authorized to discharge nutrients and sediment to the Chesapeake Bay watershed. Like NCPCP, the MS4 is addressed under the Chesapeake Bay TMDL and WIP. The MS4 is subject to the General VPDES Permit for Stormwater Discharged from Small Municipal Separate Storm Sewer Systems (the "MS4 Permit") under which DEQ has issued coverage to the City. Pursuant to the Chesapeake Bay TMDL, WIP and MS4 Permit, it is anticipated that the City will reduce nutrient and sediment discharges from the MS4 pursuant to City-developed and DEQ-approved TMDL Action Plans for each of three, five-year permit cycles, which are referred to as the First Bay TMDL Permit Cycle (5% Progress), Second Bay TMDL Permit Cycle (40% Progress), and Third Bay TMDL Permit Cycle (100% Progress). During 2020, the City is in its Second Bay TMDL Permit Cycle (2018-2023).
- C. <u>The City's Plan for Continuing Compliance</u>. The City achieved its Chesapeake Bay TMDL reduction goals for the First Bay TMDL Permit Cycle by implementation of certain best

management practices ("BMPs") by June 30, 2018. During the Second Bay TMDL Permit Cycle, a combination of factors present major compliance challenges including a substantially higher reduction target (40% compared to 5%), the possible statewide downrating of the benefits of the street sweeping credits, and financial obstacles stemming from the 2020 pandemic. To better manage these challenges and promote compliance, rather than relying exclusively on financing and constructing retrofit projects on a condensed 5-year schedule (i.e., Second Bay TMDL Permit Cycle) or 10-year schedule (Third Bay TMDL Permit Cycle), the City is expanding its TMDL reduction strategies to include acquisition and use of TN, TP and TSS credits to be generated and supplied by NCPCP. This compliance method also better incorporates ongoing stormwater quality improvements from redevelopment projects, which are subject to TP reduction criteria (and associated TN and TSS reductions) under the applicable water quality design requirements of DEQ's Virginia Stormwater Management Program Regulation, 9VAC25-870-63.A.2. By aligning with the normal redevelopment cycle rather than scheduling retrofits prior to redevelopment activity, the City's Chesapeake Bay TMDL Action Plan will also conserve scarce state (Stormwater Local Assistance Fund) and local resources for other important water quality projects and public needs.

D. <u>Legal Authority</u>. Pursuant to Virginia Code § 62.1-44.19:21, the City may acquire and use nutrient credits for purposes of compliance with the Chesapeake Bay TMDL loading reductions of the MS4 Permit, including credits generated by the County's NCPCP by discharging less TN or TP than permitted under the Watershed General Permit. Pursuant to Virginia Code § 62.1-44.19:21.1, the City may also acquire and use sediment credits for purposes of compliance with the Chesapeake Bay TMDL loading reductions of the MS4 Permit, including credits generated by the County's NCPCP by discharging less TSS than allocated under the Chesapeake Bay TMDL and WIP. With respect to all three parameters, it is recognized that this authority does not limit or otherwise affect the authority of DEQ to establish and enforce more stringent water quality-based effluent limitations in permits where such limitations are necessary to protect local water quality and, further, that the use of water quality credits does not relieve an MS4 permit holder of any requirement to comply with any applicable local water quality-based limitations.

AGREEMENT

NOW, THEREFORE, in consideration of the foregoing premises (hereby incorporated as if fully set forth herein), the mutual covenants and conditions herein, and other good and valuable consideration, the receipt and sufficiency of which the County and the City acknowledge, the Parties hereby agree as follows.

1. Credit Quantities. Beginning for the compliance year (January 1 through December 31) which starts January 1, 2022 and for each compliance year thereafter through and including compliance year 2030, the County agrees to transfer annually to the City a pro rata share of the County's available NCPCP-generated TN, TP and TSS credits not to exceed (a) the City's actual credit need for MS4 Permit compliance or (b) the maximum quantity set forth on the City's Required Credit Schedule for MS4 Permit Compliance in Attachment A hereto, whichever is less on a parameter-by-parameter basis. Available credits are expected to vary annually based on the operating conditions experienced at NCPCP, the facility's actual performance, and applicable laws, regulations and permits then in effect. The City's pro rata share shall be based on the portion

of NCPCP treatment capacity reserved for the City's use (4.2 MGD) compared to total treatment capacity (currently 67 MGD). This Agreement does not guarantee to the City the availability of a sufficient quantity of credits in any year, nor does it impose upon the County any requirement to operate NCPCP in any particular manner or at any additional expense to provide such credits. For purposes of this Agreement, "credit" means a "point source nitrogen credit" or "point source phosphorus credit" as defined in the Watershed General Permit or "sediment credit" as defined in Virginia Code § 62.1-44.19:21.1.

- 2. Annual Transfer Procedure. For each compliance year for which this Agreement is in effect and subject to the requirements and limitations of Paragraph 1 above, the City shall request in writing and the County shall transfer the available credits to the City by May 20 immediately following the compliance year during which the County generated the credits. Such transfer shall be made in writing using the Water Quality Credit Transfer Form set forth in Attachment B hereto. The first such transfer shall occur by May 20, 2023 using compliance year 2022 credits.
- 2. Price of Credits. In light of the County's reservation of treatment capacity for the City and the City's responsibility for a certain portion of capital costs and operation and maintenance costs under the General Services Agreement, there shall be no additional monetary cost charged by the County to the City for the City's pro rata share of available credits up to and including the maximum quantities set forth on the credit schedule in Attachment A hereto; however, the City agrees that its share of any credit sales revenue obtained by the County from sale of NCPCP-generated credits through the Virginia Nutrient Credit Exchange Association, Inc. (the "Nutrient Exchange") or otherwise shall be reduced to account for the transfer of credits to City for its direct use. For example, if 100% of the City's pro rata share of NCPCP-generated credits are transferred to the City in a given year, the City shall receive no portion of the credit sales revenue derived from the remaining NCPCP credits in that year. As another example, if 50% of the City's pro rata share of NCPCP-generated credits are transferred to the City in a given year, the City shall receive only 50% of the amount of the credit sales revenue derived from the remaining NCPCP credits that it would otherwise have received.
- 4. <u>Authorized Use</u>. The City agrees that its sole and limited use of the credits transferred under this Agreement shall be for the purpose of MS4 Permit compliance and Chesapeake Bay TMDL implementation under such permit as described herein and that it shall not transfer any portion of the NCPCP-generated credits to any other person or entity.
- 5. Term. This Agreement shall be in effect as of the date first shown above upon execution by both Parties and shall expire on June 30, 2030. Notwithstanding the preceding sentence, if either Party fails to perform a material obligation hereunder, and fails to cure such failure to perform within thirty (30) days of written notice from the non-defaulting Party, the non-defaulting Party may terminate this Agreement upon written notice to the other Party.
- 6. <u>Regulatory Plans & Approvals</u>. In furtherance of this Agreement, the Parties shall collaborate on appropriate submittals to and requests from DEQ as set forth in this paragraph; however, the County shall have no responsibility for the failure or refusal of DEQ or other governmental authority to approve such transfers.

- a. <u>City's TMDL Action Plan</u>. For purposes of annual credit transfers, the City shall include in its Chesapeake Bay TMDL Action Plan a provision for the receipt and use of TN, TP and TSS credits from the NCPCP substantially in the form set forth in <u>Attachment C</u> hereto (or such other provision as may be agreeable to the County).
- b. Exchange Compliance Plan. The County is a member of the Nutrient Exchange and a participant in its Exchange Compliance Plan previously submitted by the Nutrient Exchange to, and approved by, DEQ pursuant to the Watershed General Permit. During the next annual update of the Exchange Compliance Plan due to DEQ on or before February 1, 2021, the County shall notify the Nutrient Exchange of the credit transfer provided by this Agreement and request the Nutrient Exchange's next Exchange Compliance Plan annual update account for such transfer.
- 7. <u>Further Cooperation</u>. The Parties shall continue to cooperate with each other as reasonably necessary to confirm or bring about the transfers contemplated by this Agreement. If for any reason the County is prohibited or otherwise unable to transfer credits as provided herein, the City shall be solely responsible for otherwise meeting its TMDL and MS4 Permit obligations.
- 8. Force Majeure. The obligations of the County, including its credit transfer obligations, shall be suspended while and as long as performance is prevented or impeded by (a) strikes, disturbances, riots, fire, severe weather, acts of war, acts of terrorism, acts of God, epidemic, pandemic, government action, major technical, engineering or construction related delays, or any other cause similar or dissimilar to the forgoing that is beyond the reasonable control of and not due to the gross negligence of the County; (b) any facts or circumstances that qualify as an Extraordinary Condition within the meaning of the Water Quality Improvement Grant Agreement by and between DEQ and the County regarding nutrient removal technology installed at NCPCP; or (c) any facts or circumstances that qualify as an Upset within the meaning of the VPDES Permit Regulation, 9 VAC 25-31, or any permits issued thereunder to NCPCP. For clarity, the County assumes no obligation under this Agreement to install, upgrade, improve, or alter the operation of any of its facilities for purposes of providing credits to the City.
- 9. <u>Change in Law.</u> In the event of any material change in applicable laws or regulations, the Parties shall work together to attempt to amend this Agreement to conform to such change, while maintaining as closely as practicable the provisions and intent of this Agreement.
- 10. <u>No Third-Party Beneficiaries</u>. This Agreement is solely for the benefit of the Parties hereto and their permitted successors and assigns and shall not confer any rights or benefits on any other person or entity.
- 11. <u>No Assignment</u>. No Party may transfer or assign this Agreement, or its rights or obligations hereunder, without the prior written consent of the other Party, which consent shall not be unreasonably withheld.
- 12. <u>Expenses; Commissions</u>. Each Party shall pay its own fees and expenses, including its own counsel fees, incurred in connection with this Agreement or any transaction contemplated

hereby, except that within thirty (30) days of the date of an invoice issued by the County the City shall reimburse the County's counsel fees for developing this agreement in an amount not to exceed ten thousand dollars (\$10,000) by check made payable to the County.

- 13. Governing Law; Venue; Severability. This Agreement is a Virginia contract that shall be construed in accordance with and governed for all purposes by the laws of the Commonwealth of Virginia. This Agreement is deemed executed and accepted in Fairfax County and all questions with respect to any of its provisions shall be instituted, maintained, and contested in a court of competent jurisdiction in Fairfax County. If any word or provision of this Agreement as applied to any Party or to any circumstance is adjudged by a court to be invalid or unenforceable, the same shall in no way affect any other circumstance or the validity or enforceability of any other word or provision.
- 14. <u>No Waiver</u>. Neither any failure to exercise or any delay in exercising any right, power or privilege under this Agreement by either Party shall operate as a waiver, nor shall any single or partial exercise of any right, power or privilege hereunder preclude the exercise of any other right, power or privilege. No waiver of any breach of any provision shall be deemed to be a waiver of any preceding or succeeding breach of the same or any other provision, nor shall any waiver be implied from any course of dealing.
- 15. <u>Entire Agreement</u>; <u>Amendments</u>. This Agreement contains the entire agreement between the Parties as to the subject matter hereof and supersedes all previous written and oral negotiations, commitments, proposals and writings. No amendments may be made to this Agreement except by a writing signed by both Parties.
- 16. <u>Counterparts</u>; <u>Signatures</u>; <u>Copies</u>. This Agreement may be executed in counterparts, both of which shall be deemed an original, but all of which together shall constitute one and the same instrument. A facsimile or scanned signature may substitute for and have the same legal effect as an original signature. Any copy of this executed Agreement made by photocopy, facsimile or scanner shall be considered the original for all purposes.
- 17. Authorization. Each Party represents that its execution, delivery and performance under this Agreement have been duly authorized by all necessary action on its behalf, and do not and will not violate any provision of its enabling legislation, charter, ordinances, articles of incorporation, bylaws, or regulations, as applicable, or result in a material breach of or constitute a material default under any agreement, indenture, or instrument of which it is a party or by which it or its properties may be bound or affected. To each Party's knowledge there are no actions, suits or proceedings, pending or threatened against such Party or any of its properties, before any court or governmental authority that, if determined adversely to such Party, would have a material adverse effect on the transactions contemplated by this Agreement.

IN WITNESS WHEREOF, the Parties hereto have caused the execution of this Agreement as of the date first written above.

[SIGNATURES BEGIN ON FOLLOWING PAGE]

SIGNATURE PAGE OF WATER QUALITY CREDIT AGREEMENT FOR CHESAPEAKE BAY IMPLEMENTATION BY AND BETWEEN THE COUNTY OF FAIRFAX AND THE CITY OF FAIRFAX

COUNTY OF FAIRFAX, VIRGINIA

By:

Bryan J. Hill County Executive

APPROVED AS TO FORM:

6

SIGNATURE PAGE OF WATER QUALITY CREDIT AGREEMENT FOR CHESAPEAKE BAY IMPLEMENTATION BY AND BETWEEN THE COUNTY OF FAIRFAX AND THE CITY OF FAIRFAX

CITY OF FAIRFAX, VIRGINIA

By

Robert A. Stalzer City Manager

ATTEST:

City Clerk

APPROVED AS TO FORM:

City Attorney

WATER QUALITY CREDIT AGREEMENT FOR CHESAPEAKE BAY TMDL IMPLEMENTATION ATTACHMENT A

CITY'S REQUIRED CREDIT SCHEDULE FOR MS4 PERMIT COMPLIANCE

	Water Quality	Credits (lbs/yr)	
Pollutant Parameter	2 nd Permit Cycle	3 rd Permit Cycle	Total Both Cycles
TN	1,499.71	2,249.57	3,749.28
TP	188.53	282.80	471.33
TSS	159,771.39	239,657.09	399,428.48

CREDIT AGREEMENT FOR CHESAPEAKE BAY TMDL IMPLEMENTATION ATTACHMENT B

WATER QUALITY CREDIT TRANSFER FORM

<u>Instructions</u>: This form is to be completed and executed by the County and delivered to the City on or before each May 20 immediately following the calendar year of credit generation by the County.

By execution and delivery of this Water Quality Credit Transfer Form, the following water quality credits, in the amounts specified below, are hereby transferred in accordance with, and for the specific and limited purposes of, the Water Quality Credit Agreement for Chesapeake Bay TMDL Implementation by and between the County of Fairfax and the City of Fairfax.

Transferor:	County of Fairfax Noman M. Cole, Jr., Pollution Control Plant
Transferee:	City of Fairfax Municipal Separate Storm Sewer System
TN Credit Quantity:	lbs
TP Credit Quantity:	lbs
TSS Credit Quantity:	lbs
Year Generated:	
Date Transferred:	
Signed (for the County):	
Name (Print):	
Title:	

WATER QUALITY CREDIT AGREEMENT FOR CHESAPEAKE BAY TMDL IMPLEMENTATION ATTACHMENT C

MS4 CHESAPEAKE BAY TMDL ACTION PLAN PROVISION FOR USE OF FAIRFAX COUNTY NCPCP-GENERATED WATER QUALITY CREDITS

This plan includes the generation and use of TN, TP and TSS water quality credits pursuant to the Water Quality Credit Agreement for Chesapeake Bay TMDL Implementation to which the City of Fairfax and the County of Fairfax are signatories and pursuant to any other water quality credit exchange the City may secure in accordance with applicable laws and regulations. This compliance method is in lieu of exclusive reliance on more traditional stormwater retrofit projects, which may not be feasible to execute on a condensed 10-year schedule (i.e., Second and Third Bay TMDL Permit Cycles). Not only does incorporation of this method have the advantage of more reliably meeting the MS4 Permit's short deadlines, but it is also beneficial to the public in that it will help meet the City's Chesapeake Bay TMDL reduction goals more cost-effectively than otherwise possible. This component of the plan is fully in accordance with Virginia Code §62.1-44.19:21 (TN and TP) and §62.1-44.19:21.1 (TSS).



Appendix B. Updated Land Cover Analysis

1001 Boulders Parkway Suite 300 Richmond, VA 23225 P 804.200.6500 F 804.560.1016 www.timmons.com

MEMORANDUM

TO: Satoshi Eto

FROM: Sheila Reeves, PE, CFM

DATE: 12/3/2021

RE: Updated Land Cover Analysis

Timmons has completed a land cover analysis to identify forested areas within the existing City of Fairfax MS4 regulated area as of June 30, 2009. The intent of this evaluation is to refine the land cover totals used to calculate the pollutant source loading for the Chesapeake TMDL Pollutants of Concern (POC). To perform this task, TG analyzed GIS datasets including VGIN land cover (2011) and 2009 aerial photography downloaded from the from Fairfax County website: https://www.fairfaxcounty.gov/nadar/services/AerialPhotography/2009AerialPhotography/ImageServer. City staff subsequently field verified the areas delineated as forested in the 2021 re-evaluation to verify that the forested areas have an unmanaged understory. Areas that were noted by City staff as having managed understories were recategorized as managed turf. A summary of the final land cover recategorization developed as part of this task is provided in Figure 1.

Lai	nd Cover	Accounting	3
	2015	Bertend	Ch
	Table	Revised	Change
	(acres)	2021 (Acres)	(Acres)
Impervious	1,549	1,570	21
Pervious	2,166	2,046	(121)
Forested	244	343	99
Open Water	4	4	-
TOTAL	3,963	3,963	

Figure 1. Summary of Land Cover Categorization Changes

Timmons has prepared updated POC Source loading calculations using the refined land cover analysis for 2009 land cover. It was determined that this exercise to refine the 2009 land cover categorization **removes 855-lb TN and 15-lb TP** from the TMDL POC Source Loading calculations. The increase in impervious cover results in a **3,829-lb increase in TSS** to the TMDL POC Source Loading calculations, see Figure 2.

P	OC Loading	:	Original 2015 Action Plan	Revised 2021 Action Plan	*Original	*Revised	
		EOS Loading	Estimated Total	Estimated Total	2015 Action	2021 Action	Change in
Subsource	Pollutant	Rate (lbs/ac/yr)	POC Load	POC Load	Plan	Plan	POC Load
Regulated Urban Impervious		16.86	26,111.76	26,472.48	47,928	47,072	(855)
Regulated Urban Pervious		10.07	21,816.05	20,599.90			
Regulated Urban Impervious	Phosphorus	1.62	2,508.96	2,543.62	3,397	3,382	(15)
Regulated Urban Pervious	·	0.41	888.24	838.72	0,007	5,562	(23)
Regulated Urban Impervious		1171.32	1,814,070.14	1,839,130.53	2,194,930	2,198,759	3,829
Regulated Urban Pervious		175.8	380,860.15	359,628.79	2,194,930	2,198,739	3,629
		*Does	not include load fro	om "New Sources" a	ns determined ir	n Table 5 of the 2	015 Action Plan

Figure 2. POC Source Loading Calculation Comparison

Next Steps:

City staff will need to update Table 1 of the City's Chesapeake Bay Action Plan (which is MS4 Permit Table 3b) with the refined land cover acreage for Pervious and Impervious Cover shown Figure 1 of this memo in the "Revised 2021" column. Subsequently, Table 2 and Table 3 of the Action Plan will also need to be updated to reflect revised TMDL POC Reduction Requirements.



Appendix C. Daniels Run Stream Restoration Calculations

DANIELS RUN STREAM RESTORATION

FINAL DESIGN PLAN CITY OF FAIRFAX, VIRGINIA

OWNER/APPLICANT:

CITY OF FAIRFAX C/O MS. CHRISTINA ALEXANDER 10455 ARMSTRONG STREET ROOM 200 FAIRFAX, VIRGINIA 22030

ENGINEER:

FRANK R. GRAZIANO, P.E.
WETLAND STUDIES AND SOLUTIONS, INC.
5300 WELLINGTON BRANCH DRIVE
SUITE 100
GAINESVILLE, VIRGINIA 20155

SITE NOTES:

TAX MAP PARCELS: 57-2-02-182

PARCEL ADDRESS: 3705 OLD LEE HIGHWAY FAIRFAX, VIRGINIA 22031

PARCEL AREA: 13.7 ACRES
DISTURBED AREA: 1.4 ACRES

VICINITY MAP



SOILS MAP



SHEET INDEX

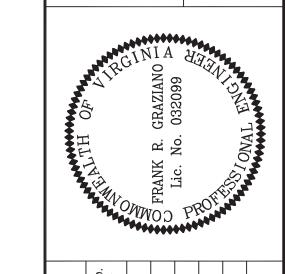
SHEET 1	COVER SHEET
SHEET 2	OVERALL SITE EXHIBIT
SHEET 3	GRADING PLAN & LONGITUDINAL PROFILE
SHEET 4	SEDIMENT SIZING, REINFORCED BED MIXTURE
	SPECIFICATIONS, CONSTRUCTION TOLERANCES,
	GRADING NOTES, & SEQUENCE OF CONSTRUCTION
SHEET 5-6	CONSTRUCTION DETAILS
SHEET 7	EROSION & SEDIMENT CONTROL PLAN
SHEET 8	EROSION & SEDIMENT CONTROL DETAILS
SHEET 9	EROSION & SEDIMENT CONTROL NARRATIVE
SHEET 10	GEOMETRY PLAN & STRUCTURE STAKEOUT
SHEET 11	PLANTING PLAN
SHEET 12	VEGETATION SCHEDULE
SHEET 13	PLANTING NOTES & DETAILS
SHEET 14	EXISTING CONDITIONS PLAN
SHEET 15	TREE PRESERVATION PLAN
SHEET 16	DESIGN NARRATIVE
SHEET 17	100-YEAR FLOODPLAIN ANALYSIS
SHEET 18	100-YEAR FLOODPLAIN ANALYSIS - CROSS SECTIONS
SHEET 19	WATER QUALITY IMPACT ASSESSMENT

Table 8. Daniels Run Stream Restoration POC Credits

Table V.J.1 -	Urban Stream Restoration Interim Approve	d Removal I	Rates	
BMPs	How Credited	TN	TP	TSS
Stream Restoration	Mass reduction/length (lbs./linear ft.)	0.075	0.068	44.88
City	of Fairfax - Daniels Run Stream Restoration	Project		
Linear ft. of Stream Restoration	DOC Demoved essentided (the Averal)	TN	TP	TSS
765	POC Removal provided (lbs./year)	57.38	52.02	34333.20

Daniels Run is located behind Daniels Run Elementary School, within the City of Fairfax. The Latitude and Longitudinal coordinates of the project are 38"51'5.74"N; 77"17'37.98"W respectively, and the overall construction cost for the project was \$563,000.00.

ZƏM	CODOROS SILT LOAIVI	PUUK-F, VV, D	FOON, F, VV	LOVV	"
30A	CODORUS & HATBORO	POOR-F, W, B	POOR, F, W	LOW	III
102	WHEATON LOAM	GOOD	FAIR - S	HIGH	IVB
Source: Fairfa	ax County Digital Data				Scale: 1" = 500'



	Ap By				
	Rev. App				
REVISIONS					SCALE: AS NOTED
REV	No. Date Description				DATE: JANUARY 2015
	Date				IE: JAN
	No.				DAT
	. 1.7	-		 	

Horizontal Datum: VCS NAD 83

Vertical Datum: NGVD 29

Boundary and Topo Source:
WSSI and City of Fairfax Digital Data

Design Draft Approved

SDD ADE EDG

Sheet # 1 of 19

Computer File Name:
L\22000s\22300\22338.02\CADD\04-ENGR\10-Final Planset
COVER SHEET.dwg

RESPONSIBLE LAND DISTURBER
NAME: FRANK R. GRAZIANO, P.E.
CERTIFICATION No: PROFESSIONAL
ENGINEER #032099
EXPIRATION DATE: 2/29/2016
CONTACT PHONE NO: (703) 679-5600



Appendix D. City Hall Pond Retrofit Calculations

CONSTRUCTION PLANS CITY HALL POND RETROFIT

SP-22-00507 PIN #: 57 4 02 013 A 10455 ARMSTRONG STREET CITY OF FAIRFAX, VIRGINIA 22030

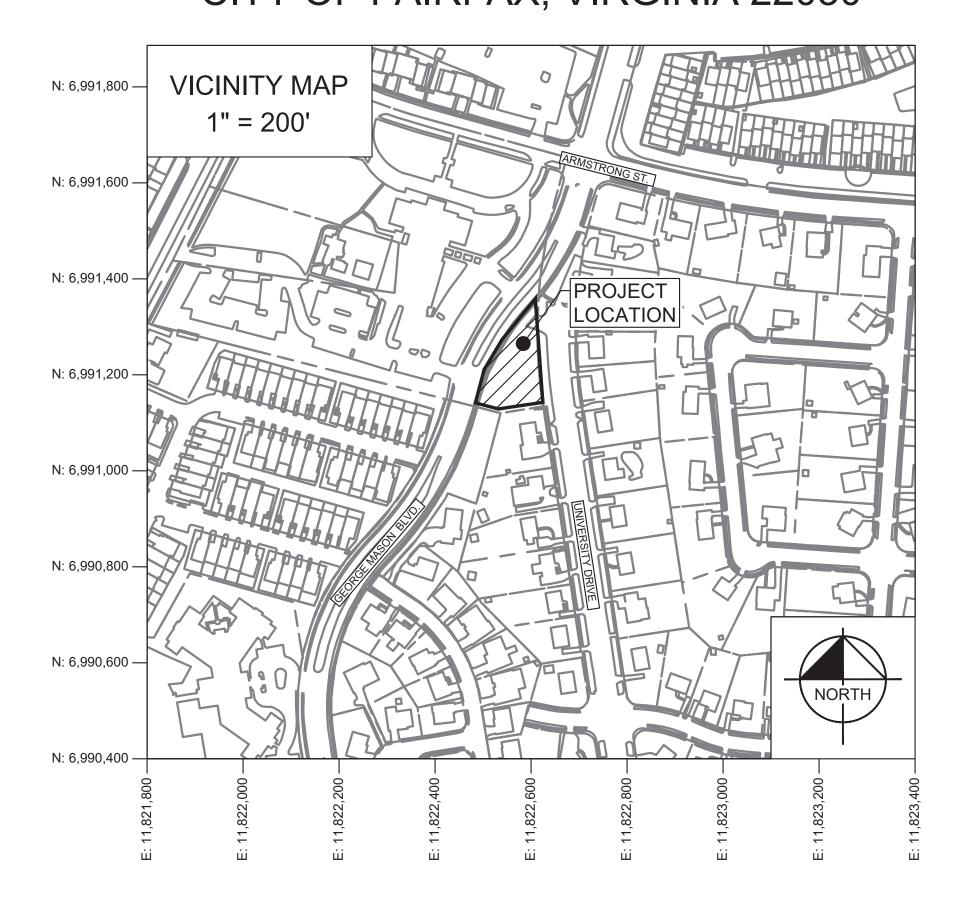
PROJECT NARRATIVE

THIS PROJECT CONSISTS OF THE MAINTENANCE, ENHANCEMENT, AND RETROFIT OF THE STORMWATER MANAGEMENT POND LOCATED AT 10455 ARMSTRONG STREET (CITY HALL POND). THE POND DRAINS APPROXIMATELY 3.49 ACRES FROM GEORGE MASON BOULEVARD AND ADJACENT NEIGHBORHOODS. THE POND RETROFIT PROJECT INCLUDES INSTALLATION OF A SEDIMENT FOREBAY AND INCREASE IN POND TREATMENT VOLUME. AS PART OF THE DESIGN, A VEGETATIVE BENCH HAS BEEN INCLUDED AND SINUOSITY HAS BEEN ADDED TO THE POND FLOOR TO INCREASE STORMWATER HYDRAULIC RESIDENCE TIME. THE ADDITION OF THE FOREBAY WILL PROVIDE A MAINTENANCE FEATURE FOR THE FACILITY THAT WILL ALLOW FOR EASE OF MAINTENANCE AFTER IMPLEMENTATION. THE POLLUTANT OF CONCERN (POC) CREDITS GENERATED FROM THE THE RETROFIT OF THIS POND WILL BE APPLIED TO THE THE CITY'S CHESAPEAKE BAY TMDL REDUCTION REQUIREMENTS. THE RETROFIT OF THIS POND WILL GENERATE 1130.94 LBS./YR. OF TOTAL SUSPENDED SOLIDS (TSS), 7.36 LBS./YR. OF NITROGEN, AND .40 LBS./YR. OF PHOSPHORUS. ALL CREDITING WAS PERFORMED IN ACCORDANCE WITH GUIDANCE MEMO NO. 20-2003 TITLED "CHESAPEAKE BAY TMDL SPECIAL CONDITION GUIDANCE" DATED FEBRUARY 6, 2021.

GENERAL NOTES

- . THE SUBJECT PROPERTY OF THIS PLAN IS THE FOLLOWING:
- 1.1. TAX MAP NUMBER: 57 4 02 013 A
- 1.2. PARCEL AREA: 8.26 ACRES (359,805.60 SF)
- I.3. DEED BOOK AND NUMBER: DB 1808, PG 166
- 4. ESTIMATED DISTURBED AREA: 0.45 AC
- TOPOGRAPHIC INFORMATION SHOWN IS BASED ON GROUND SURVEYS PREPARED BY RICE ASSOCIATES ON JUNE, 2021. THE HORIZONTAL DATUM IS NAD83 WHILE THE VERTICAL DATUM IS NAVD88. THE GROUND SURVEYS HAVE BEEN SUPPLEMENTED WITH THE BEST AVAILABLE DATA FROM THE CITY OF FAIRFAX GEOGRAPHIC INFORMATION SYSTEM. NOTE: KIMLEY-HORN PERFORMED A VERTICAL DATUM CONVERSION ON APRIL 11, 2022 TO CONVERT THE ORIGINAL RICE ASSOCIATES SURVEY FROM NAVD88 TO NGVD29. AN ELEVATION ADJUSTMENT OF 0.78 FEET WAS APPLIED TO ALL POINT AND ELEVATION DATA THROUGHOUT THIS PLAN SET. THE DATUM SHIFT WAS PERFORMED USING THE NOAA "ORTHOMETRIC HEIGHT CONVERSION" TOOL.
- THE EXISTING UTILITIES, AS SHOWN HEREON, ARE APPROXIMATE ONLY. NO GUARANTEE IS HEREIN MADE OR IMPLIED THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT ALL UTILITY COMPANIES AND TO VERIFY THE TYPE, SIZE, AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO STARTING THE WORK. ANY DISCREPANCIES IN OR FROM THE INFORMATION SHOWN HEREON SHALL BE REPORTED TO KIMLEY-HORN AND ASSOCIATES..
- CONTRACTORS SHALL NOTIFY OPERATORS WHO MAINTAIN UNDERGROUND UTILITY LINES IN THE AREA OF PROPOSED EXCAVATION AND/OR BLASTING AT LEAST TWO WORKING DAYS, BUT NOT MORE THAN 10 WORKING DAYS PRIOR TO COMMENCEMENT OF EXCAVATION OR DEMOLITION.
- 5. APPROVAL OF THESE PLANS IN NO WAY RELIEVES THE CONTRACTOR OF ALL APPLICABLE FEDERAL, STATE, AND LOCAL ORDINANCES.
- THE AREA SHOWN HERON IS LOCATED ON THE FLOOD INSURANCE RATE MAPS (FIRM), COMMUNITY PANEL NO. 5155240005D, WITH AN EFFECTIVE DATE OF JUNE 2, 2006. FIRM PANEL NO. 5155240005D INDICATES THAT THE PROJECT AREA IS NOT LOCATED IN A FEMA SPECIAL FLOOD HAZARD AREA (SFHA).
- 7. TO THE BEST KNOWLEDGE OF THE ENGINEER, THERE ARE NO EXISTING GRAVES OR BURIAL SITES LOCATED ON THE PROPERTY. THE SUBJECT PROPERTY IS NOT LISTED UNDER THE NATIONAL REGISTER OF HISTORICAL PLACES.
- TO THE BEST KNOWLEDGE OF THE ENGINEER, THIS SITE PLAN CONFORMS TO ALL APPLICABLE ORDINANCES, REGULATIONS AND ADOPTED STANDARDS, UNLESS OTHERWISE SPECIFICALLY NOTED.
- 9. TO THE BEST KNOWLEDGE OF THE ENGINEER, THERE ARE NO WETLANDS ON THIS SITE.
- 10. THERE ARE NO RESOURCE PROTECTION AREAS (RPA's) ON THE SUBJECT PROPERTY.

	OWNER	CLIENT	ENGINEER
NAME	CITY OF FAIRFAX	CITY OF FAIRFAX	KIMLEY-HORN
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO, P.E.
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589



AGENT AUTHORIZATION LETTER	City of Fairfax APPROVED SITE PLAN
To Whom IT May Concern: I/We, The City of Fairfax, the undersigned title owner(s) of the property identified below do hereby authorize, to act as my/our agent(s) in the furtherance of an application for a Major Site Plan, to act as my/our agent(s) in the furtherance of an application for a Major Site Plan, on my/our property located at: 10455 Armstrong Street in Fairfax, Virginia 22030 Tax Map No: 5 4 02 013 A Thank you in advance for your cooperation. Date: By:	Zoning Official Date Review approval by:
ALL TITLE OWNERS MUST SIGN IN PRESENCE OF NOTARY. IF THERE IS MORE THAN ON OWNER, FILL OUT MULTIPLE APPLICATIONS	Wastewater ReviewerGIS ManagerBonding AdministratorDate

	Sheet List Table
Sheet Number	Sheet Title
01	COVER SHEET
02	NOTES AND DETAILS - 1
03	NOTES AND DETAILS - 2
04	EXISTING CONDITIONS
05	PHOTOSTATION LOCATION MAP
06	PHOTOSTATION LOCATION - PHOTOS
07	DEMOLITION AND ACCESS PLAN
08	EROSION AND SEDIMENT CONTROL PLAN - PHASE I
09	EROSION AND SEDIMENT CONTROL PLAN - PHASE II
10	EROSION AND SEDIMENT CONTROL - NOTES
11	EROSION AND SEDIMENT CONTROL - DETAILS I
12	EROSION AND SEDIMENT CONTROL - DETAILS II
13	POND HYDROLOGY
14	PROPOSED POND RETROFIT LAYOUT & GRADING
15	PROPOSED POND ROUTING & HYDRAULIC ANALYSIS
16	STORMWATER MANAGEMENT NOTES & CREDITING
17	PLANTING PLAN
18	PLANTING NOTES & DETAILS
19	BMP MAINTENANCE
20	HISTORICAL PLANS - 1
21	HISTORICAL PLANS - 2
22	HISTORICAL PLANS - 3
23	HISTORICAL PLANS - 4
24	HISTORICAL PLANS - 5
25	HISTORICAL PLANS - 6

	CITY OF FA		
The following affidavit and check	clist must be printed on the cover page ar	d signed by a certified engineer, architect or land surveyor.	
I Jon D'Alessandro the attached site plan that is requi	Certification for Complet do hereby certify that this site pla red pursuant to Section 110-6.8 in the Co	n checklist is complete and accurate for use in staff's evalua-	ation c
(signature)	(date)	(SEAL)	





JONATHAN JOSEPH
D'ALESSANDRO
Lic No. 052336
05/09/2022

_	FROM CITY OF FAIRFAX	08/07/2022	KH
No.	REVISIONS	DATE	ВУ

© 2021 KIMLEY—HORN AND ASSOCIATES, INC.
11400 COMMERCE PARK DR., SUITE 400, RESTON, VA 2019
PHONE: 703-674-1300 FAX: 703-674-1350
WWW.KIMLEY-HORN.COM

DATE
08/25/2022
SCALE AS SHOWN
DESIGNED BY J.J.D
DRAWN BY J.A.C

ITY HALL POND RETROFI
PREPARED FOR

pelow.
sheet number
ore you dig.

PROPERTY INFORMATION

- TAX REFERENCE NUMBER: 57 4
- 2. PROPERTY PARCEL NUMBER: 57 4 02 013 A
- 3. ADDRESS: 10455 ARMSTRONG STREET FAIRFAX, VA 22030
- 4. GEOGRAPHIC COORDINATES: LATITUDE 38.841025, LONGITUDE -77.308268

PROPERTY OWNER INFORMATION

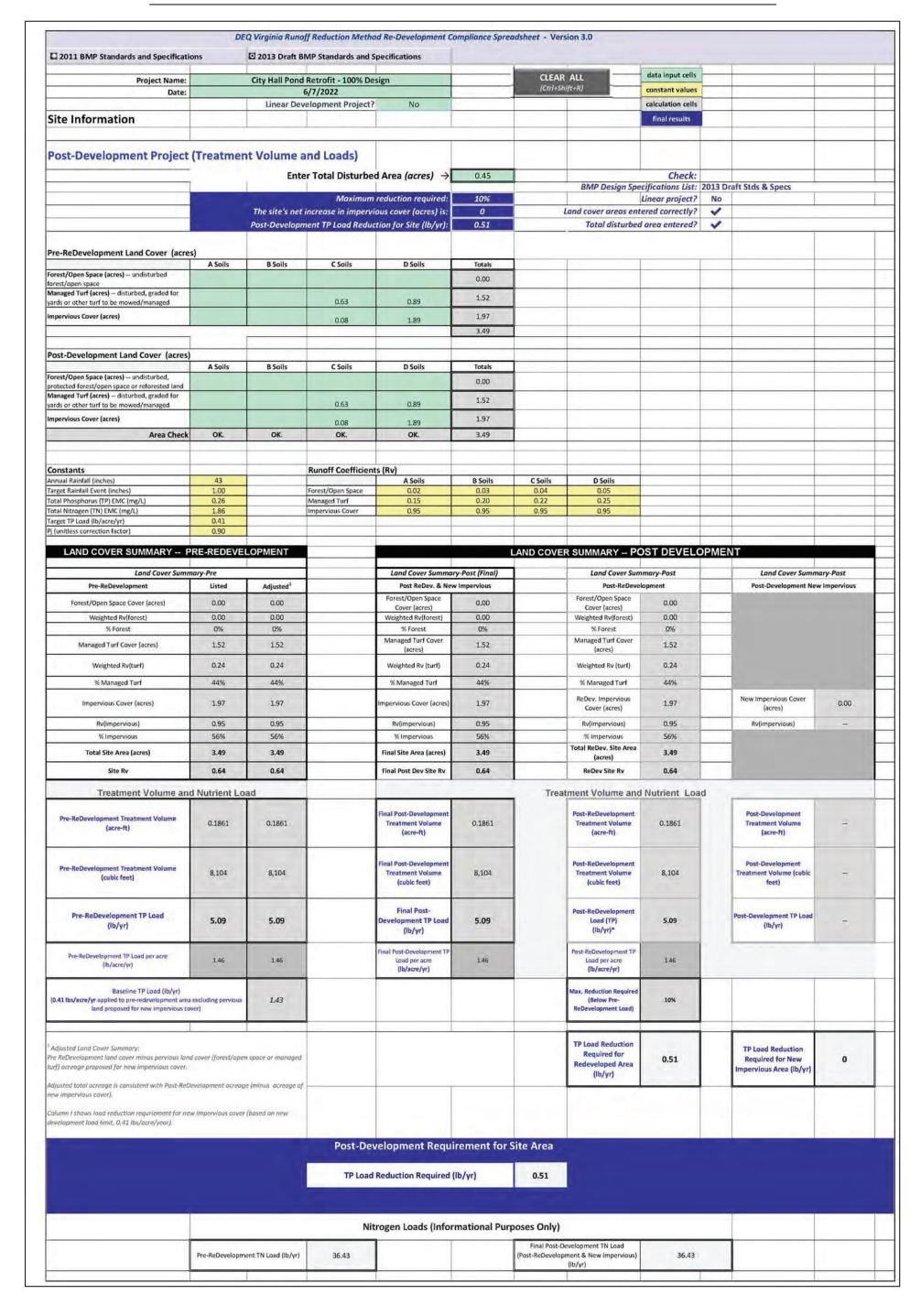
- 1. NAME: CITY OF FAIRFAX
- 2. ADDRESS: 10455 ARMSTRONG STREET FAIRFAX, VA 22030
- 3. TELEPHONE NUMBER: 703-385-7810

THIS PROJECT CONSISTS OF THE MAINTENANCE, ENHANCEMENT, AND RETROFIT OF THE STORMWATER MANAGEMENT POND LOCATED AT 10455 ARMSTRONG STREET (CITY HALL POND). THE POND DRAINS APPROXIMATELY 3.49 ACRES FROM GEORGE MASON BOULEVARD AND ADJACENT NEIGHBORHOODS. THE POND RETROFIT PROJECT INCLUDES INSTALLATION OF A SEDIMENT FOREBAY AND INCREASE IN POND TREATMENT VOLUME. AS PART OF THE DESIGN, A VEGETATIVE BENCH HAS BEEN INCLUDED AND SINUOSITY HAS BEEN ADDED TO THE POND FLOOR TO INCREASE STORMWATER HYDRAULIC RESIDENCE TIME. THE ADDITION OF THE FOREBAY WILL PROVIDE A MAINTENANCE FEATURE FOR THE FACILITY THAT WILL ALLOW FOR EASE OF MAINTENANCE AFTER IMPLEMENTATION. THE PROPOSED STORMWATER MANAGEMENT FACILITY WILL BE MAINTAINED THROUGH THE CITY OF FAIRFAX'S PUBLIC BMP MAINTENANCE PROGRAM.

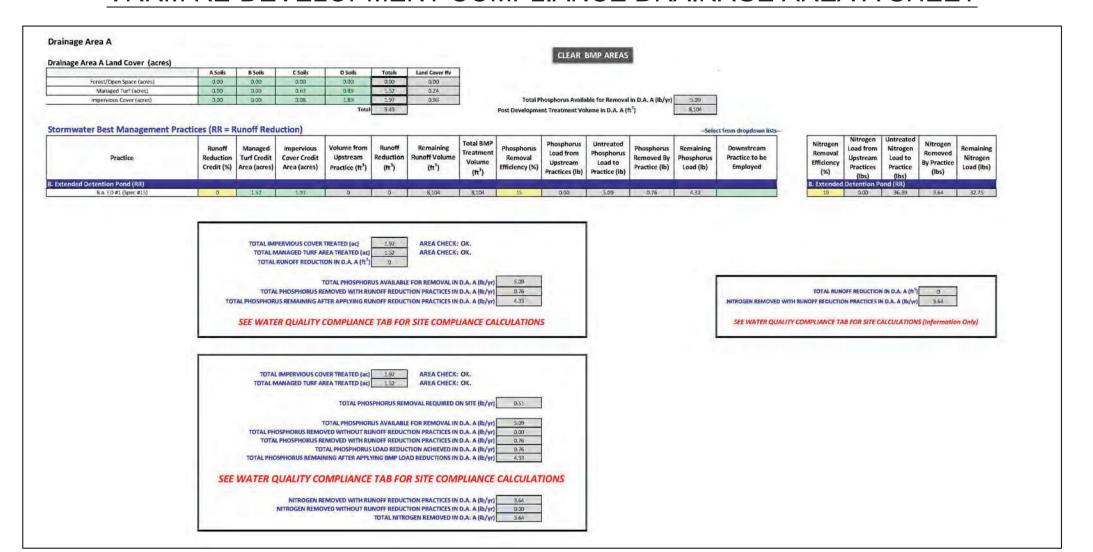
NO MODIFICATIONS WILL BE MADE TO THE EXISTING STORM SEWER INFRASTRUCTURE ON SITE AND NO ADDITIONAL STORMWATER INFLOWS WILL BE ADDED TO THE STORMWATER MANAGEMENT FACILITY. THERE IS ONE (1) EXISTING 18" RCP INFLOW PIPE THAT DISCHARGES INTO THE FACILITY. FLOW ATTENUATION IS PROVIDED BY A 48" DIAMETER RISER STANDPIPE WITH A 1.5" DIAMETER ORIFICE PLATE AND AN 18" PRINCIPAL SPILLWAY PIPE. THE PRINCIPAL SPILLWAY PIPE TIES THE STORMWATER MANAGEMENT FACILITY BACK INTO THE CITY'S MS4 THROUGH A 36" RCP.

CITY HALL POND DISCHARGES THROUGH A SERIES OF PIPES, TO DANIELS RUN WHICH IS A MAIN TRIBUTARY OF ACCOTINK CREEK. ACCOTINK CREEK HAS A BENTHIC (SEDIMENT), CHLORIDE, AND FECAL COLIFORM TMDL. THE RETROFIT OF THIS FACILITY WILL NOT ONLY PROVIDE THE CHESAPEAKE BAY TMDL CREDIT FOR THE CITY, BUT WILL ALSO HELP ADDRESS THE CITY'S LOCAL TMDL REQUIREMENTS FOR SEDIMENT IMPAIRMENTS IN ACCOTINK CREEK.

VRRM RE-DEVELOPMENT COMPLIANCE SITE SHEET



VRRM RE-DEVELOPMENT COMPLIANCE DRAINAGE AREA A SHEET



CITY HALL POND RETROFIT CHESAPEAKE BAY TMDL POLLUTANT OF CONCERN (POC) - REDUCTION CALCULATIONS

Methodology used was obtained from t		•	
TMDL Special Condition	<i>n Guidance</i> , dated November	12, 2020.	
BMP Retrofit Type:	BMP Enhancement		
BMP Treatment Practice:	Dry Detention Pond		
Note: Classification obtained from Tab	ole V.C.1 - Chesapeake Bay Pro	ogram BMPs, Established	
	Efficiencies		
	age Basin Information		
Drainage Basin = Ni+	Potomac River Basin rogen Loading Rate	-	
Regulate Impervious =	16.86	lbs/ac/yr	
Regulate Pervious =	10.07	lbs/ac/yr	
	sphorus Loading Rate	1.00/ 0.0/ /.	
Regulate Impervious =	1.62	lbs/ac/yr	
Regulate Pervious =	0.41	lbs/ac/yr	
Total Sus	pend Solids Loading Rate		
Regulate Impervious =	1,171.32	lbs/ac/yr	
Regulate Pervious =	175.8	lbs/ac/yr	
Note: Loading rates obtained from Tab		rative Code (9VAC25-890	
	0) General Permit		
	ninage Basin Information		
Total Drainage Area =	3.49 1.56	ac	
Impervious = Pervious =	1.93	ac ac	
	Load In The BMP Drainage Bas		
Nitrogen =	45.74	lbs/yr	
Phosphorus =	3.32	lbs/yr	
Total Suspend Solids =	2,166.55	lbs/yr	
Exi	sting BMP Effiency		
Nitrogen =	5	%	
Phosphorus =	10	%	
Total Suspend Solids =	10	%	
Note: Efficiencies obtained from Tabl	le V.C.1 - Chesapeake Bay Pro	gram BMPs, Established	
	ies (Dry Detention Pond)		
	MP Effiency Modification		
Missing Forebay=	10	%	
Missing Micropool =	10	%	
Missing Length/Width = Total =	2 22	% %	
	d Existing BMP Effiency	/0	
Nitrogen =	3.9	%	
Phosphorus =	7.8	%	
Total Suspend Solids =	7.8	%	
Pro	posed BMP Effiency	•	
Nitrogen =	20	%	
Phosphorus =	20	%	
Total Suspend Solids =	60	%	
Note: Efficiencies obtained from Tabl	le V.C.1 - Chesaneake Bay Pro	gram BMPs. Established	
	Ory Extended Detention Pond		
(2	, 222	,	
ВМЕ	P Effiency Difference		
Nitrogen =	16.1	%	
Phosphorus =	12.2	%	
Total Suspend Solids =	52.2	%	
Final P	Polutant Load Recution		
Nitrogen =	7.36	lbs/yr	
		lbs/vr	

0.40

1130.94

|Phosphorus =

Total Suspend Solids =

SHEET NUMBER

lbs/yr

lbs/yr



Appendix E. Lion Run Outfall Restoration POC Reduction Calculations

100% CONSTRUCTION PLANS LION RUN SITE OUTFALL AND GULLY STABILIZATION PROJECT

PIN#: 48 3 02 020 & 58 1 02 003 3501 LION RUN CITY OF FAIRFAX, VIRGINIA

VICINITY MAP

PROJECT NARRATIVE

THIS PROJECT CONSISTS OF THE STABILIZATION OF A

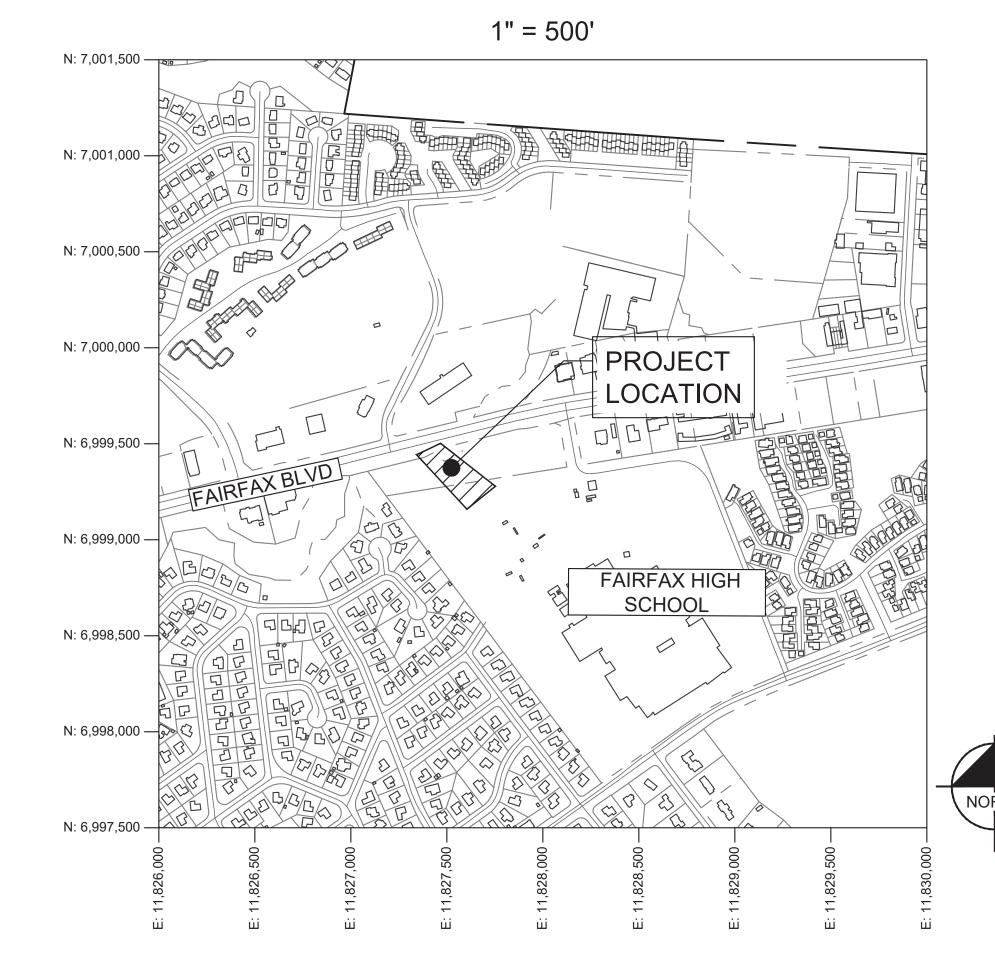
THIS PROJECT CONSISTS OF THE STABILIZATION OF APPROXIMATELY 375 LINEAR FEET OF AN ACTIVELY ERODING OUTFALL CHANNEL. THE PROJECT LIMITS BEGIN AT THE DISCHARGE OF A 60" RCP PIPE AND END AT THE CONFLUENCE OF ACCOTINK CREEK. THE PROJECT IS LOCATED IN THE VICINITY OF FAIRFAX HIGH SCHOOL IN THE CITY OF FAIRFAX, VIRGINIA. THE LIMITS OF DISTURBANCE ARE 0.85 ACRES. THE POLLUTANT OF CONCERN (POC) CREDITING AND DESIGN FOR THE OUTFALL WAS DONE IN ACCORDANCE WITH THE GUIDANCE MEMO "RECOMMENDATIONS FOR CREDITING OUTFALL AND GULLY STABILIZATION PROJECTS IN THE CHESAPEAKE BAY WATERSHED", DATED OCTOBER 15, 2019. REPRESENTATIVE SOIL FIELD SAMPLES WERE OBTAINED FROM THE PROJECT SITE AND PROCEED AT A LABORATORY TO OBTAIN THE SOILS BULK DENSITY, NITROGEN CONCENTRATION, AND PHOSPHORUS CONCENTRATION. THE SOIL SAMPLE BULK DENSITY WAS 78.66 LB/FT³ AND THE CONCENTRATIONS WERE 0.66 LBS OF PHOSPHORUS PER 1 TON OF SEDIMENT AND 1.60 LBS OF NITROGEN PER 1 TON OF SEDIMENT. THE POLLUTANT OF CONCERN CREDIT REDUCTION FROM THIS PROJECT IS 45,077.02 LBS/YR OF TOTAL SUSPENDED SOLIDS (TSS), 36.06 LBS/YR OF NITROGEN. AND 14.07 LBS/YR OF PHOSPHORUS.

GENERAL NOTE

- 1. THE SUBJECT PROPERTIES OF THIS PROJECT IS TAX MAP NUMBER: 48 3 02 020 & 58 1 02 003
- 2. TOPOGRAPHIC INFORMATION SHOWN IS BASED ON GROUND SURVEYS PERFORMED BY RICE ASSOCIATES ON JULY, 2021. THE TOPOGRAPHIC INFORMATION HAS BEEN CONVERTED FROM VERTICAL DATUM NAVD88 TO NGVD29 BY KIMLEY-HORN. THE HORIZONTAL DATUM IS NAD83. THE GROUND SURVEYS HAVE BEEN SUPPLEMENTED WITH THE BEST AVAILABLE DATA FROM THE CITY OF FAIRFAX GEOGRAPHIC INFORMATION SYSTEM.
- 3. THE EXISTING UTILITIES, AS SHOWN HEREON, ARE APPROXIMATE ONLY. NO GUARANTEE IS HEREIN MADE OR IMPLIED THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT ALL UTILITY COMPANIES AND TO VERIFY THE TYPE, SIZE, AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO STARTING THE WORK. ANY DISCREPANCIES IN OR FROM THE INFORMATION SHOWN HEREON SHALL BE REPORTED TO KIMLEY-HORN AND ASSOCIATES..
- 4. CONTRACTORS SHALL NOTIFY OPERATORS WHO MAINTAIN UNDERGROUND UTILITY LINES IN THE AREA OF PROPOSED EXCAVATION AND/OR BLASTING AT LEAST TWO WORKING DAYS, BUT NOT MORE THAN 10 WORKING DAYS PRIOR TO COMMENCEMENT OF EXCAVATION OR DEMOLITION.
- 5. APPROVAL OF THESE PLANS IN NO WAY RELIEVES THE CONTRACTOR OF ALL APPLICABLE FEDERAL, STATE, AND LOCAL ORDINANCES.

DECLARATION OF NO IMPACT TO THE FLOODPLAIN NARRATIVE: THE DEVELOPMENT WITHIN THE FLOODPLAIN IS RELATED TO THE MAINTENANCE AND RESTORATION OF THE EXISTING MANMADE STORM SEWER OUTFALL CHANNEL. THE INTENT OF THE CHANNEL REPAIR AND RESTORATION IS TO RETURN THE ERODED RECEIVING CHANNEL TO A STABLE CONDITION AND PREVENT FUTURE EROSION. THE PROJECT EARTHWORK IS A NET CUT AND THE PROPOSED CHANGES IN THE FLOODPLAIN CROSS SECTIONAL AREA ARE ASSUMED AS NEGLIGIBLE WHEN COMPARED TO THE OVERALL FLOODPLAIN CROSS SECTIONAL AREA. THE PROPOSED CHANNEL REPAIR WILL NOT MODIFY THE EXISTING FLOODPLAIN HYDRAULICS, NOR WILL IT IMPACT OFFSITE PROPERTY OR THE EXISTING FLOODPLAIN BOUNDARY / BASE FLOOD ELEVATIONS. THERE WILL BE NO CHANGE TO PRE AND POST DEVELOPMENT FLOODPLAIN FLOWRATE AND VELOCITY ONSITE, UPSTREAM OR DOWNSTREAM WITHIN THE STREAM CORRIDOR. ALL WORK PROPOSED AS PART OF THIS CHANNEL MAINTENANCE PROJECT IS IN COMPLIANCE WITH CITY CODE SECTION 4.15.8 APPROVAL CRITERIA.

Checklist of Submittal Requirements				
Impervious surface in the floodplain:	0.17	ac.		
Area of floodplain vegetation disturbed:	0.85	ac.		
Area of floodplain land graded:	0.35	ac.		
Maximum depth of cut or fill on floodplain land:	5.21 (cut)	ft.		



	OWNER	CLIENT	ENGINEER	
NAME	CITY OF FAIRFAX SCHOOL BOARD	CITY OF FAIRFAX	KIMLEY-HORN	
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA	
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO	
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589	

	Sheet List Table				
Sheet Number	Sheet Title				
01	COVER SHEET				
02	GENERAL NOTES & DETAILS				
03	CORRESPONDENCE				
04	EXISTING CONDITIONS				
05	EXISTING CONDITIONS				
06	PHOTO LOCATION MAP				
07	EROSION & SEDIMENT CONTROL PHASE I				
08	EROSION & SEDIMENT CONTROL PHASE II				
09	EROSION & SEDIMENT CONTROL NOTES & DETAILS				
10	EROSION & SEDIMENT CONTROL NOTES & DETAILS				
11	EROSION & SEDIMENT CONTROL NOTES & DETAILS				
12	EROSION & SEDIMENT CONTROL NOTES & DETAILS				
13	EXISTING HYDROLOGY				
14	LAND COVER ANALYSIS (TR55)				
15	EXISTING CONDITIONS HYDROGRAPH				
16	POC CREDITING SUMMARY				
17	OUTFALL RESTORATION				
18	LANDSCAPING PLAN				
19	PLANTING DETAILS				
20	EXISTING TREE INVENTORY				
21	EXISTING TREE INVENTORY				





JUAN A. CAMPOS

JUAN A. CAMPOS

Lic. No. 0402061628

07/27/2022

OVENTO ON AL ENGINEERING

PUBLIC WORKS COMMENTS 06/16/2022 J.A.C PUBLIC WORKS COMMENTS 07/27/2022 J.A.C

Kimley >>> Hoff

110557012
110557012
DATE
06/15/2022
SCALE AS SHOWN
DESIGNED BY J.A.C
DRAWN BY J.A.C

GULLY RESTORATION
I RUN SITE

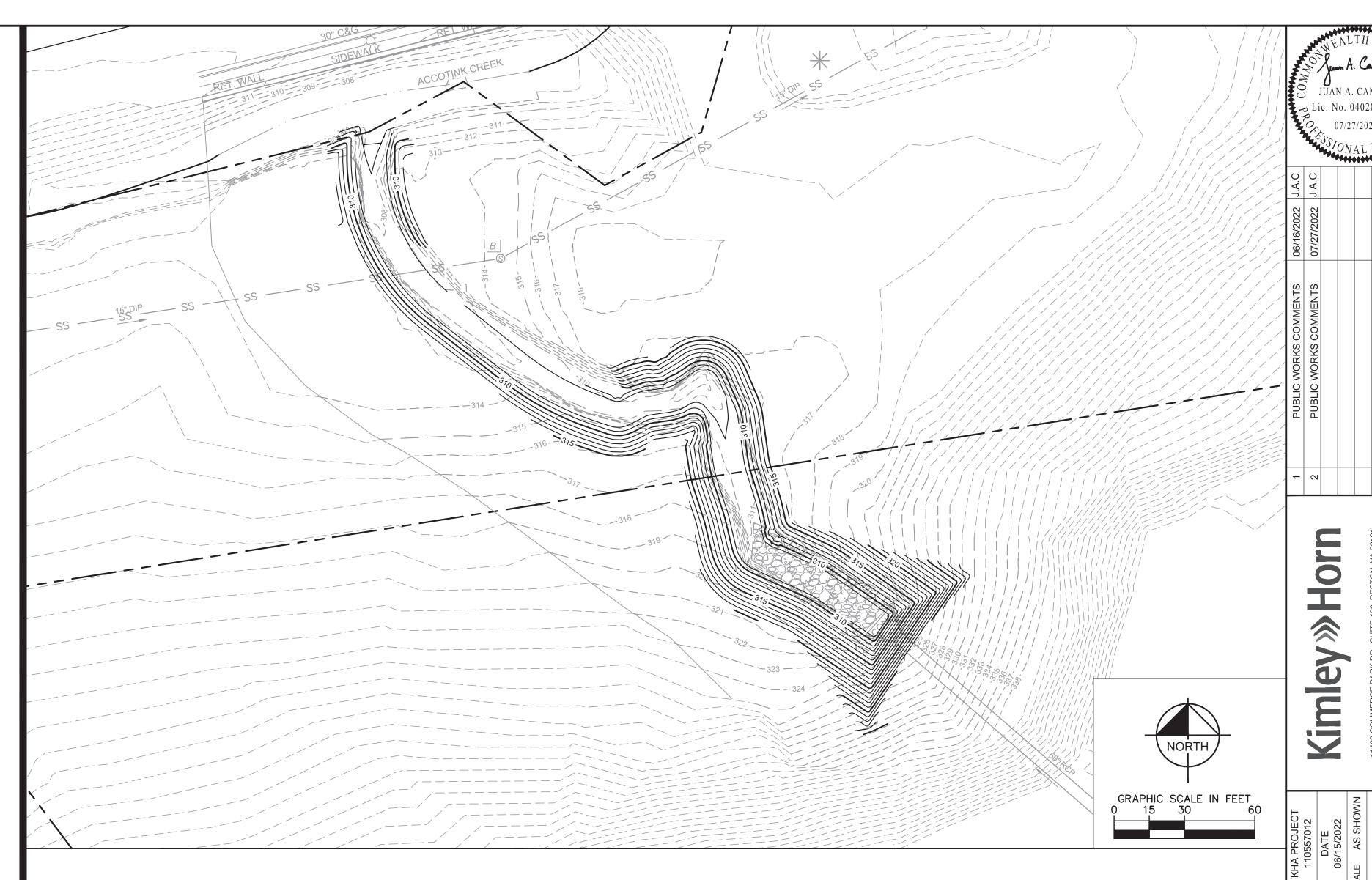
COVER SHE
OUTFALL AND GULLY I
LION RUN S

SHEET NUMBER

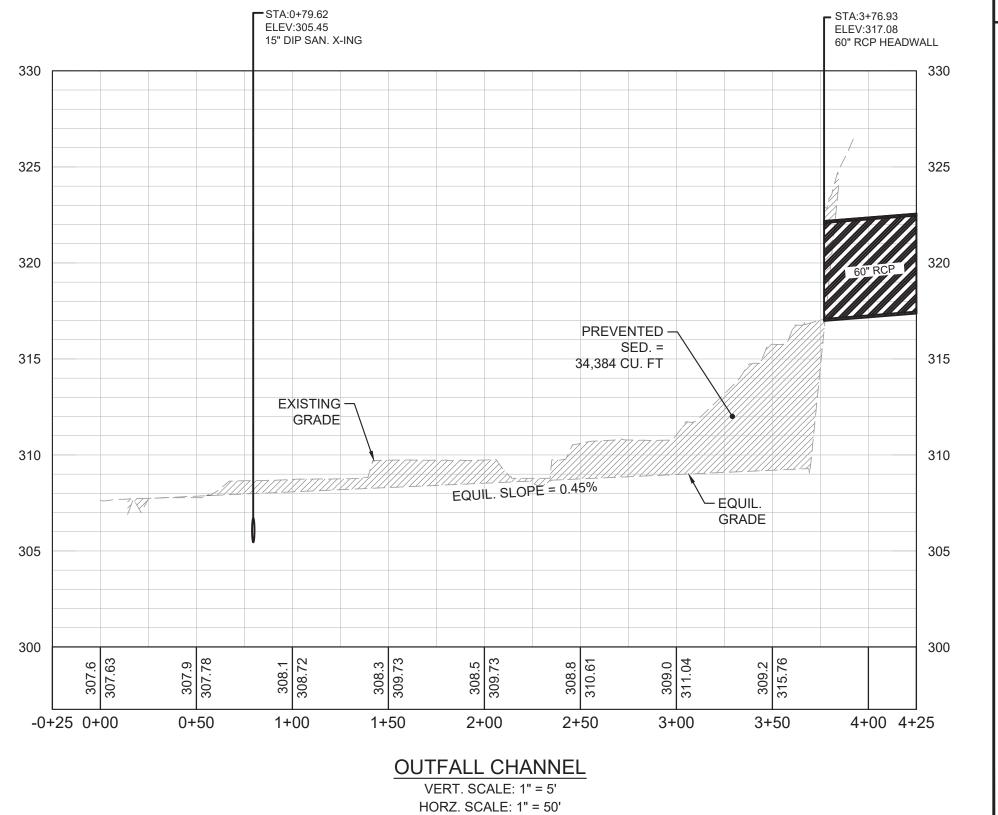
Field Data					
Bulk Density = 78.66 $lb./ft^3$					
1 ton of sediment =	0.664	lb. of (P)			
1 ton of sediment =	1.6	lb. of (N)			

Project Information				
Project Name: CITY OF FAIRFAX OUTFALL AND GULLY STABILIZATION				
Project Number: 110557012				
Date: 5/19/2022				
esign By: JJD				

Design By:	חוו	
Frieting Outfall Char	and Canditian Danamatana	
	nnel Condition Parameters	
Drainage Area (A _d)=	56.8	ас
Drainage Area (A _d)=	0.2300	km²
Mean Flow Depth =	3.500	ft
	ixisting Channel Conditions 376.930	ft
Length of Proposed Reach = Channel Slope =	0.025	ft/ft
Bank Height =	5.363	ft
Bottom Width =	9.633	ft
Top Width =	27.233	ft
Bulk Density (Estimate) =	84.278	lb./ft ³
Step 2 - Define the Equ	uilibrium Channel Conditions	
Is there a pipe outfall or other defining infrastructure site?	e present upstream of the restoration	Yes
Ups	tream Limit	
L_{ma}	_{ax} = 153A _d ^{0.6}	
Maximum Upstream Channel Length (L _{max}) =	Not Applicable	ft
	rium Bed Slope	
Choose Bed Condition =	Bed Condition 1	
Bed Condition 1 =	Cohesive Bed	
Bed Condition 2 =	Sand and Fine Grave (0.1-5mm	particle size)
Bed Condition 3 =	Beds Coarser than Sand (>5mm	particle size)
	on 1: Cohesive Bed	
$S_{eq} =$	= 0.0028A ^{-0.33}	
Equilibrium Slope (S _{eq})=	0.0045	ft/ft
·	nd Fine Gravel	
	06 / (y * 62.43)	
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
·	arser than Sand	1935
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
·	ium Bank Slopes	1975
Bank Slopes =		-
<u>-</u>		
Future Bo	ttom Width (est)	
Bottom Width =	ttom Width (est) 10	ft
Bottom Width =	• •	ft
Bottom Width =	10 e Total Prevented Sediment	
Bottom Width = Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate	10 Prevented Sediment Channel Condition - Equilibrium Channe	l Condition
Step 3: Calculate the Volume of Prevented Sediment = Existing Column of Prevented Sediment (S _v)=	10 E Total Prevented Sediment Thannel Condition - Equilibrium Channe 1,273.47	l Condition Cu. Yd.
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Column \ of \ Prevented \ Sediment \ (S_v) =$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$	10 E Total Prevented Sediment Thannel Condition - Equilibrium Channe 1,273.47 34,383.69	l Condition Cu. Yd. Cu. ft.
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Column \ of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: \ Convert \ the \ Total \ Sediment \ Volume \ Output \ Outp$	10 Protal Prevented Sediment Channel Condition - Equilibrium Channe 1,273.47 34,383.69 Volume to Annual Prevented Sediment I	l Condition Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction	10 Protal Prevented Sediment Channel Condition - Equilibrium Channe 1,273.47 34,383.69 Volume to Annual Prevented Sediment In in Efficiency and Timescale	l Condition Cu. Yd. Cu. ft.
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Column \ of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ S_p = \\ S_p =$	10 Protal Prevented Sediment Channel Condition - Equilibrium Channe 1,273.47 34,383.69 Volume to Annual Prevented Sediment In the Efficiency and Timescale 0.5 (S _V / 30)	Cu. Yd. Cu. ft.
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Column \ of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ S_p = \\ Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ \\ On \ S_p = \\ On \ S_p =$	10 Protal Prevented Sediment Channel Condition - Equilibrium Channe 1,273.47 34,383.69 Volume to Annual Prevented Sediment In the Efficiency and Timescale 0.5 (S _V / 30) 573.06	l Condition Cu. Yd. Cu. ft.
Bottom Width = $Step \ 3: \ Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Calculate \ the$ $Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: \ Convert \ the \ Total \ Sediment \ Volume \ S_p = \\ Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Adjust \ for \ Adjust \ for \ Sediment \ S_p = \\ Adjust \ for \ Sediment \ S_p = \\ Adjust \ for \ Sediment \ S_p = \\ Adjust \ for \ Sediment \ S_p = \\ Adjust \ for \ S_p = \\ Adju$	10 Protal Prevented Sediment Thannel Condition - Equilibrium Channel 1,273.47 34,383.69 Volume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density	Cu. Yd. Cu. ft. Coad Cu. ft. / year
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Calculate \ the$ $Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Adjust \ for \ Adjust \ for \ Annual \ Prevented \ Sediment \ Load = Annual \ Prevented \ Sediment \ Prevented \ Sediment \ Load = Annual \ Prevented \ Sediment \ Prevented \ Sediment \ Prevented \ Prev$	10 Part Total Prevented Sediment Thannel Condition - Equilibrium Channel 1,273.47 34,383.69 Volume to Annual Prevented Sediment In Efficiency and Timescale $0.5 (S_v / 30)$ 573.06 Soils Bulk Density Hall Volume of Prevented Sediment * Bull	Cu. Yd. Cu. ft. Coad Cu. ft. / year
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Calculate \ the$ $Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Annual \ Prevented \ Sediment \ Load = Annual \ Annual \ Prevented \ Sediment \ Load \ (Estimate) = \\ $	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Colored \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Adjust \ for \ Reduction \ S_p = \\ Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Adjust \ for \ Adjust \ for \ Sediment \ S$	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In the Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 45,077.02	Cu. Yd. Cu. ft. Coad Cu. ft. Cu. ft.
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Column \ Of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ Of \ Prevented \ Sediment \ (S_p) = \\ Adjust \ for \ Reduction \ S_p = \\ Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Adjust \ for \ Sediment \ $	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Column \ Of \ Prevented \ Sediment \ (S_v) = \\ Volume \ of \ Prevented \ Sediment \ (S_v) = \\ Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ Of \ Prevented \ Sediment \ (S_p) = \\ Adjust \ for \ Reduction \ S_p = \\ Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) = \\ Annual \ Prevented \ Sediment \ Load \ (Estimate) = \\ Annual \ Prevented \ Sediment \ Load \ (Field \ Verified) = \\ Step \ 5: \ Determine \ the \ Estimated \ Of \ Prevented \ Sediment \ Column \ Of \ Prevented \ Sediment \ Load \ (Field \ Verified) = \\ Step \ 5: \ Determine \ the \ Estimated \ Of \ Prevented \ Sediment \ Column \ Of \ O$	10 In the total Prevented Sediment 1,273.47 34,383.69 In the inequal Prevented Sediment In the inequal P	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume for Reduction Sp = Annual Volume of Prevented Sediment (S _p) = Adjust for Reduction Adjust for Reduction Sp = Adjust for Reduction Adjust for Reduction Sp = Adjust for Reduction Adjust for Reduction Sp = Adjust for Reduction Adjust for Reduction Estimated Color 1.05 lb. of Phosphorus (P) =	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In the Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Load Cu. ft. / year k Density Ib./year Ib./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume for Reduction Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Adjust for Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Inc.) Estimated (Inc.) 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) =	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In the Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Load Cu. ft. / year k Density Ib./year Ib./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Color 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate =	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S _V / 30) 573.06 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Adjust for Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Estimated Phosphorus (P) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate =	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In the Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Bottom Width = $Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Step \ 4: Convert \ the \ Total \ Sediment \ V$ $Adjust \ for \ Reduction$ $S_p =$ $Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) =$ $Adjust \ for \ Adjust \ for \ Sediment \ (S_p) =$ $Annual \ Prevented \ Sediment \ Load \ (Estimate) =$ $Annual \ Prevented \ Sediment \ Load \ (Field \ Verified) =$ $Step \ 5: \ Determine \ the$ $Estimated \ 0$ $1.05 \ lb. \ of \ Phosphorus \ (P) =$ $2.28 \ lb. \ of \ Nitrogen \ (N) =$ $Estimated \ Phosphorus \ (P) \ Removal \ Rate =$ $Estimated \ Nitrogen \ (N) \ Removal \ Rate =$ $Estimated \ Nitrogen \ (N) \ Removal \ Rate =$ $Site \ Specifi$	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S _V / 30) 573.06 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable Not Applicable Not Applicable	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Sediment Load = Annual Prevented Sediment Load = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (I.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specifi Bulk Density =	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S , / 30) 573.06 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Se Adjusted Results	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year Ibs./year Ibs./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Color 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specific Bulk Density = 1 ton of sediment =	thannel Condition - Equilibrium Channel 1,273.47 34,383.69 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S , / 30) 573.06 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable Not Applicable Sc Adjusted Results 78.66	Cu. Yd. Cu. ft. Coad Cu. ft. / year Load Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year
Bottom Width = Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Adjust for Adjust for Adjust for Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Note that the Estimated (Not	thannel Condition - Equilibrium Channel 1,273.47 34,383.69 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Volume of Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Co Adjusted Results 78.66 0.66 1.60	Cu. Yd. Cu. ft. Cu. ft. Coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Bottom Width = Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Field Verified) = Step 5: Determine the Estimated (Note of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification Site Specification Site Specification (TSS) Removal Rate = Site Adjusted Total Suspended Solids (TSS) Removal Rate =	10 2 Total Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S _v / 30) 573.06 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Soils Adjusted Results 78.66 0.66 1.60 45,077.02	Cu. Yd. Cu. ft. Cu. ft. Coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Bottom Width = Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment (N) = Estimated Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification Site Specification (TSS) Removal Rate = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate =	10 In the total Prevented Sediment 1,273.47 34,383.69 In the in Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density In the Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable 1 ton of sediment	Cu. Yd. Cu. ft. Cu. ft. Coad Cu. ft./year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Reduction Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Sediment Load (Field Verified)) = Step 5: Determine the Estimated (Sediment Load (Field Verified)) = Step 5: Determine the Estimated (Sediment Load (Field Verified)) = Step 5: Determine the Estimated (Sediment Load (Field Verified)) = Step 5: Determine the Estimated (Sediment Load (Field Verified)) = Step 5: Determine the Estimated (Sediment Load (Field Verified)) = Step 5: Determine the Estimated (Sediment) = Step 5: Determine the Estimated (Sediment) = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate =	10 Protal Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S v / 30) 573.06 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Prota Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable Se Adjusted Results 78.66 0.66 1.60 45,077.02 14.97 36.06	Cu. Yd. Cu. ft. Cu. ft. Coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Pield Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Site Specification of Sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate = Pollutant of Concern	10 2 Total Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S _V / 30) 573.06 Soils Bulk Density Idl Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 2 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Not Applicable 1 ton of sediment	Cu. Yd. Cu. ft. Coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Bottom Width = Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Reduction Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Field Verified) = Ste	thannel Condition - Equilibrium Channel 1,273.47 34,383.69 Volume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S _v / 30) 573.06 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Ca Adjusted Results 78.66 0.66 1.60 45,077.02 14.97 36.06 1 (POC) Crediting Summary 45,077.02	Cu. Yd. Cu. ft. Cu. ft. Coad Cu. ft./year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Pield Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Site Specification of Sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate = Pollutant of Concern	10 2 Total Prevented Sediment 1,273.47 34,383.69 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S _V / 30) 573.06 Soils Bulk Density Idl Volume of Prevented Sediment * Bulk Not Applicable 45,077.02 2 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Not Applicable 1 ton of sediment	Cu. Yd. Cu. ft. Coad Cu. ft. / year Load Cu. ft. / year Lb./year Lb./year Lbs./year Lbs./year Lbs./year Lbs./year Lbs./year Lbs./year Lbs./year Lbs./year



THE POLLUTANT OF CONCERN (POC) CREDITING FOR THIS OUTFALL RESTORATION PROJECT WAS PERFORMED UNDER PROTOCOL 5 AND IN ACCORDANCE WITH THE GUIDANCE MEMO "RECOMMENDATIONS FOR CREDITING OUTFALL AND GULLY STABILIZATION PROJECTS IN THE CHESAPEAKE BAY WATERSHED", DATED OCTOBER 15, 2019. SITE SAMPLES WERE COLLECTED ON 04/21/2022 AND ANALYZED BY WAYPOINT ANALYTICAL ON 05/02/2022. THE SOIL SAMPLE BULK DENSITY WAS 78.66 LB/FT³ AND THE CONCENTRATIONS WERE 0.66 LBS OF PHOSPHORUS PER 1 TON OF SEDIMENT AND 1.60 LBS OF NITROGEN PER 1 TON OF SEDIMENT. THROUGH IN-SITU SITE OBSERVATIONS, THE OUTFALL CHANNEL BED WAS ASSUMED TO HAVE A COHESIVE BED PLACING THE EQUILIBRIUM SLOPE UNDER BED CONDITION 1. THE EQUILIBRIUM SLOPE WAS FOUND TO BE 0.45%. THE TOTAL VOLUME OF PREVENTED SEDIMENT WAS OBTAINED THROUGH A COMPARISON OF THE EXISTING CHANNEL CONDITIONS WITH THE USE OF SURFACE COMPARISON MODELING IN AUTODESK CIVIL 3D SOFTWARE. A TOTAL PREVENT SEDIMENT VOLUME (SV) OF 34,383.69 CUBIC FEET WAS OBTAINED. BASED ON THE PREVENTED SEDIMENT CALCULATIONS, IT IS ANTICIPATED THAT AN ESTIMATED 45,077.02 LB/YR OF SEDIMENT, 14.97 LB/YR OF PHOSPHORUS, AND 36.06 LB/YR OF NITROGEN REMOVAL WILL BE PROVIDED THROUGH CHANNEL RESTORATION.



POC CREDITING SUMMARY

330

315

310

310

311

AND GULLY RESTORATION

LION RUN SITE

LION RUN SITE

PREPARED FOR CITY OF FAIRFAX PUBLIC WORKS

SHEET NUMBER



Appendix F. Pickett Road Outfall Restoration POC Reduction Calculations

100% CONSTRUCTION PLANS PICKETT ROAD SITE OUTFALL AND GULLY STABILIZATION PROJECT

PIN#: 58 1 02 28 3410 PICKETT ROAD CITY OF FAIRFAX, VIRGINIA

VICINITY MAP

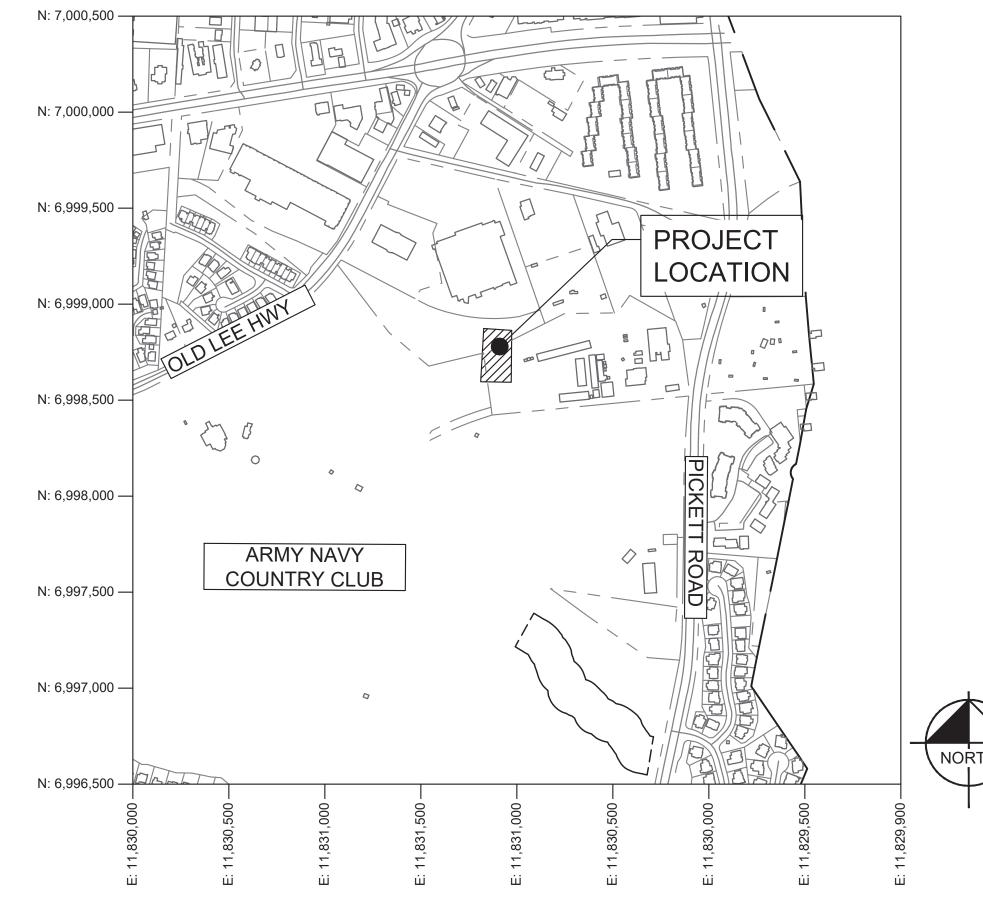
1" = 500'

PROJECT NARRATIVE

- THE SUBJECT PROPERTY OF THIS PROJECT IS TAX MAP NUMBER: 58 1 02 28
- TOPOGRAPHIC INFORMATION SHOWN IS BASED ON GROUND SURVEYS PERFORMED BY RICE ASSOCIATES ON JULY, 2021. THE TOPOGRAPHIC INFORMATION HAS BEEN CONVERTED FROM VERTICAL DATUM NAVD88 TO NGVD29 BY KIMLEY-HORN. THE HORIZONTAL DATUM IS NAD83. THE GROUND SURVEYS HAVE BEEN SUPPLEMENTED WITH THE BEST AVAILABLE DATA FROM THE CITY OF FAIRFAX GEOGRAPHIC INFORMATION SYSTEM.
- THE EXISTING UTILITIES, AS SHOWN HEREON, ARE APPROXIMATE ONLY. NO GUARANTEE IS HEREIN MADE OR IMPLIED THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT ALL UTILITY COMPANIES AND TO VERIFY THE TYPE, SIZE, AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO STARTING THE WORK. ANY DISCREPANCIES IN OR FROM THE INFORMATION SHOWN HEREON SHALL BE REPORTED TO KIMLEY-HORN AND ASSOCIATES..
- CONTRACTORS SHALL NOTIFY OPERATORS WHO MAINTAIN UNDERGROUND UTILITY LINES IN THE AREA OF PROPOSED EXCAVATION AND/OR BLASTING AT LEAST TWO WORKING DAYS, BUT NOT MORE THAN 10 WORKING DAYS PRIOR TO COMMENCEMENT OF EXCAVATION OR DEMOLITION.
- APPROVAL OF THESE PLANS IN NO WAY RELIEVES THE CONTRACTOR OF ALL APPLICABLE FEDERAL, STATE, AND LOCAL ORDINANCES.

DECLARATION OF NO IMPACT TO THE FLOODPLAIN NARRATIVE: THE DEVELOPMENT WITHIN THE FLOODPLAIN IS RELATED TO THE MAINTENANCE AND RESTORATION OF THE EXISTING MANMADE STORM SEWER OUTFALL CHANNEL. THE INTENT OF THE CHANNEL REPAIR AND RESTORATION IS TO RETURN THE ERODED RECEIVING CHANNEL TO A STABLE CONDITION AND PREVENT FUTURE EROSION. THE PROJECT EARTHWORK IS A NET CUT AND THE PROPOSED CHANGES IN THE FLOODPLAIN CROSS SECTIONAL AREA ARE ASSUMED AS NEGLIGIBLE WHEN COMPARED TO THE OVERALL FLOODPLAIN CROSS SECTIONAL AREA. THE PROPOSED CHANNEL REPAIR WILL NOT MODIFY THE EXISTING FLOODPLAIN HYDRAULICS, NOR WILL IT IMPACT OFFSITE PROPERTY OR THE EXISTING FLOODPLAIN BOUNDARY / BASE FLOOD ELEVATIONS. THERE WILL BE NO CHANGE TO PRE AND POST DEVELOPMENT FLOODPLAIN FLOWRATE AND VELOCITY ONSITE, UPSTREAM OR DOWNSTREAM WITHIN THE STREAM CORRIDOR. ALL WORK PROPOSED AS PART OF THIS CHANNEL MAINTENANCE PROJECT IS IN COMPLIANCE WITH CITY CODE SECTION 4.15.8 APPROVAL CRITERIA.

Checklist of Submittal Requirements					
Impervious surface in the floodplain: 0.23 ac.					
Area of floodplain vegetation disturbed:	0.49	ac.			
Area of floodplain land graded: 0.10 ac					
Maximum depth of cut or fill on floodplain land:	4.61 (cut)	ft.			



	OWNER	CLIENT	ENGINEER	
NAME	NAME CITY OF FAIRFAX CITY OF FAIRFAX		KIMLEY-HORN	
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA	
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO	
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589	

Sheet List Table				
Sheet Number	Sheet Title			
01	COVER SHEET			
02	GENERAL NOTES & DETAILS			
03	CORRESPONDENCE			
04	EXISTING CONDITIONS			
05	PHOTO LOCATION MAP			
06	EROSION & SEDIMENT CONTROL PHASE I			
07	EROSION & SEDIMENT CONTROL PHASE II			
08	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
09	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
10	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
11	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
12	EXISTING HYDROLOGY			
13	LAND COVER ANALYSIS (TR55)			
14	EXISTING CONDITIONS HYDROGRAPH			
15	POC CREDITING SUMMARY			
16	OUTFALL RESTORATION			
17	LANDSCAPING PLAN			
18	PLANTING DETAILS			
19	EXISTING TREE INVENTORY			



		7990	1000	14.	
J.A.C	J.A.C				ВУ
06/16/2022 J.A.C	07/27/2022 J.A.C				DATE
PUBLIC WORKS COMMENTS	PUBLIC WORKS COMMENTS				REVISIONS
_	2				No.

SHEET NUMBER

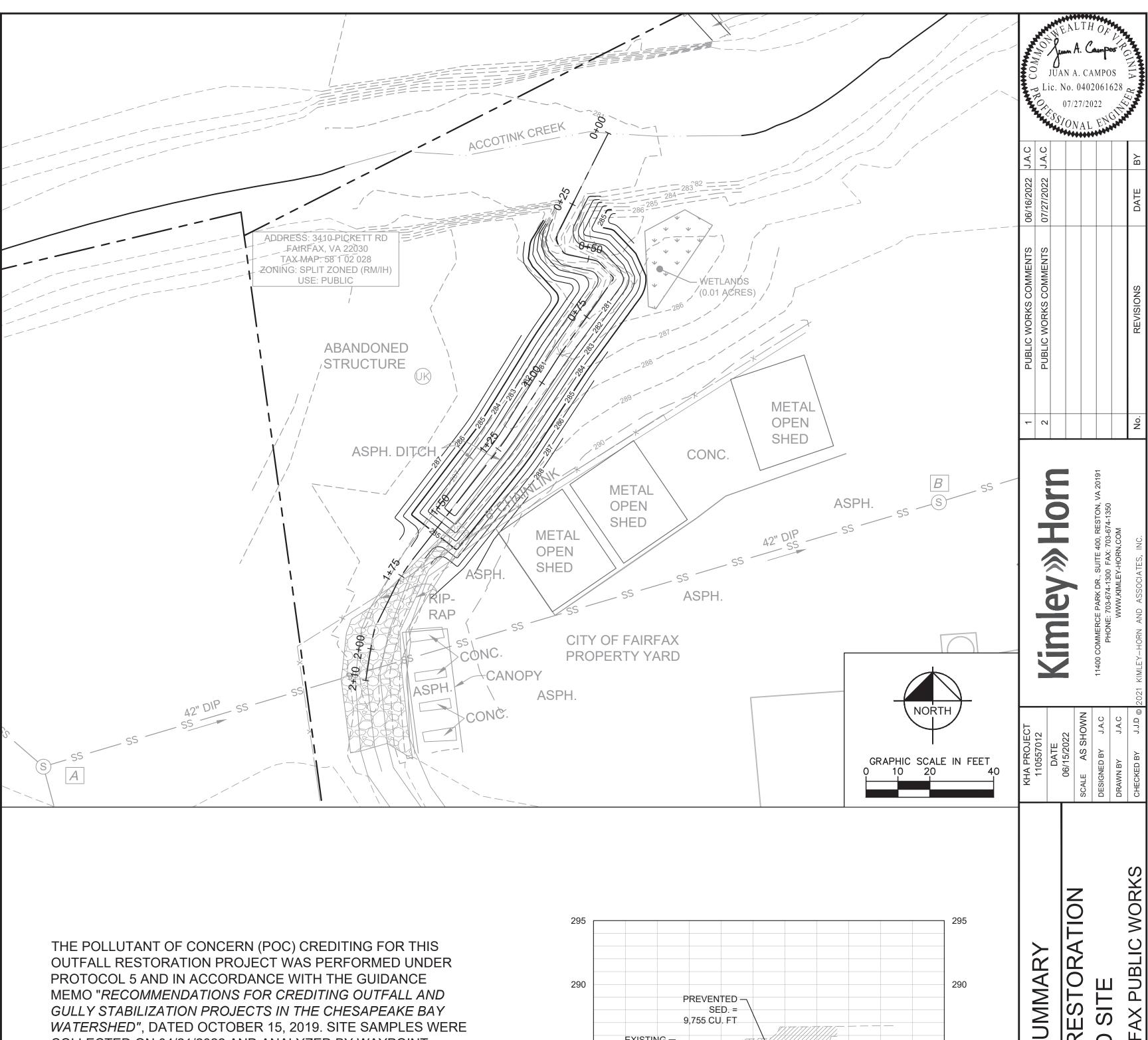
01



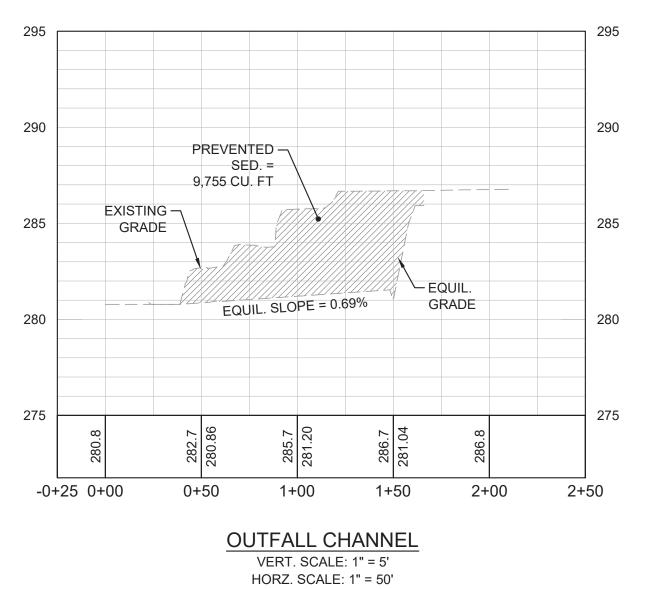
Field Data				
Bulk Density = 71.17 // // // // // // // 71.17				
1 ton of sediment =	0.64	lb. of (P)		
1 ton of sediment =	3.2	lb. of (N)		

Project Information				
Project Name:	CITY OF FAIRFAX OUTFALL AND GULLY STABILIZATION			
Project Number: 110557012				
Date:	5/19/2022			
Design By: JJD				

Existing Outfall Char	nnel Condition Parameters							
Drainage Area (A _d)=	15.98	ас						
1 11		km²						
Drainage Area (A _d)=	0.0647							
Mean Flow Depth = 1.330 ft Step 1 - Define the Existing Channel Conditions								
Length of Proposed Reach = 150.000 ft								
Channel Slope =	ft/ft							
Bank Height =	3.733	ft						
Bottom Width =	4.133	ft						
Top Width =	18.533	ft						
Bulk Density (Estimate) =	84.278	lb./ft³						
Step 2 - Define the Eq	uilibrium Channel Conditions							
Is there a pipe outfall or other defining infrastructur site?	e present upstream of the restoration	Yes						
	ax= 153A _d 0.6							
		f.						
Maximum Upstream Channel Length (L _{max}) = Equilib	Not Applicable rium Bed Slope	ft						
Choose Bed Condition =	Bed Condition 1							
Bed Condition 1 =	Cohesive Bed							
Bed Condition 2 =	Sand and Fine Grave (0.1-5mm	particle size)						
Bed Condition 3 =	,	n particle size)						
	ion 1: Cohesive Bed							
S_{eq} =	= 0.0028A ^{-0.33}							
Equilibrium Slope (S _{eq})=	0.0069	ft/ft						
Sand a	and Fine Gravel							
$S_{eq} = 0$.06 / (y * 62.43)							
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft						
·	arser than Sand							
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft						
·	ium Bank Slopes							
Bank Slopes =		-						
Future Bo	ettom Width (est)							
Bottom Width =	3.5	ft						
Step 3: Calculate the	e Total Prevented Sediment							
Volume of Prevented Sediment = Existing C	Channel Condition - Equilibrium Channe	l Condition						
Volume of Prevented Sediment (S _v)=	361.28	Cu. Yd.						
Volume of Prevented Sediment (S _v)=	9,754.56	Cu. ft.						
Step 4: Convert the Total Sediment \	Volume to Annual Prevented Sediment I	Load						
	n in Efficiency and Timescale							
·	: 0.5 (S _v / 30)							
Annual Volume of Prevented Sediment (S _p)=	162.58	Cu. ft. / year						
Adjust for	Soils Bulk Density							
Annual Prevented Sediment Load = Annu	•	·						
Annual Prevented Sediment Load (Estimate) =	Not Applicable	lb./year						
Annual Prevented Sediment Load (Field Verified) =	11,570.53	lb./year						
	e Annual Prevented Nutrients Conversion Factors							
1.05 lb. of Phosphorus (P) =	1 ton of sediment	t						
2.28 lb. of Nitrogen (N) =	1 ton of sediment	t						
Estimated Phosphorus (P) Removal Rate =	Not Applicable	lbs./year						
Estimated Nitrogen (N) Removal Rate =	Not Applicable	lbs./year						
Site Specifi	ic Adjusted Results	-						
Bulk Density =	71.17	lb./ft ³						
1 ton of sediment =	0.64	<i>lb. of (P)</i>						
1 ton of sediment =	3.20	lb. of (N)						
Site Adjusted Total Suspended Solids (TSS) Removal Rate =	11,570.53	lbs./year						
Site Adjusted Phosphorus (P) Removal Rate =	3.70	lbs./year						
Site Adjusted Nitrogen (N) Removal Rate =	18.51	lbs./year						
Pollutant of Concern	n (POC) Crediting Summary							
Total Suspended Solids (TSS) Removal Rate =	11,570.53	lbs./year						
Phosphorus (P) Removal Rate =	3.70	lbs./year						
Nitrogen (N) Removal Rate =	18.51	lbs./year						
-		· *						



COLLECTED ON 04/21/2022 AND ANALYZED BY WAYPOINT ANALYTICAL ON 05/02/2022. THE SOIL SAMPLE BULK DENSITY WAS 71.17 LB/FT³ AND THE CONCENTRATIONS WERE 0.64 LBS OF PHOSPHORUS PER 1 TON OF SEDIMENT AND 3.20 LBS OF NITROGEN PER 1 TON OF SEDIMENT. THROUGH IN-SITU SITE OBSERVATIONS, THE OUTFALL CHANNEL BED WAS ASSUMED TO HAVE A COHESIVE BED PLACING THE EQUILIBRIUM SLOPE UNDER BED CONDITION 1. THE EQUILIBRIUM SLOPE WAS FOUND TO BE 0.69%. THE TOTAL VOLUME OF PREVENTED SEDIMENT WAS OBTAINED THROUGH A COMPARISON OF THE EXISTING CHANNEL CONDITIONS WITH THE USE OF SURFACE COMPARISON MODELING IN AUTODESK CIVIL 3D SOFTWARE. A TOTAL PREVENT SEDIMENT VOLUME (SV) OF 9,755 CUBIC FEET WAS OBTAINED. BASED ON THE PREVENTED SEDIMENT CALCULATIONS, IT IS ANTICIPATED THAT AN ESTIMATED 11,570.53 LB/YR OF SEDIMENT, 3.70 LB/YR OF PHOSPHORUS, AND 18.51 LB/YR OF NITROGEN REMOVAL WILL BE PROVIDED THROUGH CHANNEL RESTORATION.



POC CREDITING SUMMARY
OUTFALL AND GULLY RESTORATION
PICKETT ROAD SITE

SHEET NUMBER



Appendix G. Shiloh Street Outfall Restoration POC Reduction Calculations

100% CONSTRUCTION PLANS SHILOH STREET SITE OUTFALL AND GULLY STABILIZATION PROJECT

PIN#: 47 4 01 002 C 10400 SHILOH STREET CITY OF FAIRFAX, VIRGINIA

VICINITY MAP

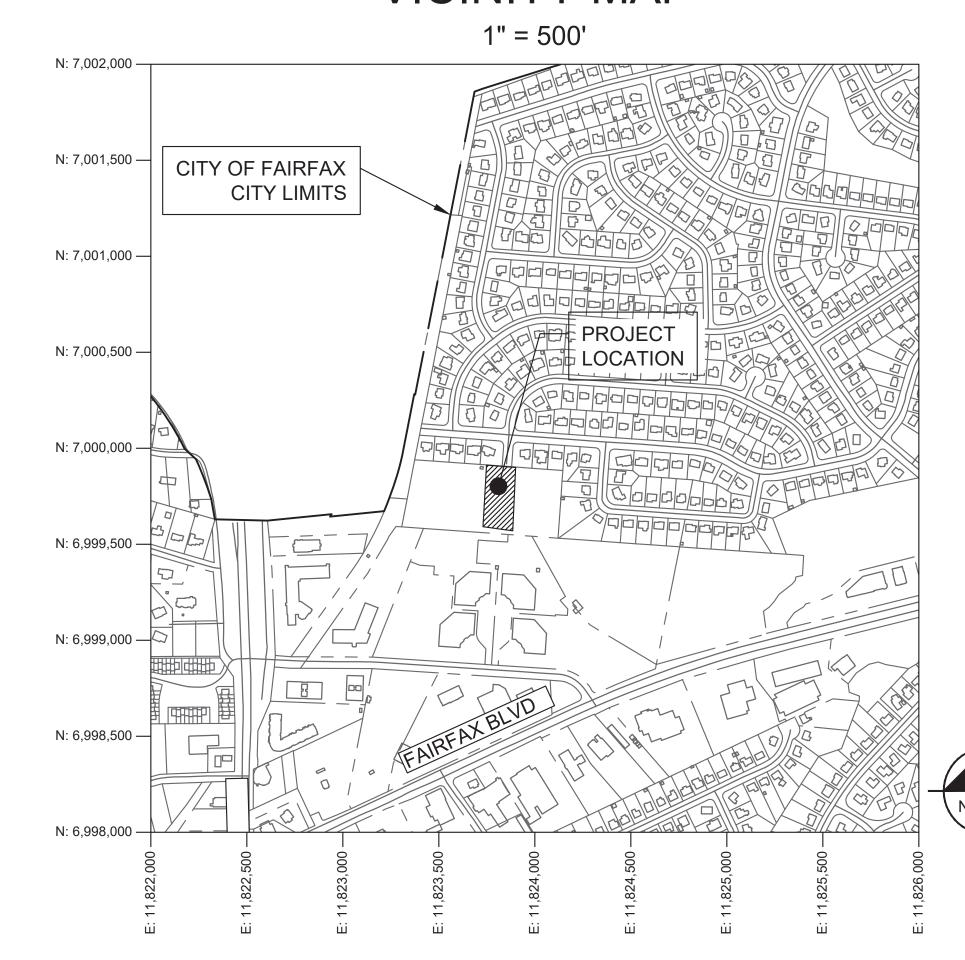
PROJECT NARRATIVE

(TSS), 17.09 LBS/YR OF NITROGEN, AND 9.25 LBS/YR OF PHOSPHORUS

- THE SUBJECT PROPERTY OF THIS PROJECT IS TAX MAP NUMBER: 47 4 01 002 C
- TOPOGRAPHIC INFORMATION SHOWN IS BASED ON GROUND SURVEYS PERFORMED BY RICE ASSOCIATES ON JULY, 2021. THE TOPOGRAPHIC INFORMATION HAS BEEN CONVERTED FROM VERTICAL DATUM NAVD88 TO NGVD29 BY KIMLEY-HORN. THE HORIZONTAL DATUM IS NAD83. THE GROUND SURVEYS HAVE BEEN SUPPLEMENTED WITH THE BEST AVAILABLE DATA FROM THE CITY OF FAIRFAX GEOGRAPHIC INFORMATION SYSTEM.
- THE EXISTING UTILITIES, AS SHOWN HEREON, ARE APPROXIMATE ONLY. NO GUARANTEE IS HEREIN MADE OR IMPLIED THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT ALL UTILITY COMPANIES AND TO VERIFY THE TYPE, SIZE, AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO STARTING THE WORK. ANY DISCREPANCIES IN OR FROM THE INFORMATION SHOWN HEREON SHALL BE REPORTED TO KIMLEY-HORN AND ASSOCIATES..
- CONTRACTORS SHALL NOTIFY OPERATORS WHO MAINTAIN UNDERGROUND UTILITY LINES IN THE AREA OF PROPOSED EXCAVATION AND/OR BLASTING AT LEAST TWO WORKING DAYS, BUT NOT MORE THAN 10 WORKING DAYS PRIOR TO COMMENCEMENT OF EXCAVATION OR DEMOLITION.
- APPROVAL OF THESE PLANS IN NO WAY RELIEVES THE CONTRACTOR OF ALL APPLICABLE FEDERAL, STATE, AND LOCAL ORDINANCES.

DECLARATION OF NO IMPACT TO THE FLOODPLAIN NARRATIVE: THE DEVELOPMENT WITHIN THE FLOODPLAIN IS RELATED TO THE MAINTENANCE AND RESTORATION OF THE EXISTING MANMADE STORM SEWER OUTFALL CHANNEL. THE INTENT OF THE CHANNEL REPAIR AND RESTORATION IS TO RETURN THE ERODED RECEIVING CHANNEL TO A STABLE CONDITION AND PREVENT FUTURE EROSION. THE PROJECT EARTHWORK IS A NET CUT AND THE PROPOSED CHANGES IN THE FLOODPLAIN CROSS SECTIONAL AREA ARE ASSUMED AS NEGLIGIBLE WHEN COMPARED TO THE OVERALL FLOODPLAIN CROSS SECTIONAL AREA. THE PROPOSED CHANNEL REPAIR WILL NOT MODIFY THE EXISTING FLOODPLAIN HYDRAULICS, NOR WILL IT IMPACT OFFSITE PROPERTY OR THE EXISTING FLOODPLAIN BOUNDARY / BASE FLOOD ELEVATIONS. THERE WILL BE NO CHANGE TO PRE AND POST DEVELOPMENT FLOODPLAIN FLOWRATE AND VELOCITY ONSITE, UPSTREAM OR DOWNSTREAM WITHIN THE STREAM CORRIDOR. ALL WORK PROPOSED AS PART OF THIS CHANNEL MAINTENANCE PROJECT IS IN COMPLIANCE WITH CITY CODE SECTION 4.15.8 APPROVAL CRITERIA.

Checklist of Submittal Requirements				
Impervious surface in the floodplain:	0.08	ac.		
Area of floodplain vegetation disturbed:	0.51	ac.		
Area of floodplain land graded:	0.11	ac.		
Maximum depth of cut or fill on floodplain land:	2.23 (cut)	ft.		



	OWNER	CLIENT	ENGINEER	
NAME	CITY OF FAIRFAX	CITY OF FAIRFAX	KIMLEY-HORN	
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA	
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO	
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589	

Sheet List Table				
Sheet Number	Sheet Title			
01	COVER SHEET			
02	GENERAL NOTES & DETAILS			
03	CORRESPONDENCE			
04	EXISTING CONDITIONS			
05	PHOTO LOCATION MAP			
06	EROSION & SEDIMENT CONTROL PHASE I			
07	EROSION & SEDIMENT CONTROL PHASE II			
08	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
09	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
10	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
11	EROSION & SEDIMENT CONTROL NOTES & DETAILS			
12	EXISTING HYDROLOGY			
13	LAND COVER ANALYSIS (TR55)			
14	EXISTING CONDITIONS HYDROGRAPH			
15	POC CREDITING SUMMARY			
16	OUTFALL RESTORATION			
17	LANDSCAPING PLAN			
18	PLANTING DETAILS			
19	EXISTING TREE INVENTORY			



PARAMANANA.							
J.A.C	J.A.C						λα
06/16/2022 J.A.C	07/27/2022 J.A.C						TATE
PUBLIC WORKS COMMENTS	PUBLIC WORKS COMMENTS						SINCISIME

SHEET NUMBER

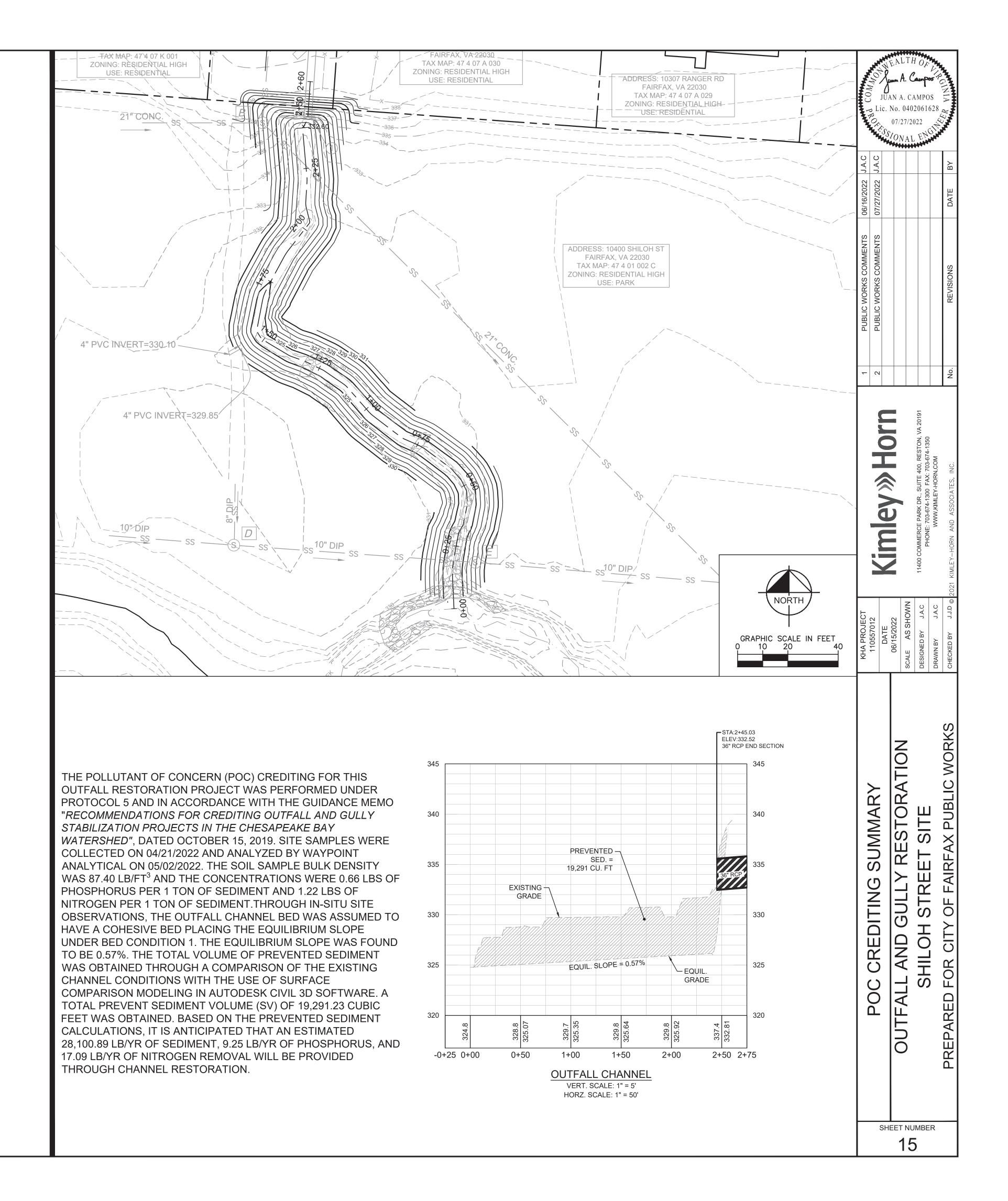
01

Know what's below.

Field Data				
Bulk Density =	87.4	lb./ft³		
1 ton of sediment =	0.658	lb. of (P)		
1 ton of sediment =	1.216	lb. of (N)		

Project Information				
Project Name:	CITY OF FAIRFAX OUTFALL AND GULLY STABILIZATION			
Project Number: 110557012				
Date:	5/19/2022			
Design By:	JJD			

	and Candition Demonstrate	
_	nnel Condition Parameters	
Drainage Area (A _d)=	28.77	ac 2
Drainage Area (A _d)=	0.1165	km ²
Mean Flow Depth =	1.933	ft
	Existing Channel Conditions	C.
Length of Proposed Reach =	245.120	ft ++ /++
Channel Slope = Bank Height =	0.032 2.457	ft/ft ft
Bottom Width =	7.600	ft ft
Top Width =	30.100	ft
Bulk Density (Estimate) =	84.278	lb./ft ³
	uilibrium Channel Conditions	10.730
Is there a pipe outfall or other defining infrastructur site?		Yes
Ups	tream Limit	
L _{ma}	ax= 153A _d ^{0.6}	
Maximum Upstream Channel Length (L _{max}) =	Not Applicable	ft
<u> </u>	rium Bed Slope	
Choose Bed Condition =	Bed Condition 1	
Bed Condition 1 =	Cohesive Bed	
Bed Condition 2 =	Sand and Fine Grave (0.1-5mm	
Bed Condition 3 =		n particle size)
	ion 1: Cohesive Bed	
	= 0.0028A ^{-0.33}	I
Equilibrium Slope (S _{eq})=	0.0057	ft/ft
	nd Fine Gravel	
$S_{eq} = 0$.06 / (y * 62.43)	T
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
Bed Cod	arser than Sand	
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
Equilibri	ium Bank Slopes	
Bank Slopes =		-
I	ettom Width (est)	Ι .
Bottom Width =	6	ft
Step 3: Calculate the	e Total Prevented Sediment	
Volume of Prevented Sediment = Existing C	Channel Condition - Equilibrium Channe	el Condition
Volume of Prevented Sediment (S _v)=	714.49	Cu. Yd.
Volume of Prevented Sediment (S _v)=	19,291.23	Cu. ft.
	Volume to Annual Prevented Sediment	
•	n in Efficiency and Timescale	Loud
	: 0.5 (S _v / 30)	
Annual Volume of Prevented Sediment (S_p)=	321.52	Cu ft /
		Cu. ft. / year
Adjust for	Soils Bulk Density	
Annual Prevented Sediment Load = Annu	ual Volume of Prevented Sediment * Bul	k Density
Annual Prevented Sediment Load (Estimate) =	Not Applicable	lb./year
Annual Prevented Sediment Load (Field Verified) =	28,100.89	lb./year
·	e Annual Prevented Nutrients	
	Conversion Factors	
1.05 lb. of Phosphorus (P) =	1 ton of sedimen	
2.28 lb. of Nitrogen (N) =	1 ton of sedimen	ı
Estimated Phosphorus (P) Removal Rate =	Not Applicable	lbs./year
Estimated Nitrogen (N) Removal Rate =	Not Applicable	lbs./year
	ic Adjusted Results	
Bulk Density =	87.40	lb./ft ³
1 ton of sediment =	0.66	lb. of (P)
1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal	1.22	lb. of (N)
Site Adjusted Total Suspended Solids (TSS) Removal	28,100.89	lbs./year
Rate =	9.25	the been
Site Adjusted Phasphorus (D) Pameural Data -		lbs./year
		The lucas
Site Adjusted Nitrogen (N) Removal Rate =	17.09	lbs./year
Site Adjusted Nitrogen (N) Removal Rate = Pollutant of Concern	17.09 n (POC) Crediting Summary	
Site Adjusted Nitrogen (N) Removal Rate = Pollutant of Concern Total Suspended Solids (TSS) Removal Rate =	17.09 n (POC) Crediting Summary 28,100.89	lbs./year
	17.09 n (POC) Crediting Summary	





Appendix H. Westmore Elementary School/Dog Park Bioretention Calculations

WESTMORE SCHOOL DOG PARK

11000 BERRY STREET CITY OF FAIRFAX, VIRGINIA 22030 TAX MAP ID: 57101009 PLAN NUMBER: 18-00225

LEE HIGHWAY (RT 29) SCALE: 1'' = 300'

PROJECT NARRATIVE

THIS SITE IS LOCATED WITHIN THE CITY OF FAIRFAX CORPORATE LIMITS AT 11000 BERRY STREET FAIRFAX, VA 22030 AND IS ADJACENT TO RESIDENTIAL SINGLE FAMILY DETACHED HOUSES. THIS PROJECT CONSISTS OF THE DEVELOPMENT OF A DOG PARK.

Sheet Number	Sheet Title
C0.0	COVER
S1.0	EXISTING SURVEY
C1.0	NOTES AND DETAILS
C1.1	NOTES AND DETAILS
C2.0	EXISTING CONDITIONS
C3.0	DEMOLITION PLAN
C4.0	EROSION AND SEDIMENT CONTROL PHASE I
C4.1	EROSION AND SEDIMENT CONTROL PHASE I
C4.2	E&S NOTES & DETAILS
C4.3	E&S NOTES & DETAILS
C4.4	E&S NOTES & DETAILS
C4.5	E&S NOTES & DETAILS
C5.0	LAYOUT PLAN
C5.1	SITE NOTES & DETAILS
C5.2	SITE NOTES & DETAILS
C5.3	SITE NOTES & DETAILS
C6.0	GRADING PLAN
C6.1	STORM SEWER PROFILES AND COMPUTATION
C6.2	STORM SEWER DETAILS
C6.3	DITCH COMPUTATIONS
C7.0	BMP AREA MAP
C7.1	BMP COMPUTATIONS
C7.2	BMP COMPUTATIONS
C7.3	PRE & POST DRAINAGE ANALYSIS
C7.4	SWM COMPUTATIONS
C7.5	SWM COMPUTATIONS
C8.0	BIORETENTION PLAN & PROFILE
C8.1	SWM NOTES & DETAILS
C8.2	SWM NOTES & DETAILS
C8.3	SWM NOTES & DETAILS
L1.0	LANDSCAPE PLAN
L1.1	LANDSCAPE NOTES & DETAILS

TOTAL SHEETS

RECEIVED

Community Dev & Planning

JUL 03 2018

City of Fairfax APPROVED SITE PLAN Fire Marshal (for water distribution system & fire hydrant location)
_Fairfax Water Millord City Engineer BAR Liaison

Mend - GIS Manager

NOT REQUIRED Bonding Administrator

5/2-mueuter

SHEET NO. C0.0

OWNER

NOTICE REQUIRED

PRIMARY UTILITY COMPANIES

FAIRFAX CO. WASTEWATER COLLECTION

FAIRFAX COUNTY PUBLIC SAFETY

VERIZON (BELL ATLANTIC)

DOMINION VIRGINIA POWER

DIVISION

FAIRFAX WATER

WASHINGTON GAS

EMERGENCY

PROJECT AREA:

CURRENT ZONE:

EXISTING USE:

PROPOSED USE:

MINIMUM YARDS:

FRONT

Police/Fire/Rescue: 911

Non Emergency No.: (703) 993-8370 Miss Utility: 1-800-552-7001 OR 811

TOTAL PROPERTY AREA: 10.00 AC

CALL "MISS-UTILITY" AT LEAST 48 HOURS IN

ADVANCE OF ANY EARTH DISTURBING ACTIVITIES.

0.68 AC

OPEN SPACE/PARK

OPEN SPACE/PARK

REQUIRED

ALSO BE USED TO SERVE IN AN EMERGENCY CONDITION.

CONTRACTORS SHALL NOTIFY OPERATORS WHO MAINTAIN UNDERGROUND UTILITY LINES IN THE AREA OF

NUMBERS OF THE OPERATORS OF UNDERGROUND UTILITY LINES APPEAR BELOW. THESE NUMBERS SHALL

EMERGENCY

1-866-366-4357

703-323-1211

1-800-837-4966

ZONING TABULATIONS

SITE TABULATIONS

PROPOSED

113.6 FT

75 FT

322 FT

703-691-2131 OR 911

703-289-6395 OR 703-289-6323

703-750-1000 (GAS LEAK 703-750-4831)

CITY OF FAIRFAX 10455 ARMSTRONG STREET FAIRFAX, VIRGINIA 22030 PHONE: (703) 385-7800

APPLICANT

CITY OF FAIRFAX PARKS AND RECREATION 10455 ARMSTRONG STREET FAIRFAX, VIRGINIA 22030 CONTACT: CATHY SALGADO PHONE: (703) 385-7853

ENGINEER

TIMMONS GROUP 20110 ASHBROOK PLACE, SUITE 100 ASHBURN, VIRGINIA 20147 CONTACT: CASEY KIGHT, LA PHONE: (703) 554-6710

> APPROVED FAIRFAX WATER DATE 7/5/2018

Enter Total Disturbed Area (acres) ightarrow0.68

Maximum reduction required: 10% The site's net increase in impervious cover (acres) is: 0.194 Post-Development TP Load Reduction for Site (lb/yr):

Check:

BMP Design Specifications List: 2013 Draft Stds & Specs Linear project? No Land cover areas entered correctly? 🧼

Total disturbed area entered?

Pre-ReDevelopment Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) undisturbed,					0.00
protected forest/open space or reforested land					
Managed Turf (acres) disturbed, graded for					0.64
yards or other turf to be mowed/managed				0.64	0.04
Impervious Cover (acres)				0.04	0.04
	And the second s	4 ilian produce and a financial and a financia			0.68

Post-Development Land Cover (acres)

Constants

Annual Rainfall (inches)

Target Rainfall Event (inches) Total Phosphorus (TP) EMC (mg/L)

Total Nitrogen (TN) EMC (mg/L)

Target TP Load (lb/acre/yr)

P) (unitless correction factor)

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) undisturbed, protected forest/open space or reforested land					0,00
Managed Turf (acres) disturbed, graded for yards or other turf to be mowed/managed				0,45	0.45
Impervious Cover (acres)				0.24	0.24
Area Check	ok,	oĸ.	OK.	ÖK.	0.68

43 1.00

0.26

1.86

0.41 0.90 Runoff Coefficients (Rv)

	A Soils	B Soils	C Soils	D Soils	
Forest/Open Space	0.02	0.03	0.04	0.05	
Managed Turf	0.15	0.20	0.22	0.25	
Impervious Cover	0.95	0.95	0.95	0.95	

mary-Pre	
Listed	Adjusted
00,00	0,00
0.00	0.00
0%	0%
0.64	0.45
0.25	0.25
94%	91%
0.04	0.04
0.95	0.95
6%	9%
0.68	0.49
	Listed 0.00 0.00 0.64 0.25 94% 0.04 0.95 6%

Treatment Volume and	A NUMERICAL	au
Pre-ReDevelopment Treatment Volume (acre-ft)	0.0168	0.0128
Pre-ReDevelopment Treatment Volume (cubic feet)	732	556
Pre-ReDevelopment TP Load (lb/yr)	0.46	0.35
Pre-ReDevelopment TP Load per acre (lb/acre/yr)	0.67	0.71
Baseline TP Load (lb/yr) (0.41 lbs/acre/yr applied to pre-redevelopment pervious land proposed for new impervio	0.20	

¹ Adjusted Land Cover Summary: Pre ReDevelopment land cover minus pervious land cover (forest/open space or managed turf) acreage proposed for new impervious cover.

Adjusted total acreage is consistent with Post-ReDevelopment acreage (minus acreage of new impervious cover).

Column I shows load reduction requriement for new impervious cover (based on new development load limit, 0.41 lbs/acre/year).

Land Cover Summar	Land Cover Summary-Post (Final)		ımary-Post	Land Cover Summary-Post		
Post ReDev. & New	Impervious	Post-ReDeve	opment	Post-Development New Imperv		
Forest/Open Space Cover (acres)	0.00	Forest/Open Space Cover (acres)	0.00			
Weighted Rv(forest)	0.00	Weighted Rv(forest)	0.00			
% Forest	0%	% Forest	0%			
Managed Turf Cover (acres)	0.45	Managed Turf Cover (acres)	0.45			
Weighted Rv (turf)	0.25	Weighted Rv (turf)	0.25			
% Managed Turf	65%	% Managed Turf	91%			
mpervious Cover (acres)	0.24	ReDev. Impervious Cover (acres)	0.04	New Impervious Cover (acres)	0.19	
Rv(impervious)	0.95	Rv(impervious)	0.95	Rv(impervious)	0.95	
% Impervious	35%	% Impervious	9%			
Final Site Area (acres)	0.68	Total ReDev. Site Area (acres)	0.49			
Final Post Dev Site Rv	0.49	ReDev Site Rv	0.31			

		Treatment Volume and	d Nutrient Load		and the state of t
Final Post-Development Treatment Volume (acre-ft)	0.0281	Post-ReDevelopment Treatment Volume (acre-ft)	0.0128	Post-Development Treatment Volume (acre-ft)	0.0154
Final Post-Development Treatment Volume (cubic feet)	1,225	Post-ReDevelopment Treatment Volume (cubic feet)	556	Post-Development Treatment Volume (cubic feet)	669
Final Post- Development TP Load (lb/yr)	0.77	Post-ReDevelopment Load (TP) (lb/yr)*	0.35	Post-Development TP Load (lb/yr)	0.42
Final Post-Development TP Load per acre (lb/acre/yr)	1.13	Post-ReDevelopment TP Load per acre (lb/acre/yr)	0.71	March State - Administracy - The State of the Company of the Compa	
No. of the control of		Max. Reduction			

TP Load Reduction Required for	
Redeveloped Area (lb/yr)	0.03

(Below Pre-ReDevelopment Load)

TP Load Reduction Required for New Impervious Area (lb/yr)	0.34	
Impervious Area (lb/yr)		

Post-Development Requirement for Site Area TP Load Reduction Required (lb/yr)

Nitrogen Loads (Informational Purposes Only)

Pre-ReDevelopment TN Load (lb/yr)	3.29	

Final Post-Development TN Load	
-ReDevelopment & New Impervious)	5.50
(lb/yr)	

Lic. No. 001348 JULY 2, 2018

JAN. 26, 2018

SHEET NO.

Drainage Area A

Drainage Area A Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals	Land Cover Rv
Forest/Open Space (acres)					0.00	0.00
Managed Turf (acres)				0.45	0.45	0.25
Impervious Cover (acres)				0.24	0.24	0.95
	_			Total	0.68	



Total Phosphorus Available for Removal in D.A. A (lb/yr) 1,225 Post Development Treatment Volume in D.A. A (ft³)

Stormwater Rest Management Practices (RR = Runoff Reduction)

Stormwater Best Managemei	nt Practice:	s(RR = Run)	off Reducti	on)									Select from dropdown lists
Practice	Runoff Reduction Credit (%)	Managed Turf Credit Area (acres)	Impervious Cover Credit Area (acres)	Volume from Upstream Practice (ft ³)	Runoff Reduction (ft ³)	Remaining Runoff Volume (ft ³)	Total BMP Treatment Volume (ft ³)	Phosphorus Removal Efficiency (%)	Phosphorus Load from Upstream Practices (lb)		Phosphorus Removed By Practice (lb)	Remaining Phosphorus Load (lb)	Downstream Practice to be Employed
6. Bioretention (RR)													
6.a. Bioretention #1 or Micro-Bioretention #1 or Urban Bioretention (Spec #9)	40			0		0	O	25	0.00	0.00	0.00	0.00	
6.b. Bioretention #2 or Micro-Bioretention #2 (Spec #9)	80	0.27	0.24	0	850	213	1,063	50	0.00	0.67	0.60	0.07	

TOTAL IMPERVIOUS COVER TREATED (ac) 0.24 AREA CHECK: OK. TOTAL MANAGED TURF AREA TREATED (ac) 0.27 AREA CHECK: OK. TOTAL RUNOFF REDUCTION IN D.A. A (ft ³) 850	
TOTAL PHOSPHORUS AVAILABLE FOR REMOVAL IN D.A. A (Ib/yr)	0.77
TOTAL PHOSPHORUS REMOVED WITH RUNOFF REDUCTION PRACTICES IN D.A. A (lb/yr)	0.60
TOTAL PHOSPHORUS REMAINING AFTER APPLYING RUNOFF REDUCTION PRACTICES IN D.A. A (lb/yr)	0.17

SEE WATER QUALITY COMPLIANCE TAB FOR SITE COMPLIANCE CALCULATIONS

TOTAL IMPERVIOUS COVER TREATED (ac) 0.24 AREA CHECK: OK. TOTAL MANAGED TURF AREA TREATED (ac) 0.27 AREA CHECK: OK.	
TOTAL PHOSPHORUS REMOVAL REQUIRED ON SITE (lb/yr)	0.38
TOTAL PHOSPHORUS AVAILABLE FOR REMOVAL IN D.A. A (lb/yr)	0.77
TOTAL PHOSPHORUS AVAILABLE FOR REMOVAL IN D.A. A (lb/yr) TOTAL PHOSPHORUS REMOVED WITHOUT RUNOFF REDUCTION PRACTICES IN D.A. A (lb/yr)	0.77
TOTAL PHOSPHORUS REMOVED WITHOUT RUNOFF REDUCTION PRACTICES IN D.A. A (lb/yr)	0.00

SEE WATER QUALITY COMPLIANCE TAB FOR SITE COMPLIANCE CALCULATIONS

NITROGEN REMOVED WITH RUNOFF REDUCTION PRACTICES IN D.A. A (lb/yr)	4.39
NITROGEN REMOVED WITHOUT RUNOFF REDUCTION PRACTICES IN D.A. A (lb/yr)	0,00
TOTAL NITROGEN REMOVED IN D.A. A (lb/yr)	4.39

Site Results (Water Quality Compliance)

D.A. B

0

0.00

0.00

0.00

Parameter 1	•					
Area Checks	D.A. A	D.A. B	D.A. C	D.A. D	D.A. E	AREA CHECK
FOREST/OPEN SPACE (ac)	0.00	0.00	0.00	0.00	0.00	OK.
IMPERVIOUS COVER (ac)	0.24	0.00	0.00	0.00	0.00	OK.
IMPERVIOUS COVER TREATED (ac)	0,24	0.00	0.00	0.00	0.00	OK.
MANAGED TURF AREA (ac)	0.45	0.00	0.00	0.00	0.00	OK.
MANAGED TURF AREA TREATED (ac)	0.27	0.00	0.00	0.00	0.00	OK.
AREA CHECK	OK.	OK.	OK.	OK.	OK.	

D.A. C

0

0.00

0.00

0.00

0.00 0.00

D.A. D

0.00

0.00

0.00

D.A. E

0.00

0.00

0.00

0.00

TOTAL

850

0.77

0.60

0.17

Site Treatment Volume (ft³) 1,225

RUNOFF REDUCTION VOLUME ACHIEVED (ft³)

TP LOAD AVAILABLE FOR REMOVAL (lb/yr)

TP LOAD REDUCTION ACHIEVED (lb/yr)

Enter design storm rainfall depths (in):

Runoff Volume and Curve Number Calculations

L-year storm	2-year storm	10-year storm
2.62	3.17	4.87

Drainage Area Curve Numbers and Runoff Depths*

Curve numbers (CN, CNadj) and runoff depths (RV Developed) are computed with and without reduction practices.

Drainage Area A		A Soils	B Soils	C Soils	D Soils	Total Area (acres): 0.68
Forest/Open Space undisturbed, protected	Area (acres)	0.00	0.00	0.00	0.00	Runoff Reduction
forest/open space or reforested land	CN	30	55	70	77	Volume (ft³): 850
Managed Turf disturbed, graded for yards or other	Area (acres)	0.00	0.00	0.00	0.45	
turf to be mowed/managed	CN	39	61	74	80	
	Area (acres)	0.00	0.00	0.00	0.24	
Impervious Cover	CN	98	98	98	98	
					CN _(D.A. A) 86	
		1-year storm	2-year storm	10-year storm		
RV _{Developed} (watershed-inch) with no Ru	noff Reduction*	1.34	1.81	3,35		
RV _{Developed} (watershed-inch) with Ru	noff Reduction*	1.00	1.47	3.00		
•	Adjusted CN*	80	81	82		

Total Phosphorus

NITROGEN LOAD REDUCTION ACHIEVED (lb/yr) 4.39

Total Filospilolus	
FINAL POST-DEVELOPMENT TP LOAD (lb/yr)	0.77
TP LOAD REDUCTION REQUIRED (lb/yr)	0.38
TP LOAD REDUCTION ACHIEVED (lb/yr)	0.60
TP LOAD REMAINING (lb/yr):	0.17

TP LOAD REMAINING (lb/yr) 0.17

REMAINING TP LOAD REDUCTION REQUIRED (lb/yr): 0.00 ** TARGET TP REDUCTION EXCEEDED BY 0.22 LB/YEAR **

Total Nitrogen (For Information Purposes)

Runoff Reduction Volume and TP By Drainage Area

POST-DEVELOPMENT LOAD (lb/yr)	5.50
NITROGEN LOAD REDUCTION ACHIEVED (lb/yr)	
REMAINING POST-DEVELOPMENT NITROGEN LOAD (lb/vr)	1.11

JULY 2, 2018

THIS DRAWING PREPARED AT THE	110 Ashbrook Place, Suite 100 Ashburn, VA 20147 703.726.1342 FAX 703.726.1345 www.timmons.com	REVISION DESCRIPTION	1ST SUBMISSION	2ND SUBMISSION	3RD SUBMISSION	

20110 Ash TEL 703.72	REVI	1	2	3		
HROUGH OURS.						
R VISION ACHIEVED THROUGH OURS.	DATE	03/14/2018	05/17/2018	07/02/2018		
R VISIO	J		DA	TE 6, 2	201	8

CHECKED BY



Appendix I. University Drive Traffic Calming Calculations



DEPARTMENT OF PUBLIC WORKS

Transportation Division 10455 Armstrong St. Room 200A Fairfax, VA 22030

Phone: 703-385-7889

UNIVERSITY DRIVE TRAFFIC CALMING

PROJECT DESCRIPTION

THE PURPOSE OF THE UNIVERSITY DRIVE TRAFFIC CALMING IMPROVEMENTS IS TO IMPROVE THE SAFETY OF THE LOCAL RESIDENTS WITH THE POTENTIAL INCREASE IN TRAFFIC ON UNIVERSITY DRIVE.

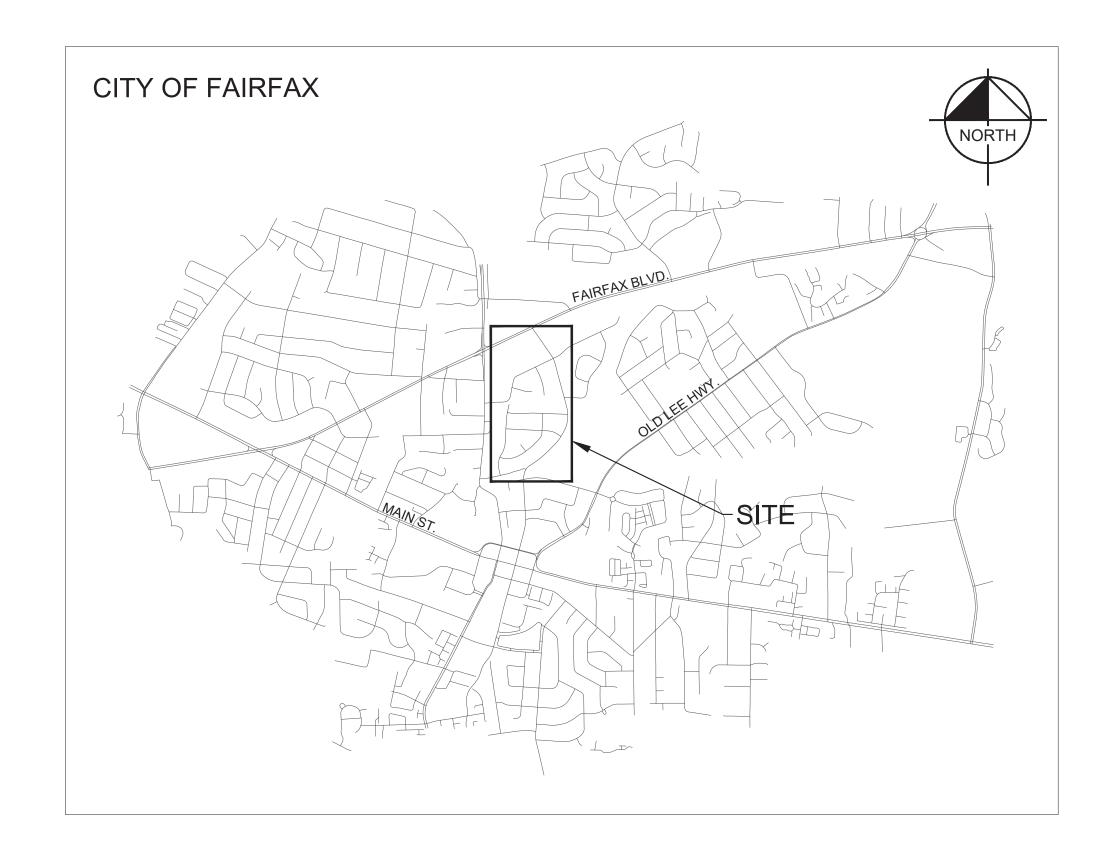
THE WORK OF THIS PROJECT INCLUDES THE FOLLOWING IMPROVEMENTS:

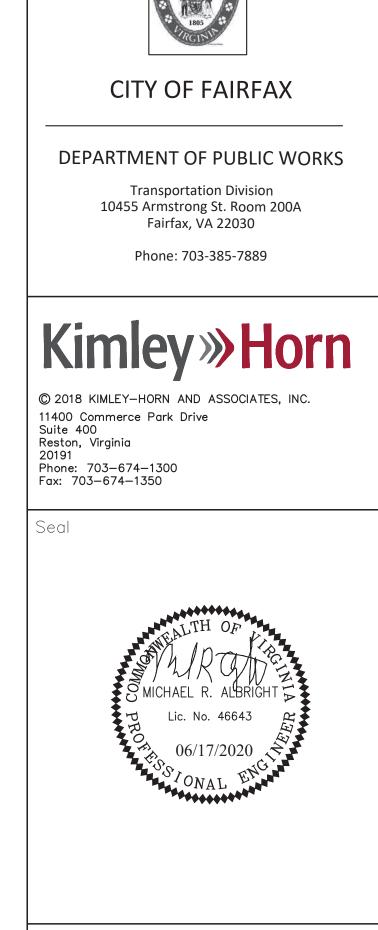
- 1. SIDEWALK CONSTRUCTION BETWEEN WOOD ROAD AND STRATFORD AVENUE
- 2. CURB EXTENSION CONSTRUCTION AT THE FORD ROAD INTERSECTION AND STRATFORD AVENUE INTERSECTION
- 3. CHICANE CONSTRUCTION BETWEEN FORD ROAD AND WOOD ROAD AND JEAN STREET AND STRATFORD AVENUE
- 4. CURB REALIGNMENT AT THE KENMORE DRIVE INTERSECTION
- 5. PEDESTRIAN ACCESSIBLE ADA RAMPS
- 6. SIGNING AND PAVEMENT MARKING
- 7. LANDSCAPING
- 8. LIGHTING

THE WORK OF THIS PROJECT WILL INCLUDE, BUT IS NOT LIMITED TO, DEMOLITION, EXCAVATION, RESTORATION, LANDSCAPING, SIGNING AND PAVEMENT MARKING, AND MAINTENANCE OF TRAFFIC.

THE CONTRACTOR SHALL COMPLETE THE WORK IN ACCORDANCE WITH THESE PLANS, REFERENCE SPECIFICATIONS, AND OTHER CONTRACT DOCUMENTS.

Location Map





Date

TABLE OF CONTENTS

SHEET NO.	DESCRIPTION
1	COVER/INDEX SHEET
2A-D	GENERAL NOTES AND DETAILS
2E	RIGHT OF WAY DATA
2F	SURVEY CONTROL DATA
2G	CONSTRUCTION ALIGNMENT DATA
2H-I	BMP CALCULATIONS AND DETAILS
3A-F	CONSTRUCTION PLAN AND INTERIM
	PAVEMENT MARKINGS
4A-F	FINAL PAVEMENT MARKING PLAN
5A-F	EROSION AND SEDIMENT CONTROL
6A-C	CURB RAMP DETAILS
7A-G	LANDSCAPE PLAN AND DETAILS
XS1-7	CROSS SECTIONS

CITY OF FAIRFAX, VIRGINIA
DEPARTMENT OF PUBLIC WORKS

CHECKED BY

UNIVERSITY DRIVE TRAFFIC CALMING

KENMORE DRIVE TO STRATFORD AVENUE

JUNE 17, 2020

SCALE SEE GRAPHIC SCALE

UPC # 113121

SHEET

1

NOTE: THE TOTAL TREATMENT AREA (0.63 AC) FOR THE PROPOSED BMP'S IS GREATER THAN THE SITE DISTURBED AREA OF 0.45 AC DUE TO OFF-SITE IMPERVIOUS FLOW WHICH IS CURRENTLY UNTREATED NOR DETAINED IN EXISTING SWM/BMP FACILITIES

DEQ Virginia Runoff Reduction Method Re-Development Compliance Spreadsheet - Version 3.0

BMP Design Specifications List: 2013 Draft Stds & Specs

Site Summary - Linear Development Project***

Project Title: University Drive Traffic Calming

Date: 43859	Total Rainfall (in):	43
	Total Disturbed Acreage:	0.63

Site Land Cover Summary

Pre-ReDevelopment Land Cover (acres)

	A soils	B Soils	C Soils	D Soils	Totals	% of Total
Forest/Open (acres)	0.00	0.00	0.00	0.00	0.00	0
Managed Turf (acres)	0.00	0.00	0.00	0.28	0.28	44
Impervious Cover (acres)	0.00	0.00	0.00	0.35	0.35	56
					0.63	100

Post-ReDevelopment Land Cover (acres)

	A soils	B Soils	C Soils	D Soils	Totals	% of Total
Forest/Open (acres)	0.00	0.00	0.00	0.00	0.00	0
Managed Turf (acres)	0.00	0.00	0.00	0.20	0.20	32
Impervious Cover (acres)	0.00	0,00	0.00	0.43	0.43	68
	-				0.63	100

Site Ty and Land Cover Nutrient Loads

	Final Post-Development (Post-ReDevelopment & New Impervious)	Post- ReDevelopment	Post- Development (New Impervious)	Adjusted Pre- ReDevelopment	
Site Rv	0.73	0.70	0.95	0.70	
Treatment Volume (ft ³)	1,664	1,388	276	1,388	
TP Load (lb/yr)	1.05	0.87	0.17	0.87	

			and the second s		Intracte/ VII	and the same of th	
	0.73	0.70	0.95	0.70	1.59	1.66	
nent Volume (ft³)	1,664	1,388	276	1,388			
d (lb/yr)	1.05	0.87	0.17	0.87			

TP Load per acre

(lb/acre/yr)

TP Load per acre

Load per acre

(lb/acre/yr)

1.59

Total TP toad Ned decidor Ned alled (10/ yr)	0.51	19/0	iiya
Total TP Load Reduction Required (lb/yr)	0.31	N/A***	N/A***

	Final Post-Development Load (Post-ReDevelopment & New Impervious)	Pre- ReDevelopment
TN Load (lb/yr)	7.48	6.57

Site Compliance Summary - ***Linear Development Project

Pre-ReDevelopment Load 20%		

	593	Total Runoff Volume Reduction (ft ³)
	0.51	Total TP Load Reduction Achieved (lb/yr)
	4.26	Total TN Load Reduction Achieved (lb/yr)
	0.53	Remaining Post Development TP Load (lb/yr)
**	0.00	Remaining TP Load Reduction (lb/yr)

TARGET TP REDUCTION EXCEEDED BY 0.2 LB/YEAR **

Drainage Area Summary

	D.A. A	D.A. B	D.A. C	D.A. D	D.A. E	Total
Forest/Open (acres)	0.00	0.00	0.00	0.00	0.00	0.00
Managed Turf (acres)	0.20	0.00	0.00	0.00	0.00	0.20
Impervious Cover (acres)	0.43	0.00	0.00	0.00	0.00	0.43
Total Area (acres)	0.63	0.00	0.00	0.00	0.00	0.63

Drainage Area Compliance Summary

#2000000000000000000000000000000000000	D.A. A	D.A. B	D.A. C	D.A. D	D.A. E	Total
TP Load Reduced (lb/yr)	0.51	0.00	0.00	0.00	0.00	0.51
TN Load Reduced (lb/yr)	4.26	0.00	0.00	0.00	0.00	4.26

Drainage Area A Summary

Land Cover Summary

	A Soils	B Soils	C Soils	D Soils	Total	% of Total
Forest/Open (acres)	0.00	0.00	0.00	0.00	0.00	0
Managed Turf (acres)	0.00	0.00	0.00	0.20	0.20	32
Impervious Cover (acres)	0.00	0.00	0.00	0.43	0.43	68
					0.62	

BMP Selections

Practice	Managed Turf Credit Area (acres)	Impervious Cover Credit Area (acres)	BMP Treatment Volume (ft³)	TP Load from Upstream Practices (lbs)	Untreated TP Load to Practice (lbs)	TP Removed (lb/yr)	TP Remaining (lb/yr)	Downstream Treatment to be Employed
2.i. To Stormwater Planter, Urban Bioretention (Spec #9, Appendix A)		0.43	1,482.86	0.00	0.93	0.51	0,42	

Total Impervious Cover Treated (acres)	0.43
Total Turf Area Treated (acres)	0.00
Total TP Load Reduction Achieved in D.A. (lb/yr)	0.51
Total TN Load Reduction Achieved in D.A.	4.26

Runoff Volume and CN Calculations

	1-year storm	2-year storm	10-year storm	
Target Rainfall Event (in)	2.60	3.14	4.82	

Drainage Areas	RV & CN	Drainage Area A	Drainage Area B	Drainage Area C	Drainage Area D	Drainage Area E
CN						
RR (ft ³)		593	0	0	0	0
	RV wo RR (ws-in)	1.79	0.00	0.00	0.00	0.00
1-year return period	RV w RR (ws-in)	1.53	0.00	0.00	0.00	0.00
	CN adjusted	89	0	0	0	0
	RV wo RR (ws-in)	2.29	0.00	0.00	0.00	0.00
2-year return period	RV w RR (ws-in)	2.03	0.00	0.00	0.00	0.00
	CN adjusted	89	0	0	0	0
	RV wo RR (ws-in)	3.91	0.00	0.00	0.00	0.00
10-year return period	RV w RR (ws-in)	3.65	0.00	0.00	0.00	0.00
	CN adjusted	89	0	0	0	0

COMPLIANCE WITH THE WATER QUALITY DESIGN CRITERIA IS DETERMINED UTILIZING THE VIRGINIA RUNOFF REDUCTION METHOD. MICRO-BIORETENTION IS THE SELECTED BMP TO REDUCE POLLUTANT LOADS AND/OR RUNOFF VOLUME. THE PEAK DISCHARGE REQUIREMENTS ARE DETERMINED IN ACCORDANCE WITH THE VDOT DRAINAGE MANUAL

THE MAXIMUM PEAK FLOW RATE IS DETERMINED FROM THE ENERGY BALANCE EQUATION IN THE VDOT DRAINAGE MANUAL. THE MAXIMUM PEAK FLOW RATE FROM THE 1-YR 24 HOUR STORM IN THE POST DEVELOPMENT CONDITION IS 1.65 CFS.

HYDRAFLOW IS USED TO DETERMINE THE PROPOSED SITE RUNOFF TREATED BY THE RAIN GARDENS. THE PROPOSED SITE RUNOFF IS 1.62 CFS, MEETING THE MAXIMUM PEAK FLOW RATE REQUIREMENT.

$$Q_{\text{Developed}} = \text{I.F.} \times \left(\frac{Q_{\text{Pre-Developed}} \times RV_{\text{Pre-Developed}}}{RV_{\text{Developed}}} \right)$$

$$= \frac{1.840cfs \times 3829cuft}{RV_{\text{Developed}}}$$

$$e_{loped} = .90 \left(\frac{3829 cuft}{3829 cuft} \right)$$

Where:

I.F. (Improvement Factor) = 0.8 for sites > 1 acre LDA or 0.9 for sites ≤ 1 acre LDA Q_{Developed} = the allowable peak flow rate of runoff from the developed site for the 1-yr

RV_{Developed} = the volume of runoff from the site in the developed condition for the 1-yr

QPre-Developed = the peak flow rate of runoff from the site in the pre-developed condition for the 1-yr 24-hour storm. RV_{Pre-Developed} = the volume of runoff from the site in pre-developed condition for the 1-

yr 24-hour storm. QForest = the peak flow rate of runoff from the site in a forested condition for the 1-yr

RVForest = the volume of runoff from the site in a forested condition for the 1-yr 24-

Hydrograph Summary Report Hydrographs Extension for Autodesk® Civil 3D® 2019 by Autodesk, Inc. v2020

Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to Peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph Description	
1	SCS Runoff	1.840	2	716	3,829				Existing Total Site Drainage	
2	SCS Runoff	1.840	2	716	3,829				Proposed Site Drainage - No Treatme	
3	SCS Runoff	1.622	2	716	3,307		T-1000		Proposed Site Drainage - Treated	

Hydrograph Report

Hydraflow Hydrographs Extension for Autodeski® CIVII 3D® 2019 by Autodesk, Inc. v2020 Thursday, 01 / 30 / 2020

Hyd. No. 1

Q (cfs)

Existing Total Site Drainage

----- Hyd No. 1

= SCS Runoff Peak discharge = 1.840 cfs Hydrograph type = 716 min Storm frequency = 1 yrs Time to peak = 2 min = 3,829 cuft Time interval Hyd. volume = 0.630 ac = 92 Drainage area Curve number = 0 ftBasin Slope = 0.0 % Hydraulic length Tc method = User Time of conc. (Tc) = 5.00 min = 2.60 inDistribution = Type II Total precip. = 24 hrs Shape factor = 484 Storm duration

Existing Total Site Drainage

Hyd. No. 1 -- 1 Year

120 240 360 480 600 720 840 960 1080 1200 1320

URBAN BIORETENTION SIZING

MINIMUM SIZING REQUIREMENT WAS DETERMINED PER VA DCR STORMWATER DESIGN SPECIFICATION 9, APPENDIX 9-A

PROPOSED BMP's MEET THE MINIMUM SIZING REQUIREMENT

 $Tv_{BMP} = [(1)(R_V)(A)/12]$ $Tv_{BMP} = [(1)(1664)(.63)/12]$ $Tv_{BMP} = 87.36 \text{ cuft}$

 $\frac{87.36ft^3}{4} = 21.84ft^3 \ per \ BMP$



CITY OF FAIRFAX

DEPARTMENT OF PUBLIC WORKS

Transportation Division 10455 Armstrong St. Room 200A Fairfax, VA 22030

Phone: 703-385-7889

© 2018 KIMLEY-HORN AND ASSOCIATES, INC. 11400 Commerce Park Drive Suite 400 Reston, Virginia 20191 Phone: 703-674-1300 Fax: 703-674-1350



Revisions	Date
	
	<u> </u>
	
DESIGNED BY	
DRAWN BY	
CHECKED BY	

CITY OF FAIRFAX, VIRGINIA DEPARTMENT OF PUBLIC WORKS

UNIVERSITY DRIVE TRAFFIC CALMING KENMORE DRIVE TO STRATFORD AVENUE BMP CALCULATIONS

UPC # 113121

Q (cfs)

SCALE SEE GRAPHIC SCALE

SHEET



Appendix J. Calculating VSMP Pollutant Reductions Creditable to Chesapeake Bay Existing Source Load Reductions



City of Fairfax, Virginia

10455 Armstrong Street • Fairfax, VA 22030-3630

Satoshi Eto Public Works Program Manager (703) 273-6073 Satoshi.Eto@fairfaxva.gov

Version 01.23.2023

STORMWATER STANDARD OPERATING PROCEDURE

CALCULATING VSMP POLLUTANT REDUCTIONS CREDITABLE TO CHESAPEAKE BAY

EXISTING SOURCE LOAD REDUCTIONS

OBJECTIVE

Identify and quantify pollutant load reductions associated with redevelopment projects that can be credited against the City's Chesapeake Bay TMDL Special Condition requirement to reduce pollutants from Existing Sources.

ACRONYMS AND DEFINITIONS

Existing Sources Existing Sources – Pervious and impervious urban land uses

served by the MS4 as of June 30, 2009

Municipal Separate Storm Sewer System MS4

Pervious and impervious urban and uses served by the MS4 **New Sources**

developed or redeveloped on

or after July 1, 2009

Virginia Pollutant Discharge Elimination System **VPDES VSMP** Virginia Stormwater Management Program

RATIONALE

As a DEQ-authorized VSMP located in the Chesapeake Bay Protection Act's Tidewater Virginia, the City is required to ensure that projects disturbing 2,500 ft.² or greater of land meet VSMP post-development water quality design criteria. For new impervious cover at new and redevelopment projects, the VSMP post-development water quality design criterium is 0.41 lbs./ac./yr. of phosphorus for new impervious cover¹. For existing impervious cover at redevelopment projects, the design criterium requires the reduction of phosphorus loads by 10% for projects less than one (1) acre in land disturbance or 20% for projects one acre or greater in land disturbance. Developers can use either on-site stormwater management practices or if local water quality allows off-site mitigation such as the purchase of nonpoint source nutrient credits to meet the VSMP design criteria.

Concurrently, as an operator of a small municipal separate storm sewer system (MS4) regulated under the VPDES General Permit for Stormwater Discharges from Small MS4s, the City is required to reduce pollutant loads from Existing Sources as shown below:

¹ The water quality design criteria for new development of 0.41 lbs./ac./yr. is based on a presumption that the pollutant load associated with a land use of 60% forest, 30% open, and 10% impervious cover is protective of Chesapeake Bay water quality. City of Fairfax Chesapeake Bay Pollutant Load Reduction Crediting Associated with Redevelopment

Eviating Source Land Has	Pollutant Reductions			
Existing Source Land Use	Nitrogen	Phosphorus		
Impervious Regulated Lands	9%	16%		
Pervious Regulated Lands	6%	7.25%		

The VSMP pollutant reductions associated redevelopment also provide a reduction in the VPDES Existing Source loads. However, pollutant reductions required for new development under the VSMP do not represent a reduction in the VPDES Existing Load as these pollutant reductions are done to ensure Chesapeake Bay water quality protection from New Sources. Excess pollutant removal above the required VSMP pollutant reductions for both new and redevelopment are creditable towards the VPDES MS4 Existing Loads reduction requirements.

These SOPs have been created to allow the City to identify and quantify the VSMP pollutant load reductions creditable to the VPDES MS4 Existing Source load reduction requirements.

PROCEDURES

As part of the VSMP plan approval process, projects are required to submit calculations demonstrating pollutant loads, pollutant load reduction requirements, and documentation and calculation verifying compliance with VSMP water quality requirements. This documentation is provided through the use and submission of the Virginia Runoff Reduction Method (VRRM) spreadsheets. The VRRM site worksheet for redevelopment projects calculates the total phosphorus load reduction required for the entire project and automatically separates the applicable portion for redeveloped acreages and the applicable portion for newly developed acreages (Figure 1). The total phosphorus (TP) load reduction for Redeveloped Area (lb./yr.) is creditable towards the VPDES MS4 Existing Source load reduction requirements. The TP load reduction for New Impervious Area (lb./yr.) is not creditable. The TP load reduction for Redeveloped Area (lb./yr.) is creditable towards the VPDES MS4 Existing Source load reduction requirements. Additionally, any TP Reduction Exceeded identified on the VRRM Summary worksheet is creditable towards the VPDES MS4 Existing Source load reduction requirements (Figure 2).

The VRRM spreadsheet should also be utilized to determine the creditable nitrogen reductions associated with the redevelopment project. To do so, the following should be followed:

- 1. Determine the percentage of the TP Reduction Achieved that is attributable to the Total TP Reduction Required. This provides you the percentage of the total load reduction achieved that is required. The remaining percentage is overtreatment and is creditable to the VPDES MS4 Existing Source load.
- 2. Determine the percentage of the TP Required that is the TP Required for Redevelopment. This gives you the percentage of the pollutant reduction that is creditable to the VPDES MS4 Existing Source load.
- 3. Obtain the TN load reduction achieved from the VRRM Summary worksheet (Figure 3).
 - a. Multiply the TN Load reduction achieved by the percentage attributable to the TP Reduction Required.
 - i. Multiply the remainder by the percentage of the TP Required that is the TP Required for Redevelopment. The answer is the amount of TN associated with redevelopment that is creditable to the VPDES MS4 Existing Source load for Nitrogen
 - b. Repeat multiplying the TN Load reduction achieved by the percentage attributable to the TP Reduction Required.

- i. Subtract the answer from the TN Load Reduction Achieved. The remainder is overtreatment and creditable to the VPDES MS4 Existing Source load for Nitrogen.
- c. See example (Figure 4).

DRAFT INTERNAL DISTRIBUTE

DRAFT INTERNAL DISTRI

VRRM Site Worksheet

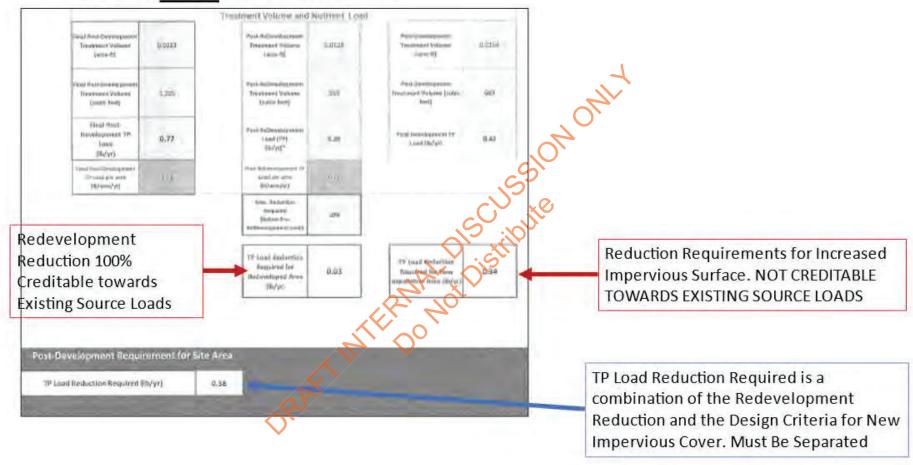


Figure 1. VRRM Redevelopment Site Worksheet Showing Phosphorus Load Reduction Requirements

VRRM <u>Summary</u> Worksheet

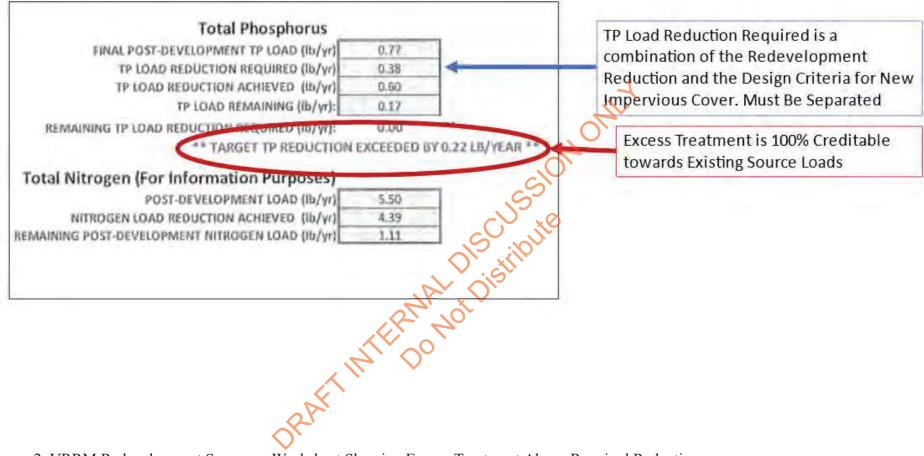


Figure 2. VRRM Redevelopment Summary Worksheet Showing Excess Treatment Above Required Reductions

VRRM Summary Worksheet

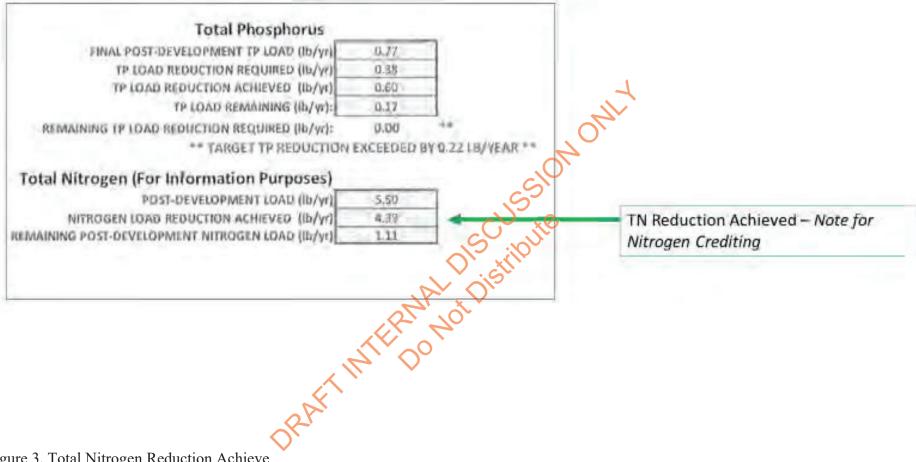


Figure 3. Total Nitrogen Reduction Achieve

Redevelopment Project A required a TP reduction associated with redevelopment of 0.03 lbs./yr. and a TP reduction of 0.35 lbs./yr. associated with new impervious cover. Redevelopment Project A achieved TP Load Reductions of 0.60 lbs./yr. and 4.39 lbs./yr. of TN.

To obtain the amount of phosphorus reduction creditable to the VPDES MS4 Existing Source load reduction requirements:

- The TP reductions totaled 0.60 lbs./yr. The required VSMP TP reductions totaled 0.38 lbs./yr. (0.03 + 0.35). The difference of 0.22 lbs./yr. of TP is creditable to the VPDES MS4 Existing Source load reduction requirements.
- The TP required for redevelopment (0.03 lbs./yr.) is creditable to the VPDES MS4 Existing Source load reduction requirements.
- The total amount of phosphorus reduction creditable from the entire project creditable to the VPDES MS4 Existing Source load reduction requirements is 0.25 lbs./yr. (0.22 + 0.03).

To obtain the amount of nitrogen reduction creditable to the VPDES MS4 Existing Source load reduction requirements:

- The TN reductions totaled 4.39 lbs./yr.
- The percentage of the TP Reductions achieved associated with Required TP reductions is 63.3%
 - o The associated TN reduction is 2.80 lbs./yr. (4.39 x 63.3%)
 - \circ The TN associated with overtreatment is 1.59 lbs /yr. (4.39 2.80). This is creditable to the VPDES MS4 Existing Source load reduction requirements.
- The percentage of the TP Required Reductions associated with TP required for redevelopment is 7.9%
 - o The associated TN reduction is 0.22 lbs./yr. (2.80 x 7.9%)
- The total amount of phosphorus reduction creditable from the entire project creditable to the VPDES MS4 Existing Source load reduction requirements is 181 lbs./yr. (1.59 + 0.22).

Figure 4. VPDES MS4 Existing Source Calculations Using VSMP Redevelopment



Appendix K. VSMP Implementation – Redevelopment Credits on Prior Developed Land

					P	hosphorus				N	litrogen		
MS4 Permit Reporting Year	Address	Latitude	Longitude	Total Reductions Achieved	Total Credited to ReDev	Total Credited to New Dev	Total Over Treated	Total Creditable To Existing Loads	Total Reductions Achieved	Total Credited to ReDev	Total Credited to New Dev	Total Over Treated	Total Creditable To Existing Loads
2023	3509 Perry Street	38.8615	-77.3113	0.10	0.05	0.05	0.00	0.05	0.66	0.33	0.33	0.00	0.33
2023	3725 Anne Pl	38.8498	-77.2915	0.09	0.03	0.06	0.00	0.03	0.67	0.22	0.45	0.00	0.22
2023	3815 Mode St	38.8465	-77.2847	0.16	0.03	0.07	0.06	0.09	1.37	0.26	0.60	0.51	0.77
2023	3821 Mode St	38.8461	-77.2835	0.12	0.05	0.07	0.00	0.05	0.87	0.36	0.51	0.00	0.36
2023	3910 Estel Rd	38.8440	-77.2821	0.05	0.04	0.02	-0.01	0.03	0.36	0.29	0.14	-0.07	0.22
2023	4105 Addison Rd	38.8423	-77.3004	0.04	0.04	0.02	0.00	0.04	0.32	0.32	0.16	-0.16	0.16
2023	9700 Fairfax Blvd	38.8646	-77.2797	0.50	0.44	0.00	0.06	0.50	1.97	1.73	0.00	0.24	1.97
2023	9709 Barlow Rd	38.8494	-77.2816	0.31	0.02	0.29	0.00	0.02	0.77	0.05	0.72	0.00	0.05
2023	9714 Ashby Rd	38.8491	-77.2821	0.09	0.06	0.00	0.03	0.09	0.71	0.47	0.00	0.24	0.71
2023	9919 Farr Dr	38.8581	-77.2900	0.05	0.03	0.02	0.00	0.03	0.36	0.22	0.14	0.00	0.22
2023	10510/10512 Cedar Ave	Multiple	Multiple	0.22	0.05	0.09	0.08	0.13	1.56	0.35	0.64	0.57	0.92
2023	10533 Cedar Ave	38.8532	-77.3117	0.03	0.03	0.01	0.00	0.03	0.23	0.23	0.08	-0.08	0.15
2023	10602 Oliver St	38.8505	-77.3108	0.19	0.07	0.11	0.00	0.07	1.37	0.50	0.79	0.07	0.58
2023	10614 Norman Ave	38.8642	-77.3135	0.17	0.04	0.12	0.01	0.05	1.28	0.30	0.90	0.08	0.38
2023	10615 Elmont Ct	38.8665	-77.3142	0.52	0.06	0.42	0.04	0.10	3.53	0.41	2.85	0.27	0.68
2023	10615 Oak Pl	38.8652	-77.3143	0.22	0.04	0.14	0.04	0.08	1.60	0.29	1.02	0.29	0.58
2022	10101 Fairfax Blvd	38.8617	-77.2933	0.39	0.16	0.00	0.23	0.39	0.00	0.00	0.00	0.00	0.00
2022	10909 Marilta Ct	38.8643	-77.3244	0.10	0.03	0.07	0.00	0.03	0.85	0.24	0.61	0.00	0.24
2022	10420 Darby St	38.8395	-77.3062	0.07	0.03	0.04	0.00	0.03	0.46	0.19	0.27	0.01	0.20
2022	10823 Woodhaven Dr	38.8566	-77.3205	0.05	0.02	0.03	0.00	0.02	0.43	0.17	0.26	0.00	0.17
2021	3600 Old Post Rd	38.8541	-77.2932	0.36	0.05	0.25	0.06	0.11	2.38	0.33	1.65	0.40	0.73
2021	9995 Fairfax Blvd			3.35	3.28	0.00	0.07	3.35	0.00	0.00	0.00	0.00	0.00
2021	Point 50 (10334 Fairfax Blvd)			1.56	1.45	0.00	0.11	1.56	4.64	4.31	0.00	0.33	4.64
2021	10706 Warwick Ave	38.8572	-77.3155	0.13	0.03	0.09	0.01	0.04	0.92	0.21	0.64	0.07	0.28
2021	Stonewood (9901-9909 Mosby Rd)	Multiple	Multiple	1.20	0.26	0.84	0.09	0.35	9.39	2.03	6.57	0.78	2.82
2021	3414 Burrows Ave	38.8646	-77.3130	0.30	0.00	0.25	0.05	0.05	2.09	0.00	1.74	0.35	0.35

					Р	hosphorus				N	litrogen		
MS4 Permit Reporting Year	Address	Latitude	Longitude	Total Reductions Achieved	Total Credited to ReDev	Total Credited to New Dev	Total Over Treated	Total Creditable To Existing Loads	Total Reductions Achieved	Total Credited to ReDev	Total Credited to New Dev	Total Over Treated	Total Creditable To Existing Loads
2021	Cobbs Grove Lane subdivision	Multiple	Multiple	1.15	0.27	0.88	0.01	0.28	8.16	1.92	6.24	0.00	1.92
2020	4221 University Dr	38.8385	-77.3066	0.08	0.02	0.06	0.00	0.02	0.58	0.15	0.44	0.00	0.15
2020	10713 Jones St	38.8448	-77.3169	0.16	0.04	0.11	0.01	0.05	1.13	0.28	0.78	0.07	0.35
2020	10341 Main St			0.73	0.10	0.49	0.14	0.24	0.00	0.00	0.00	0.00	0.00
2020	9820 Hampton Lane	38.8536	-77.2875	0.20	0.04	0.09	0.07	0.11	1.02	0.20	0.46	0.36	0.56
2020	4107 and 4109 Virginia Avenue	Multiple	Multiple	0.14	0.04	0.08	0.01	0.06	1.05	0.34	0.63	0.09	0.43
2020	10805 and 10807 First St	Multiple	Multiple	0.23	0.00	0.23	0.00	0.00	1.62	0.00	1.62	0.00	0.00
2020	3508 Winston Pl	38.8630	-77.3168	0.08	0.05	0.03	0.00	0.05	0.69	0.43	0.26	0.00	0.43
2020	3504 Cornell Rd	38.8578	-77.2851	0.07	0.06	0.02	0.00	0.06	0.50	0.43	0.14	-0.07	0.36
2020	3410 Pickett Rd	38.8601	-77.2718	0.21	0.08	0.09	0.04	0.12	0.00	0.00	0.00	0.00	0.00
2019	4040 Jermantown Rd	38.8542	-77.3331	0.12	0.02	0.05	0.05	0.07	0.00	0.00	0.00	0.00	0.00
2019	9711 Ashby Rd	38.8483	-77.2819	0.09	0.04	0.05	0.00	0.04	0.79	0.35	0.44	0.00	0.35
2019	4116 William Pl	38.8496	-77.3296	0.05	0.01	0.03	0.01	0.02	0.38	0.08	0.23	0.08	0.15
2019	4115 Burke Station Rd	38.8382	-77.2878	0.14	0.03	0.09	0.02	0.05	0.93	0.20	0.60	0.13	0.33
2019	4019 Roberts Rd	38.8430	-77.2965	0.07	0.02	0.06	0.00	0.02	0.56	0.16	0.48	-0.08	0.08
2019	3563 Old Lee Hwy	38.8562	-77.2888	0.26	0.09	0.06	0.10	0.19	1.69	0.61	0.41	0.66	1.27
2019	3504 Mavis Ct	38.8620	-77.3103	0.26	0.00	0.26	0.00	0.00	1.87	0.00	1.87	0.00	0.00
2019	4100 Addison Rd	38.8428	-77.3005	0.07	0.02	0.05	0.00	0.02	0.47	0.13	0.34	0.00	0.13
2019	10912 Byrd Dr	38.8462	-77.3202	0.81	0.33	0.12	0.37	0.70	0.54	0.21	0.08	0.25	0.46
2019	4020 Stonewall Ave	38.8404	-77.2903	0.17	0.06	0.07	0.04	0.10	1.21	0.43	0.50	0.28	0.71
2019	Mount Vineyard			3.99	1.17	3.48	-0.66	0.51	14.11	4.14	12.31	-2.33	1.80
2019	10709 Orchard St	38.8596	-77.3155	0.15	0.04	0.11	0.00	0.04	1.29	0.34	0.95	0.00	0.34
2019	10514 Oak Pl	38.8649	-77.3105	0.11	0.04	0.07	0.00	0.04	0.76	0.28	0.48	0.00	0.28
			Total	20	8.96	9.64	1.15	10	78	25	50	3.32	28



Appendix L. NPS Nutrient Credit Purchase: Whispering Hills



CITY OF FAIRFAX, VIRGINIA

Contract Number: 23031 Purchase of Nutrient Credits for the City of Fairfax Storm Sewer System

This contract entered into this ____2 day of November 2022, by CBAY-VA, LLC (Resource Environmental Solutions, LLC), 1408 B Roseneath Road, Richmond, VA 23230, hereinafter called the "Contractor" and City of Fairfax, VA, 22030.

WITNESSETH that the Contractor and City of Fairfax, VA, in consideration of the mutual covenants, promises and agreements herein contained, agree as follows:

SCOPE OF CONTRACT: The Contractor shall serve as a Nutrient Trader for the Purchase of Nutrient Credits for the City of Fairfax, VA. The Contractor shall provide qualified nutrient mitigation banks for the purchase of up to thirty (30) pounds of perpetual phosphorous credits. The credits will assist the City in reaching nutrient reductions required by its Municipal Separate Storm Sewer System (MS4) Permit Chesapeake Bay Total Maximum Daily Load (TMDL) Action Plan. The credits are required to be located within the MS4 locality or within the locality's Chesapeake Bay Tributary (Potomac) and must be applicable to City of Fairfax in accordance with § 62.1-44.19:21 of the Code of Virginia.

PERIOD OF PERFORMANCE: From date of award through June 30, 2023. This contract may be renewed by the City upon written agreement of both parties for three (3) successive one-year periods, under the terms of the current contract.

PAYMENT TERMS: Net 30

INVOICES: accountspayable@fairfaxva.gov

The contract documents shall consist of:

(1) This signed form;

CONTRD 4 CROP

- (2) Invitation for Bid #23031, dated September 27, 2022:
- (3) CBAY-VA, LLC bid dated October 24, 2022.

IN WITNESS WHEREOF, the parties have caused this Contract to be duly executed intending to be bound thereby.

DAIDDAY OWN HA

CONTRACTOR:	By: Patricia Innocente
Ben Eubanks	Patricia Innocenti
Γitle: VP. East Region & GM, Mid-Atlantic	Title: Purchasing Agent

4343.1 or against a bidder or offeror because of race, religion, color, sex, sexual orientation, gender identity, national origin, age, disability, or any other basis prohibited by state law relating to discrimination in employment. Note: This public body does not discriminate against faith-based organizations in accordance with the Code of Virginia, § 2.2-

Contact Information:

Amy Staley, Credit Sales Manager 919-209-1055 astaley@res.us

A	B	С	D	ш	ш	G *
Bank Name / HUC8	Number of Phosphorous Credits	Number of Unit Price per Phosphorous Credits Credit	Extended Price	Total Number of Corresponding Nitrogen Credits	Total Number of Corresponding Sediment Credits	Total Number ofTotal Number ofPrice per Nitrogen CreditCorrespondingCorresponding(Column D divided by Nitrogen CreditsNitrogen CreditsSediment CreditsColumn E)*
Whispering Hills / 02070008	30	\$8,500.00	\$255,000.00	81	\$37,735.50	\$3,148.15

Exhibit C

CBAY-VA, LLC

AFFIDAVIT OF PHOSPHORUS CREDIT SALE

CBAY-VA, LLC, a Virginia limited liability company (the "Seller"), hereby certifies the following:

- Pursuant to that certain Purchase and Sale Agreement dated November 2, 2022 (as the same may 1. have been amended prior to the date hereof, the "Agreement"), between the Seller and City of Fairfax, Virginia ("Buyer"), the Seller, for the benefit of the Buyer agreed to sell 30.00 nonpoint source nutrient phosphorus Credits to Buyer and retire the associated ratio of nonpoint source nitrogen and sediment Credits at the credit generating facility in the amount of **81.00** pounds of nitrogen Credits and **37,735.50** pounds of sediment Credits.
- The Seller and the Buyer as of the date hereof, have closed the transaction contemplated by the Agreement and the Company has sold to Buyer the credits described above.

WITNESS the following signa	ature:	
	Y-VA LLC, ginia limited liability company Authorized Sig	
Date:	2/1/2023	
		lay of <u>February</u> , 20 <u>23</u> , by
limited liability company.		, , ,
Notary registration number: 7746382 My commission expires: 01-31-25	risty Lynn Cappa Notary Public	State of Virginia City / County of: Richmond CRISTY LYNN CAPPS Electronic Notary Public Commonwealth of Virginia Registration No. 7746382 My Commission Expires Jan 31, 2025

Permit #: Pending

Project Description: City of Fairfax Storm Sewer System– Fairfax, VA

Permittee: City of Fairfax, Virginia **Phosphorus Credits:** 30.00 pounds

Associated Nitrogen Credits: 81.00 pounds **Associated Sediment Credits:** 37,735.50 pounds

RES.1.0 3 Exhibit D

CBAY-VA LLC

BILL OF SALE

BILL OF SALE, made as of February 1, 2023, by CBAY-VA LLC, a Virginia limited liability

company ("Seller"), to City of Fairfax, Virginia ("Buyer").

WHEREAS, Seller and Buyer have entered into that certain Purchase and Sale Agreement as of

November 2, 2022 (the "Agreement"), with respect to the sale by the Seller and purchase by the Buyer of

nonpoint source phosphorus Credits generated within the Whispering Hills Nutrient Bank Property in

Loudoun County, Virginia.

NOW, THEREFORE, for and in consideration of the payment of the Purchase Price (as defined

in the Agreement) and other good and valuable consideration, the receipt and sufficiency of which are

hereby acknowledged, Seller hereby sells, transfers, assigns, conveys, delivers and sets over to Buyer, its

successors and assigns, 30.00 pounds of phosphorus Credits and retires 81.00 pounds of nitrogen Credits

and 37,735.50 pounds of sediment Credits associated with the phosphorous Credits generated at the

Whispering Hills Property as such are described in the Agreement.

TO HAVE AND TO HOLD all such phosphorus Credits hereby sold and transferred to Buyer

and its successors and assigns forever.

IN WITNESS WHEREOF, Seller has caused this Bill of Sale to be executed by its duly

authorized representative as of the date first above written.

CBAY-VA LLC,

a Virginia Limited Liability Company

By:

Authorized Signatory

RES.1.0 4

MS4 Nutrient Credit Acquisition Form

Pursuant to Code of Virginia sections § 62.1-44.19:21.A and Part II.A.10 of the General VPDES Permit for Discharges of Stormwater from Small Municipal Separate Storm Sewer Systems, the below named Permittees hereby certify that credits have been transferred between their two facilities as outlined below in full or partial satisfaction of compliance obligations:

Facility generating credits:	ng Hills		VAN	
- wo, Bo	Fac	ility Name		Registration No.
Facility acquiring credits:	City of F	airfax		VAR <u>040064</u>
	Fac	ility Name		Registration No.
Credits Transferred				
Compliance Year:		2023	_	
Delivered Total Nitrogen C	81.00	lbs		
Delivered Total Phosphorus	30.00	_lbs		
Delivered Total Sediment	37,735.50	<u>lbs</u>		
I certify under penalty of law that the supervision in accordance with a systhe information submitted. Based of	stem designed to	assure that qualified p	ersonnel pro	operly gather and evaluate
persons directly responsible for gat		_		
knowledge and belief, true, accurat	e and complete.	I am aware that there a	re significat	nt penalties for submitting
false information, including the pos	sibility of fine or	imprisonment for kno	wing violat	ions.

Facility generating credits:	Facility acquiring credits:		
Principal Executive Officer or Authorized Agent:	Principal Executive Officer or Authorized Agent:		
Amy Staley	Robert A. Stalzer		
Typed or Printed Name	Type or Printed Name		
Amy Staly Signature	Signatur		
919-209-1055	703 385 7850		
Area Code/Phone Number	Area Code/Phone Number		
2/15/2023	2-16-23		
Date	Date		



Appendix M. DEQ MS4 Nutrient Credit Acquisition Form

MS4 Nutrient Credit Acquisition Form

Pursuant to Code of Virginia sections § 62.1-44.19:21.A and Part II.A.10 of the General VPDES Permit for Discharges of Stormwater from Small Municipal Separate Storm Sewer Systems, the below named Permittees hereby certify that credits have been transferred between their two facilities as outlined below in full or partial satisfaction of compliance obligations:

Facility generating credits:			VAN
, c	Facility Name		Registration No.
Facility acquiring credits:			VAR
	Facility Name		Registration No.
Credits Transferred			
Compliance Year:			
Delivered Total Nitrogen Credits:		lbs	
Delivered Total Phosphorus Credits:		lbs	
Facility generating credits:	Fac	ility acquiring	g credits:
Principal Executive Officer or Authorized Agent:	Princ	ipal Executive Off	icer or Authorized Agent:
Typed or Printed Name		Type or Print	ed Name
Signature		Signatur	re
Area Code/Phone Number		Area Code/Pho	one Number
Date		Date	



Appendix N. Stafford Drive Stream and Outfall Restoration Calculations

STAFFORD DRIVE STREAM RESTORATION

THIS PROJECT OUTLINES THE USE OF NATURAL CHANNEL DESIGN (NCD) TECHNIQUES FOR THE RESTORATION OF AND 181.04 LB/YR OF PHOSPHORUS

UTILITY CONTACTS

NAMES AND TELEPHONE NUMBERS OF POSSIBLE OPERATORS OF UNDERGROUND UTILITY LINES APPEAR BELOW. THESE NUMBERS SHALL ALSO BE USED TO SERVE IN AN EMERGENCY CONDITION

GAS	COLUMBIA GAS TRANSMISSION CORP. WASHINGTON GAS CNG TRANSMISSION CORP.	(703) 327 - 6331 (800) 752 - 7520 (814) 583 - 5171	
ELECTRIC	DOMINION VIRGINIA POWER NOVEC	(888) 667 - 3000 (888) 335 - 0500	MISS UTILITY
TELEPHONE	AT&T VERIZON	(800) 288 - 2747 (800) 256 - 4646	DIAL 811, OR 1-800-5 BEFORE DIGGIN
CABLE	COMCAST	(888) 375 - 4888	
WATER & SEWER	FAIRFAX WATER	(703) 698 - 5600	
OTHER	CENTURY LINK	(800) 366 - 8201 ——	

NON-EMERGENCY

FIRE AND RESCUE: (703) 385 - 7940 FOR EMERGENCIES, CALL 911

SOURCE OF TITLE

THE SUBJECT PROJECT COVERS TWO (2) DISTINCT PARCELS. THE PARCEL SITES SHOWN HEREON ARE LOCATED IN THE CITY OF FAIRFAX. THE PARCEL INFORMATION IS INCLUDED BELOW:

- 2. PARCEL ID: 47 4 02 002; DEED BOOK 16304 PAGE 911; AREA = 9.17 ACRES (399,262 SF); OWNER OF RECORD:

GENERAL NOTES

- 1. THE TOPOGRAPHIC INFORMATION SHOWN IS BASED ON GROUND SURVEYS PERFORMED BY TIMMONS GROUP ON AUGUST, 2020 - SEPTEMBER, 2020. THE SURVEY HAS BEEN SUPPLEMENTED WITH AN ADDITIONAL GROUND SURVEY CONDUCTED BY RICE ASSOCIATES ON JULY, 2021. THE HORIZONTAL DATUM IS NAD83 AND THE VERTICAL DATUM IS NGVD29. THE GROUND SURVEYS HAVE ALSO BEEN SUPPLEMENTED WITH THE BEST AVAILABLE DATA FROM THE CITY OF FAIRFAX GEOGRAPHIC INFORMATION SYSTEM.
- 2. THE EXISTING UTILITIES, AS SHOWN HEREON, ARE APPROXIMATE ONLY. NO GUARANTEE IS HEREIN MADE OR IMPLIED THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT ALL UTILITY COMPANIES AND TO VERIFY THE TYPE, SIZE, AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO STARTING THE WORK. ANY DISCREPANCIES IN OR FROM THE INFORMATION SHOWN HEREON SHALL BE REPORTED TO KIMLEY-HORN AND ASSOCIATES.
- 3. CONTRACTORS SHALL NOTIFY OPERATORS WHO MAINTAIN UNDERGROUND UTILITY LINES IN THE AREA OF PROPOSED EXCAVATION AND/OR BLASTING AT LEAST TWO (2) WORKING DAYS, BUT NOT MORE THAN TEN (10) WORKING DAYS PRIOR TO COMMENCEMENT OF EXCAVATION OR DEMOLITION.
- 4. APPROVAL OF THESE PLANS IN NO WAY RELIEVES THE CONTRACTOR OF ALL APPLICABLE FEDERAL, STATE,
- 4. THE AREA SHOWN HERON IS LOCATED ON THE FLOOD INSURANCE RATE MAPS (FIRM), COMMUNITY PANEL NO. 5155240002D, WITH AN EFFECTIVE DATE OF JUNE 2, 2006.
- 5. TO THE BEST KNOWLEDGE OF THE ENGINEER, THERE ARE NO EXISTING GRAVES OR BURIAL SITES LOCATED ON THE PROPERTY. THE SUBJECT PROPERTY IS NOT LISTED UNDER THE NATIONAL REGISTER OF HISTORICAL
- 6. TO THE BEST KNOWLEDGE OF THE ENGINEER, THIS SITE PLAN CONFORMS TO ALL APPLICABLE ORDINANCES, REGULATIONS AND ADOPTED STANDARDS, UNLESS OTHERWISE SPECIFICALLY NOTED.
- WETLAND INFORMATION IS BASED ON WETLAND DELINEATION CONDUCTED BY TIMMONS GROUP ON 08/06/2020. 8. DUE TO THE PROJECT BEING A STREAM RESTORATION, RESOURCE PROTECTION AREAS (RPA) ARE LOCATED ON THE SUBJECT PROPERTIES.

	OWNER	CLIENT	ENGINEER
NAME	CITY OF FAIRFAX	CITY OF FAIRFAX DEPARTMENT OF PUBLIC WORKS	KIMLEY-HORN
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589

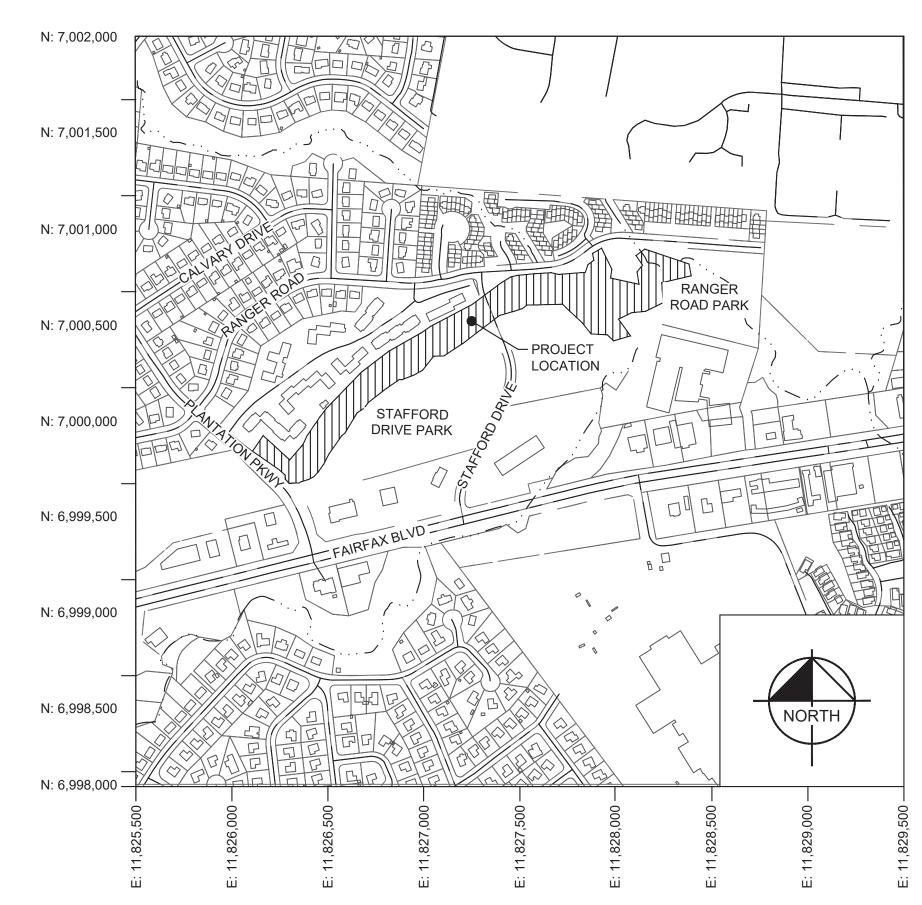
60% DESIGN

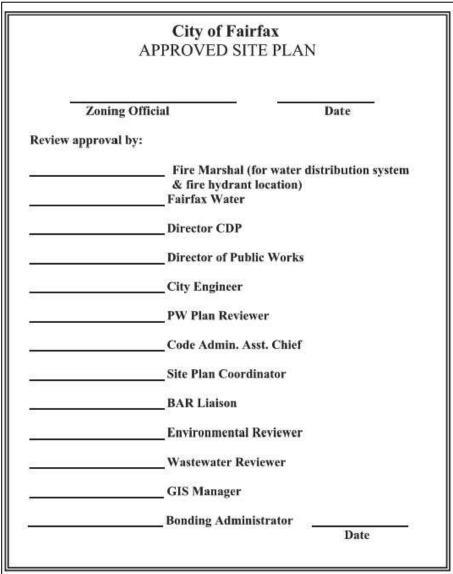
SP-##-#####

3300 STAFFORD DRIVE, FAIRFAX, VA 22030 PIN #: 47402001A, 47402002 CITY OF FAIRFAX, VA

VICINITY MAP

1" = 500'



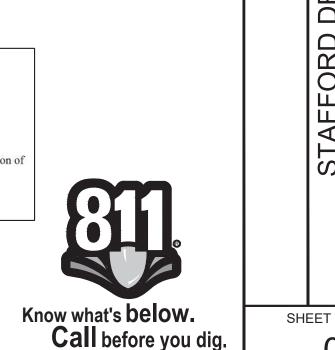


To Whom IT May Concern: I/We, The City of Fairfax identified below do hereby authorize Jon D'Ale	essandro of eact as my/our agent(s) in the furtherance of an on my/our property located at:				
Tax Map No: 47402001A & 47402002 Thank you in advance for your cooperation.					
Date:	Ву:				
COMMONWEALTH/STATE OF: Virginia					
CITY/COUNTY: City of Fairfax	, TO WIT:				
The forgoing instrument was acknowledged before me this day of					
20, by	.				
	Notary Public (Signature)				
AFFIX NOTARY SEAL/STAMP	Notary Registration No:				
	My Commission Expires:				

AGENT AUTHORIZATION LETTER

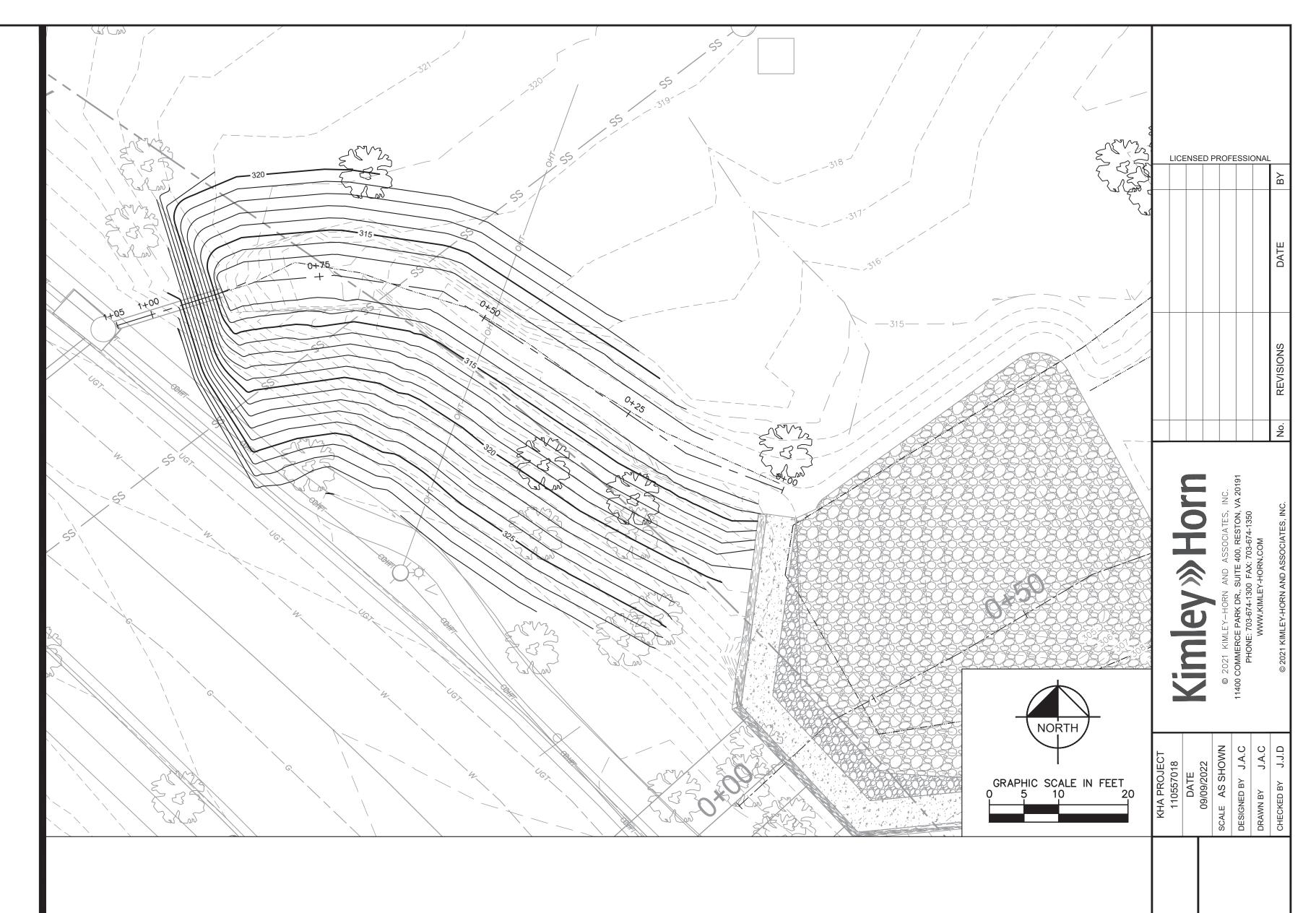
Sheet Number	Sheet Title
01	COVER SHEET
02	LEGENDS AND SYMBOLS
03	GENERAL NOTES
04	GENERAL NOTES
05	CORRESPONDENCE
06	VIEWPORT LEGEND
07	EXISTING CONDITIONS
08	EXISTING CONDITIONS
09	EXISTING CONDITIONS
10	PHOTO LOCATION MAP
11	PHOTO LOCATION MAP
12	PHOTO LOCATION MAP
13	EXISTING SITE PHOTOS
14	EXISTING SITE PHOTOS
15	DESIGN TABLE AND NARRATIVE
16	EXISTING PROFILE AND MORPHOLOGY
17	EXISTING PROFILE AND MORPHOLOGY
18	EXISTING PROFILE AND MORPHOLOGY EXISTING MORPHOLOGY TABLE
19	EXISTING CROSS-SECTIONS & PEBBLE COUNT
20	EXISTING STREAM HYDROLOGY
21	EXISTING STREAM HYDROLOGY
22	EXISTING CURVE NUMBER CALCULATIONS
23	EROSION & SEDIMENT CONTROL PHASE I
24	EROSION & SEDIMENT CONTROL PHASE I
25	EROSION & SEDIMENT CONTROL PHASE I
26	EROSION & SEDIMENT CONTROL PHASE II
27	EROSION & SEDIMENT CONTROL PHASE II
28	EROSION & SEDIMENT CONTROL PHASE II
29	EROSION & SEDIMENT CONTROL NOTES & DETAILS
30	EROSION & SEDIMENT CONTROL NOTES & DETAILS
31	EROSION & SEDIMENT CONTROL NOTES & DETAILS
32	EROSION & SEDIMENT CONTROL NOTES & DETAILS
33	STREAM RESTORATION PLAN
34	STREAM RESTORATION PLAN
35	STREAM RESTORATION PLAN
36	LONGITUDINAL PROFILE
37	LONGITUDINAL PROFILE
38	TYPICAL STREAM CROSS SECTION
39	STREAM OUTFALL CHANNELS
40	STREAM OUTFALL CHANNELS
41	STREAM OUTFALL CHANNELS
42	PROPOSED WETLANDS PLAN
43	PROPOSED WETLANDS PLAN
44	PROPOSED WETLANDS PLAN
45	PROPOSED WETLANDS PLAN
46	PROPOSED WETLANDS PLAN
47	
48	EXISTING CONDITIONS (OUTFALL 1)
	EXISTING CONDITIONS (OUTFALL 2)
49	PHOTO LOCATION (OUTFALL 1)
50	PHOTO LOCATION (OUTFALL 2)
51	EXISTING HYDROLOGY (OUTFALL 1)
52	EXISTING HYDROLOGY (OUTFALL 2)
53	OUTFALL LAND COVER ANALYSIS (TR-55)
54	POC CREDITING SUMMARY (OUTFALL 1)
55	POC CREDITING SUMMARY (OUTFALL 2)
56	OUTFALL 1 RESTORATION
57	OUTFALL 2 RESTORATION
58	SEEDING PLAN
59	SEEDING PLAN
60	SEEDING PLAN
61	PLANTING PLAN
62	PLANTING PLAN
63	PLANTING PLAN
64	SEEDING AND PLANTING SCHEDULES
65	LANDSCAPING NOTES
66	LANDSCAPING DETAILS
67	TREE REMOVAL PLAN
68	TREE REMOVAL PLAN
69	TREE REMOVAL PLAN
70	TREE REMOVAL TABLE
<u> </u>	1

	CITY OF FA Site Plan Checklist and Cer	
The following affidavit and che	cklist must be printed on the cover page and	signed by a certified engineer, architect or land surveyor.
I Jon D'Alessandro the attached site plan that is requ	Certification for Complete do hereby certify that this site plan uired pursuant to Section 110-6.8 in the Cod	checklist is complete and accurate for use in staff's evaluation of
(signature)	(date)	(SEAL)

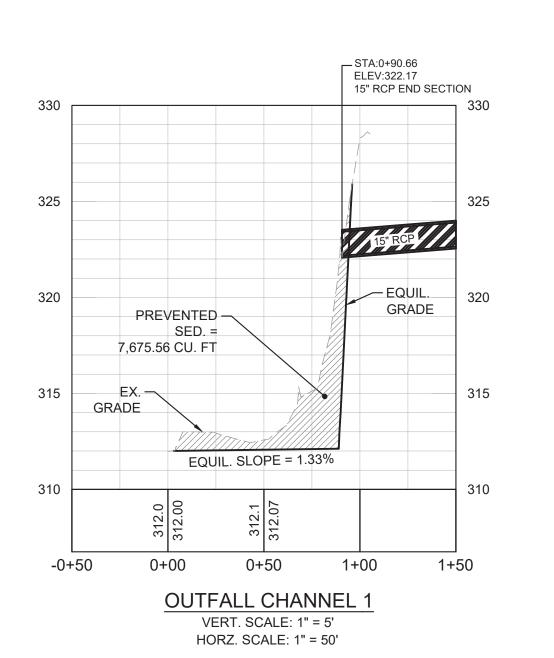


SHEET NUMBER

<u>Existing Outfall Char</u>		
Drainage Area (A _d)=	2.21	ас
Drainage Area (A _d)=	0.0089	km²
Mean Flow Depth =	0.400	ft
Step 1 - Define the E	xisting Channel Conditions	
Length of Proposed Reach =	90.660	ft
Channel Slope =	0.11	ft/ft
Bank Height =	2.62	ft
Bottom Width =	5.55	ft
Top Width =	11.04	ft
Bulk Density (Estimate) =	84.28	lb./ft ³
· · ·	uilibrium Channel Conditions	
Is there a pipe outfall or other defining infrastructure	e present upstream of the restoration	Yes
site?		
-	tream Limit	
L _m ;	ax= 153A _d ^{0.6}	
Maximum Upstream Channel Length (L _{max}) =	Not Applicable	ft
Equilib	rium Bed Slope	
Choose Bed Condition =	Bed Condition 1	
Bed Condition 1 =	Cohesive Bed	
Bed Condition 2 =	•	<u> </u>
Bed Condition 3 =		particle size)
	ion 1: Cohesive Bed	
$S_{eq} =$	= 0.0028A ^{-0.33}	
Equilibrium Slope (S _{eq})=	0.0133	ft/ft
Sand a	nd Fine Gravel	
$S_{eq} = 0.$.06 / (y * 62.43)	
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
	arser than Sand	2 . 2
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
·	ium Bank Slopes	3 , 3
Bank Slopes =	·	-
	ottom Width (est)	
Bottom Width =	3	ft
Step 3: Calculate the	e Total Prevented Sediment	
·		
Volume of Prevented Sediment = Existing C		l Condition
Volume of Prevented Sediment = Existing C	Channel Condition - Equilibrium Channe	
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v)=		l Condition Cu. Yd.
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) =	Channel Condition - Equilibrium Channe 284.28 7,675.56	Cu. Yd. Cu. ft.
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V	Channel Condition - Equilibrium Channe 284.28 7,675.56 Volume to Annual Prevented Sediment L	Cu. Yd. Cu. ft.
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Valuet for Reduction	Channel Condition - Equilibrium Channe 284.28 7,675.56 Volume to Annual Prevented Sediment Lens in Efficiency and Timescale	Cu. Yd. Cu. ft.
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction	Channel Condition - Equilibrium Channe 284.28 7,675.56 Volume to Annual Prevented Sediment L	Cu. Yd. Cu. ft.
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Valuet for Reduction $S_p = S_p = S_$	Channel Condition - Equilibrium Channe 284.28 7,675.56 Volume to Annual Prevented Sediment Lens in Efficiency and Timescale	Cu. Yd. Cu. ft.
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Valuet for Reduction S_p = Annual Volume of Prevented Sediment (S_p) =	284.28 7,675.56 Volume to Annual Prevented Sediment Len in Efficiency and Timescale 50.5 (S _v / 30)	Cu. Yd. Cu. ft.
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = $Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ S_p = S_p $	Channel Condition - Equilibrium Channe 284.28 7,675.56 Volume to Annual Prevented Sediment L in in Efficiency and Timescale $0.5 (S_v / 30)$ 127.93 Soils Bulk Density	Cu. Yd. Cu. ft. Coad Cu. ft. / year
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Valuet for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Annual Prevented Sediment Load = A	284.28 7,675.56 Volume to Annual Prevented Sediment Len in Efficiency and Timescale 10.5 (S , / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk	Cu. Yd. Cu. ft. Coad Cu. ft. / year
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Valuet for Reduction $S_p = 1000 \text{Adjust for Reduction}$ Annual Volume of Prevented Sediment (S_p) = Adjust for Adjust for Adjust for Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = $S_p = 1000 \text{Annual Prevented Sediment Load}$	284.28 7,675.56 Volume to Annual Prevented Sediment Len in Efficiency and Timescale 20.5 (S v / 30) 127.93 2 Soils Bulk Density Not Applicable	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Values for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) =	284.28 7,675.56 Volume to Annual Prevented Sediment Len in Efficiency and Timescale 20.5 (S v / 30) 127.93 2 Soils Bulk Density 284.28 7,675.56 Volume to Annual Prevented Sediment * Bulk Not Applicable 7,506.70	Cu. Yd. Cu. ft. Coad Cu. ft. / year
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Value of Prevented Sediment (S_p) = Annual Volume of Prevented Sediment (S_p) = Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the	284.28 7,675.56 Volume to Annual Prevented Sediment Lenin Efficiency and Timescale 20.5 (S v / 30) 127.93 2 Soils Bulk Density 284.28 7,675.56 Volume to Annual Prevented Sediment * Bulk Not Applicable 7,506.70 2 Annual Prevented Nutrients	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated	284.28 7,675.56 Volume to Annual Prevented Sediment Len in Efficiency and Timescale 20.5 (S _V / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Field Verified) =	284.28 7,675.56 Volume to Annual Prevented Sediment In in Efficiency and Timescale 20.5 (S _V / 30) 127.93 2 Soils Bulk Density 2 Volume of Prevented Sediment * Bulk 3 Not Applicable 7,506.70 4 Annual Prevented Nutrients Conversion Factors 1 ton of sediment	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Values for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) =	284.28 7,675.56 Volume to Annual Prevented Sediment Lenin Efficiency and Timescale 20.5 (S v / 30) 127.93 2 Soils Bulk Density 2 Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 2 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total Sediment Load (Field Verified) = Step 5: Determine (Total	284.28 7,675.56 Volume to Annual Prevented Sediment In in Efficiency and Timescale 20.5 (S _V / 30) 127.93 2 Soils Bulk Density 2 Volume of Prevented Sediment * Bulk 3 Not Applicable 7,506.70 4 Annual Prevented Nutrients Conversion Factors 1 ton of sediment	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment (S _p) = Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (The Indian Company of the Indian Company of th	284.28 7,675.56 Volume to Annual Prevented Sediment II In in Efficiency and Timescale 20.5 (S _V / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable	Cu. Yd. Cu. ft. coad Cu. ft. / year k Density Ib./year Ib./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment (S_p) = Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Sediment Load (Pield Verified)) = Step 5: Determine the Estimated (Pield Verified) = Step 5: Determine the Estimat	284.28 7,675.56 Volume to Annual Prevented Sediment II in Efficiency and Timescale 20.5 (S v / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification	284.28 7,675.56 Volume to Annual Prevented Sediment II in Efficiency and Timescale 0.5 (S , / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable I ton of sediment Not Applicable Not Applicable Not Applicable ic Adjusted Results	Cu. Yd. Cu. ft. coad Cu. ft. / year k Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification of Sediment =	284.28 7,675.56 Volume to Annual Prevented Sediment II in Efficiency and Timescale in 0.5 (S v / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 e Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable Not Applicable ic Adjusted Results 58.68	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (I.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification of Sediment = 1 ton of sediment =	284.28 7,675.56 Volume to Annual Prevented Sediment In in Efficiency and Timescale 20.5 (S v / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable ic Adjusted Results 58.68 2.60 0.90	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment (S _p) = Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine the Estimated (Total Sediment Load = Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Step 5: Determine (Total Sediment Load = Annual Prevented Sediment	284.28 7,675.56 Volume to Annual Prevented Sediment In in Efficiency and Timescale 50.5 (S v / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Soils Adjusted Results 58.68 2.60 0.90	Cu. Yd. Cu. ft. coad Cu. ft. / year k Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Annual Prevented Sediment Load = Annu Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specifi Bulk Density = 1 ton of sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal	284.28 7,675.56 Volume to Annual Prevented Sediment In in Efficiency and Timescale 20.5 (S v / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable ic Adjusted Results 58.68 2.60 0.90	Cu. Yd. Cu. ft. Coad Cu. ft. / year k Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load	284.28 7,675.56 Volume to Annual Prevented Sediment In in Efficiency and Timescale 20.5 (S , / 30) 127.93 2 Soils Bulk Density 2 Volume of Prevented Sediment * Bulk 3 Not Applicable 7,506.70 4 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 58.68 2.60 0.90 7,506.70	Cu. Yd. Cu. ft. Coad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specifi Bulk Density = 1 ton of sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate =	284.28 7,675.56 Volume to Annual Prevented Sediment II in Efficiency and Timescale 20.5 (S v / 30) 127.93 2 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 2 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Sediment Not Applicable Sediment Not Applicable Not Applicable Not Applicable Not Applicable 10 Adjusted Results 58.68 2.60 0.90 7,506.70 9.76	Cu. Yd. Cu. ft. Coad Cu. ft. / year Lb./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p)= Adjust for Annual Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load) = One of Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load) = One of Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load) = One of Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment Load) = One of Prevented Sediment Retails = One of Prevented Sediment Retails = One of Prevented Sediment Sediment Retails = One of Prevented Sedime	284.28 7,675.56 Volume to Annual Prevented Sediment II in Efficiency and Timescale in 0.5 (S v / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 e Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 58.68 2.60 0.90 7,506.70 9.76 3.38	Cu. Yd. Cu. ft. Coad Cu. ft. / year Lb./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing C Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specifi Bulk Density = 1 ton of sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate =	284.28 7,675.56 Volume to Annual Prevented Sediment In in Efficiency and Timescale 10.5 (S v / 30) 127.93 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 7,506.70 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 58.68 2.60 0.90 7,506.70 9.76 3.38 (POC) Crediting Summary	Cu. Yd. Cu. ft. coad Cu. ft. / year Lb./year Lbs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year



THE POLLUTANT OF CONCERN (POC) CREDITING FOR THIS OUTFALL RESTORATION PROJECT WAS PERFORMED UNDER PROTOCOL 5 AND IN ACCORDANCE WITH THE GUIDANCE MEMO "RECOMMENDATIONS FOR CREDITING OUTFALL AND GULLY STABILIZATION PROJECTS IN THE CHESAPEAKE BAY WATERSHED", DATED OCTOBER 15, 2019. SITE SAMPLES WERE COLLECTED ON 07/13/2022 AND ANALYZED BY WAYPOINT ANALYTICAL ON 07/22/2022. THE SOIL SAMPLE BULK DENSITY WAS 58.68 LB/FT³ AND THE CONCENTRATIONS WERE 0.90 LBS OF PHOSPHORUS PER 1 TON OF SEDIMENT AND 2.60 LBS OF NITROGEN PER 1 TON OF SEDIMENT. THROUGH IN-SITU SITE OBSERVATIONS, THE OUTFALL CHANNEL BED WAS ASSUMED TO HAVE A COHESIVE BED PLACING THE EQUILIBRIUM SLOPE UNDER BED CONDITION 1. THE EQUILIBRIUM SLOPE WAS FOUND TO BE 1.33%. THE TOTAL VOLUME OF PREVENTED SEDIMENT WAS OBTAINED THROUGH A COMPARISON OF THE EXISTING CHANNEL CONDITIONS WITH THE USE OF SURFACE COMPARISON MODELING IN AUTODESK CIVIL 3D SOFTWARE. A TOTAL PREVENT SEDIMENT VOLUME (SV) OF 7,675.56 CUBIC FEET WAS OBTAINED. BASED ON THE PREVENTED SEDIMENT CALCULATIONS, THIS OUTFALL RESTORATION WILL PROVIDE 7,506.70 LB/YR OF SEDIMENT, 9.76 LB/YR OF PHOSPHORUS, AND 3.38 LB/YR OF NITROGEN.



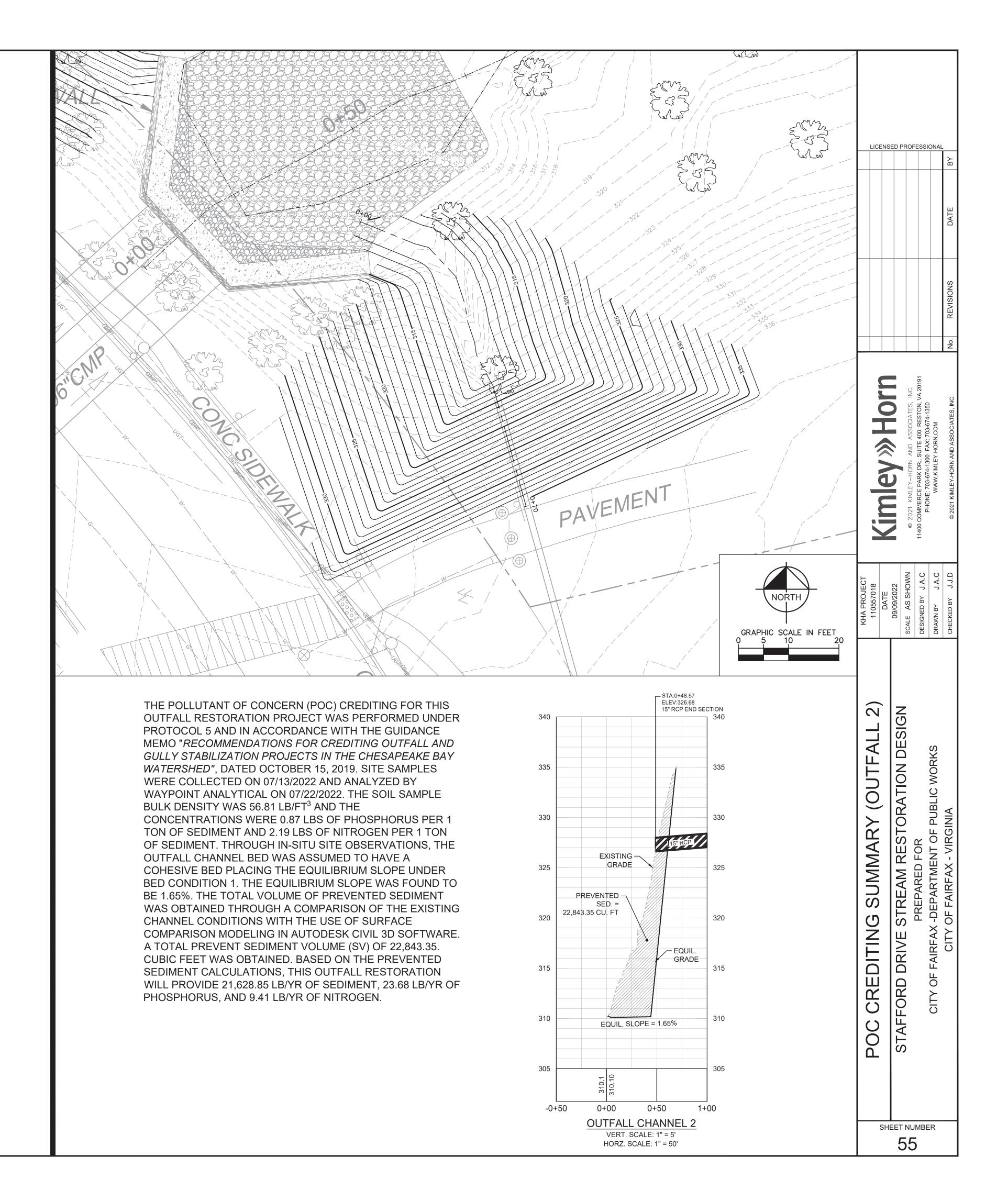
(OUTFALL SUMMARY CREDITING POC

7

SHEET NUMBER

54

1.15	ас
	km²
0.53	ft
	<i>C</i> •
	ft
	ft/ft
	ft
	ft
	ft
	lb./ft ³
re present upstream of the restoration	Yes
troom Limit	
• • •	ft
rium Bed Slope	
Bed Condition 1	
Cohesive Bed	
Sand and Fine Grave (0.1-5mm	particle size)
Beds Coarser than Sand (>5mm	particle size)
ion 1: Cohesive Bed	
= 0.0028A ^{-0.33}	
0.0165	ft/ft
and Fine Gravel	3 / 3 /
	f+ /f+
	ft/ft
	ft/ft
ium Bank Slopes	
	-
, ,	· ·
	ft
Shows at Caradition Familibuture Characal	Condition
Channel Condition - Equilibrium Channel	Condition
846.05	Cu. Yd.
846.05	Cu. Yd.
846.05 22,843.35	Cu. Yd. Cu. ft.
846.05 22,843.35 Volume to Annual Prevented Sediment L	Cu. Yd. Cu. ft.
846.05 22,843.35 Volume to Annual Prevented Sediment Lens in Efficiency and Timescale	Cu. Yd. Cu. ft.
846.05 22,843.35 Volume to Annual Prevented Sediment Lensin Efficiency and Timescale 10.5 (S _V / 30)	Cu. Yd. Cu. ft. oad
846.05 22,843.35 Volume to Annual Prevented Sediment Landin Efficiency and Timescale 50.5 (S _V / 30) 380.72	Cu. Yd. Cu. ft. oad
846.05 22,843.35 Volume to Annual Prevented Sediment Lensin Efficiency and Timescale 10.5 (S _V / 30)	Cu. Yd. Cu. ft. oad
846.05 22,843.35 Volume to Annual Prevented Sediment Landin Efficiency and Timescale 50.5 (S _V / 30) 380.72	Cu. Yd. Cu. ft. oad Cu. ft. / year
846.05 22,843.35 Volume to Annual Prevented Sediment Lensin Efficiency and Timescale 0.5 (S _V / 30) 380.72 Soils Bulk Density	Cu. Yd. Cu. ft. oad Cu. ft. / year
846.05 22,843.35 Volume to Annual Prevented Sediment Lens in Efficiency and Timescale 30.5 (S _V / 30) 380.72 Soils Bulk Density ual Volume of Prevented Sediment * Bulk	Cu. Yd. Cu. ft. oad Cu. ft. / year Density
846.05 22,843.35 Volume to Annual Prevented Sediment Lens in Efficiency and Timescale 30.5 (S _V / 30) 380.72 Soils Bulk Density ual Volume of Prevented Sediment * Bulk Not Applicable	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year
846.05 22,843.35 Volume to Annual Prevented Sediment Lender in Efficiency and Timescale 30.5 (S _V / 30) 380.72 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 21,628.85	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year
846.05 22,843.35 Volume to Annual Prevented Sediment Lendin Efficiency and Timescale 30.5 (S _V / 30) 380.72 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
846.05 22,843.35 Volume to Annual Prevented Sediment Length in Efficiency and Timescale 30.5 (S _v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients Conversion Factors	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
846.05 22,843.35 Volume to Annual Prevented Sediment Length in Efficiency and Timescale 30.5 (S v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 Annual Prevented Nutrients Conversion Factors 1 ton of sediment	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
846.05 22,843.35 Volume to Annual Prevented Sediment Length in Efficiency and Timescale 30.5 (S _V /30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
846.05 22,843.35 Volume to Annual Prevented Sediment Length in Efficiency and Timescale 20.5 (S _V / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
846.05 22,843.35 Volume to Annual Prevented Sediment Learnin Efficiency and Timescale 30.5 (S v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Length in Efficiency and Timescale 20.5 (S v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable It Adjusted Results 56.81	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Land in Efficiency and Timescale 20.5 (S v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Ic Adjusted Results 56.81 2.19	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Length in Efficiency and Timescale 20.5 (S v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable It Adjusted Results 56.81	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Land in Efficiency and Timescale 20.5 (S v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Ic Adjusted Results 56.81 2.19	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Landin Efficiency and Timescale 20.5 (S , / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 56.81 2.19 0.87 21,628.85	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Letter in Efficiency and Timescale 20.5 (S , / 30) 380.72 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 E Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 56.81 2.19 0.87 21,628.85 23.68	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Letter in Efficiency and Timescale 20.5 (S , / 30) 380.72 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 56.81 2.19 0.87 21,628.85 23.68 9.41	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Letter in Efficiency and Timescale 20.5 (S v / 30) 380.72 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 56.81 2.19 0.87 21,628.85 23.68 9.41 (POC) Crediting Summary	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ib. of (P) Ib. of (N) Ibs./year Ibs./year Ibs./year Ibs./year
846.05 22,843.35 Volume to Annual Prevented Sediment Letter in Efficiency and Timescale 20.5 (S , / 30) 380.72 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 21,628.85 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 56.81 2.19 0.87 21,628.85 23.68 9.41	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
	Existing Channel Conditions 48.57 0.28 2.40 2.70 6.87 84.28 Willibrium Channel Conditions The present upstream of the restoration Attream Limit The present Upstream of the restoration The present Upstream of the restoration Attream Limit The present Upstream of the restoration The present Upstream of Upstream of the restoration The present Upstream





Appendix O. Ashley Pond Conservancy Wet Pond Enhancement Calculations

ASHBY POND CONSERVANCY WET POND ENHANCEMENT PLANS (30% DESIGN)

9817 ASHBY ROAD, FAIRFAX, VA, 22031 PIN#: 58 1 03 000 A CITY OF FAIRFAX, VA

CONTRACTORS SHALL NOTIFY OPERATORS WHO MAINTAIN UNDERGROUND UTILITY LINES IN THE AREA OF

UTILITY CON	TACTS		
GAS	COLUMBIA GAS TRANSMISSION CORP.	(703) 327-6331	
	WASHINGTON GAS	(800) 752-7520	
	CNG TRANSMISSION CORP.	(814) 583-5171	
ELECTRIC	DOMINION VIRGINIA POWER	(888) 667-3000	MICO LITH ITY
	NOVEC	(888) 335-0500	MISS UTILITY DIAL 811, OR 1-800-552-
TELEPHONE	AT&T	(800) 288-2747	BEFORE DIGGING
	VERIZON	(800) 256-4646	
CABLE	COMCAST	(888) 375-4888	
WATER & SEWER	FAIRFAX WATER	(703) 698-5800	
OTHER	CENTURY LINK	(800) 366-8201	

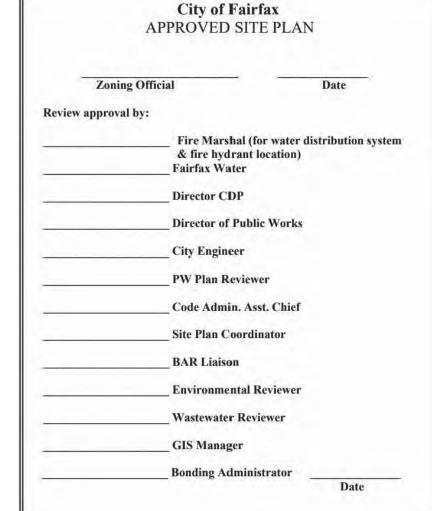
NON-EMERGENCY

POLICE: (703) 385-7924 FIRE AND RESCUE: (703) 385-7940 (FOR EMERGENCY CALL: 911)

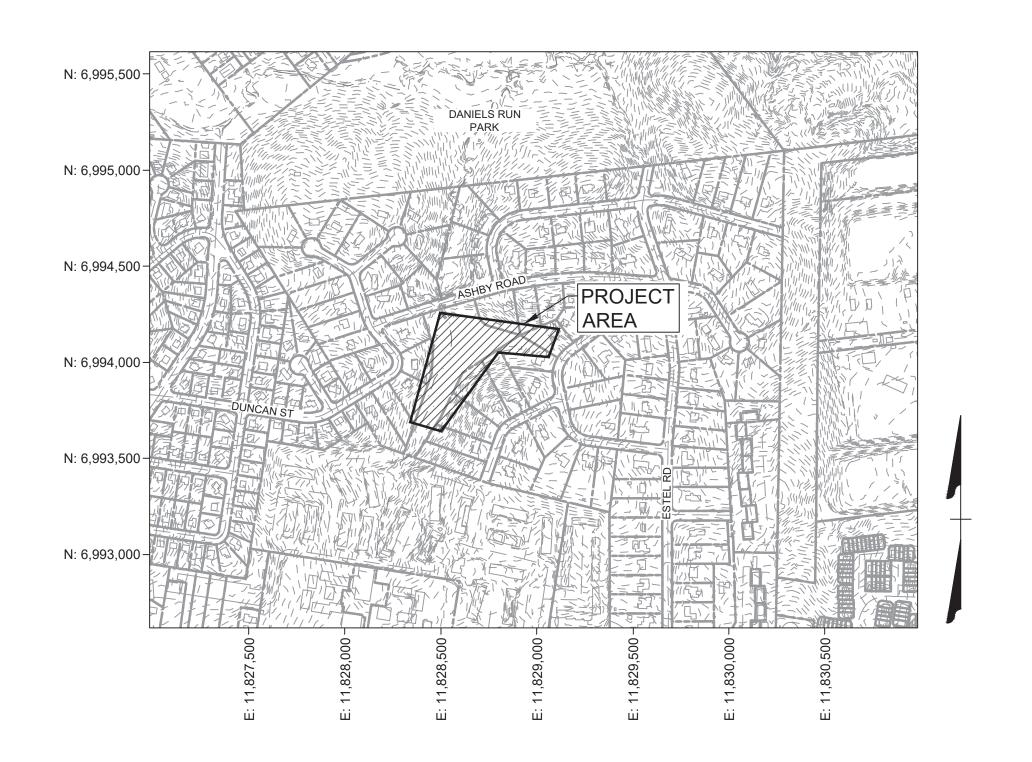
AGENT AUTHORIZATION LETTER To Whom IT May Concern identified below do hereby authorize , to act as my/our agent(s) in the furtherance of an Tax Map No: Thank you in advance for your cooperation. The forgoing instrument was acknowledged before me this _____ day of ___

AFFIX NOTARY SEAL/STAMP

Notary Public (Signature)



LOCATION MAP



VICINITY MAP

SCALE: 1'' = 500'

HORIZONTAL DATUM: NAD 83 VERTICAL DATUM: NGVD29

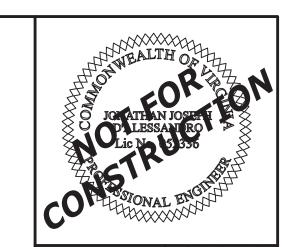
CITY OF FAIRFAX DEPARTMENT OF PUBLIC WORKS 10455 ARMSTRONG ST FAIRFAX, VA 22030 CONTACT: SATOSHI ETO PHONE: (703) 273 6073

CIVIL ENGINEER: TIMMONS GROUP 20110 ASHBROOK PLACE, SUITE 100 ASHBURN, VA 20147 CONTACT: JON D'ALESSANDRO, P.E. PHONE: (703) 554-6713

PROJECT NARRATIVE

(TMDL) REQUIREMENTS. A PRELIMINARY CHESAPEAKE BAY TMDL POLLUTANT OF CONCERN (POC) REDUCTION ANALYSIS HAS BEEN

Sheet List Table				
Sheet Sheet Title				
Number				
0.0	COVER			
1.0	LEGENDS & SYMBOLS			
1.1	GENERAL NOTES			
1.2	PERMIT CORRESPONDENCE			
2.0	EXISTING CONDITIONS			
3.0	PHOTOSTATION LOCATION MAP			
4.0	BATHYMETRIC SURVEY - TOP OF SILT			
4.1	BATHYMETRIC SURVEY - BOTTOM OF SILT			
4.2	PRELIMINARY DREDGING VOLUMETRIC ANALYSIS			
5.0	EROSION AND SEDIMENT CONTROL PHASE I			
5.1	EROSION AND SEDIMENT CONTROL PHASE II			
5.2	EROSION AND SEDIMENT CONTROL NOTES AND DETAILS			
5.3	EROSION AND SEDIMENT CONTROL NOTES AND DETAILS			
5.4	EROSION AND SEDIMENT CONTROL NOTES AND DETAILS			
5.5	EROSION AND SEDIMENT CONTROL NOTES AND DETAILS			
6.0	PRELIMINARY LAYOUT AND GRADING PLAN			
6.1	30% GRADING PROFILE			
7.0	EXISTING CONDITIONS HYDROLOGY			
7.1	EXISTING CONDITIONS HYDROLOGY - TR55			
7.2	POND ROUTING CALCULATIONS AND ANALYSIS			
7.3	CREDITING SUMMARY			
8.0	HISTORIC PLANS			
8.1	HISTORIC PLANS			
23	TOTAL SHEETS			



12/15/2020 DESIGNED BY

CHECKED BY

45558.014 SHEET NO.



Pollution Reduction Calculation Methodology narrative

The pollutant reduction calculations for the Ashby Pond Wet Pond Enhancements project were determined multiple ways due to the different components of the project. A cumulative summary of the pollutant reductions provided by the proposed restoration and enhancement is shown in Table 1.

Table 1. Ashby Pond Wet Pond Enhancement Project Pollutant of Concern (POC) Reduction Summary

Ashby Pond Potential Project(s) and corresponding estimated Chesapeake Bay Total Maximum Daily Load (TMDL) - Pollutant of Concern (POC) Load Reduction Summary					
Pollutant of Concern (POC)	Project 1 Ashby Pond Outfall Channel Restoration	Project 2 Restoration of Ashby Pond to 2011 (Original) Design Conditions	Total estimated POC Reductions provided by Projects 1 and 2		
Est. Sediment (TSS) Removal (lbs./yr.)	27,662.76	20,000.00	47,662.76		
Est. Phosphorous (P) Removal (Ibs./yr.)	14.52	73.00	87.52		
Est. Nitrogen (N) Removal (lbs./yr.)	31.54	320.00	351.54		
Estimated Pollutant of Concern Reduction Crediting Source	Channel 2 - Outfall Restoration (30% Design) - Prepared by Timmons Group (July 2020)	Ashby Pond Demonstration Project Plans - Prepared by William H. Gordon Associates, et.al. (January 2011)	Notes: These POC reductions are preliminary estimates only. Future iterations of design and analysis will further refine these numbers, and could potentially increase the POC reductions provided by each potential project.		

Narratives for the Outfall Channel 2 Restoration, as well as Pond Restoration and Enhancement are outlined below.

Outfall Channel 2 Restoration – Crediting Narrative

Crediting for the Outfall Channel 2 Restoration was performed utilizing the methodologies outlined in Protocol 5 (*Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed*). Calculation methodologies and preliminary crediting for the outfall restoration can be found in the Plan Set Assemblies located in the Section F Appendix.

Pond Restoration, Enhancement, and Retrofit

In determining a calculation methodology for the pond, consideration of the pond being credited, designed, and constructed in 2010 – 2011 during the infancy of the Virginia Runoff Reduction Method (VRRM) and BMP Clearinghouse Specification Development cannot be ignored. During this time there was a loose interpretation of design regulations, standards, and calculation methodologies because of the change from the Technical II.C Design Criteria to the Technical II.B Design Criteria.



DEQ Virginia Runoff Reduction Method New Development Compliance Spreadsheet - Version 3.0

■2011 BMP Standards and Specifications 2013 Draft BMP Standards and Specifications

Project Name: Ashby Pond Wet Pond Enhancements - SLAF Grant Section E Date: 7/14/2021 BMP Design Specifications List: 2013 Draft Stds & Specs

CLEAR ALL (Ctrl+Shift+R)

data input cells constant values calculation cells

Site Information

Post-Development Project (Treatment Volume and Loads)

Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) undisturbed,					0.00
protected forest/open space or reforested land	0.00	0.00	0.00	0.00	0.00
Managed Turf (acres) — disturbed, graded for yards or other turf to be mowed/managed	0.00	7.14	53.86	23.16	84.16
Impervious Cover (acres)	0.00	0.30	13.56	37.82	51.68
			•		135.84

Constants

Annual Rainfall (inches)	43
Target Rainfall Event (inches)	1.00
Total Phosphorus (TP) EMC (mg/L)	0.26
Total Nitrogen (TN) EMC (mg/L)	1.86
Target TP Load (lb/acre/yr)	0.41
Pj (unitless correction factor)	0.90

Runoff Coefficients (Rv)

	A Soils	B Soils	C Soils	D Soils
Forest/Open Space	0.02	0.03	0.04	0.05
Managed Turf	0.15	0.20	0.22	0.25
Impervious Cover	0.95	0.95	0.95	0.95

1,112.10

Post-Development Requirement for Site Area

TP Load Reduction Required (lb/yr) 99.76

LAND COVER SUMMARY -- POST DEVELOPMENT

Land Cover Summary	
Forest/Open Space Cover (acres)	0.00
Weighted Rv (forest)	0.00
% Forest	0%
Managed Turf Cover (acres)	84.16
Weighted Rv (turf)	0.23
% Managed Turf	62%
Impervious Cover (acres)	51.68
Rv (impervious)	0.95
% Impervious	38%
Site Area (acres)	135.84
Site Rv	0.50

Treatment Volume and Nutrient Loads		
Treatment Volume (acre-ft)	5.6800	
Treatment Volume (cubic feet)	247,423	
TP Load (lb/yr)	155.46	
TN Load (lb/yr)	1.112.10	

(Informational Purposes Only)



Appendix P. Van Dyck Park Outfall Restoration Calculations

30% CONSTRUCTION PLANS VAN DYCK PARK OUTFALL AND GULLY STABILIZATION PROJECT

PIN#: 57 2 02 176 & 57 2 02 175 3720 BLENHEIM BOULEVARD CITY OF FAIRFAX, VIRGINIA

VICINITY MAP

PROJECT NARRATIVE

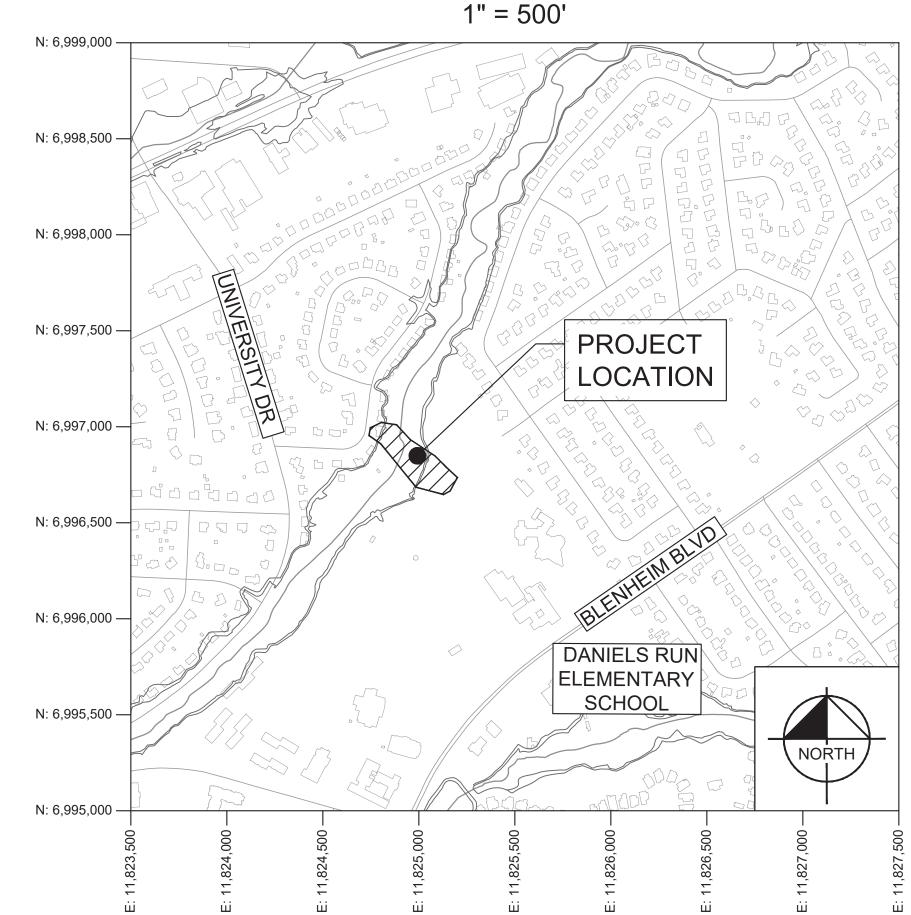
THIS PROJECT CONSISTS OF THE STABILIZATION AN ACTIVELY ERODING OUTFALL CHANNEL. THE PROJECT LIMITS BEGIN AT THE DISCHARGE OF A 15" RCP PIPE AND END AT THE CONFLUENCE OF ACCOTINK CREEK. THE PROJECT IS LOCATED IN VAN DYCK PARK IN THE CITY OF FAIRFAX, VIRGINIA.

THE POLLUTANT OF CONCERN (POC) CREDITING AND DESIGN FOR THE OUTFALL WAS DONE IN ACCORDANCE WITH THE GUIDANCE MEMO "RECOMMENDATIONS FOR CREDITING OUTFALL AND GULLY STABILIZATION PROJECTS IN THE CHESAPEAKE BAY WATERSHED", DATED OCTOBER 15, 2019.REPRESENTATIVE SOIL FIELD SAMPLES WERE OBTAINED FROM THE PROJECT SITE AND PROCEED AT A LABORATORY TO OBTAIN THE SOILS BULK DENSITY, NITROGEN CONCENTRATION.

THE SOIL SAMPLE BULK DENSITY WAS 62.43 LB/FT³ AND THE CONCENTRATIONS WERE 1.08 LBS OF PHOSPHORUS PER 1 TON OF SEDIMENT AND 1.78 LBS OF NITROGEN PER 1 TON OF SEDIMENT. THE POLLUTANT OF CONCERN CREDIT REDUCTION FROM THIS PROJECT IS 150,862.10 LBS/YR OF TOTAL SUSPENDED SOLIDS (TSS), 134.27 LBS/YR OF NITROGEN AND 81.47 LBS/YR OF PHOSPHORUS.

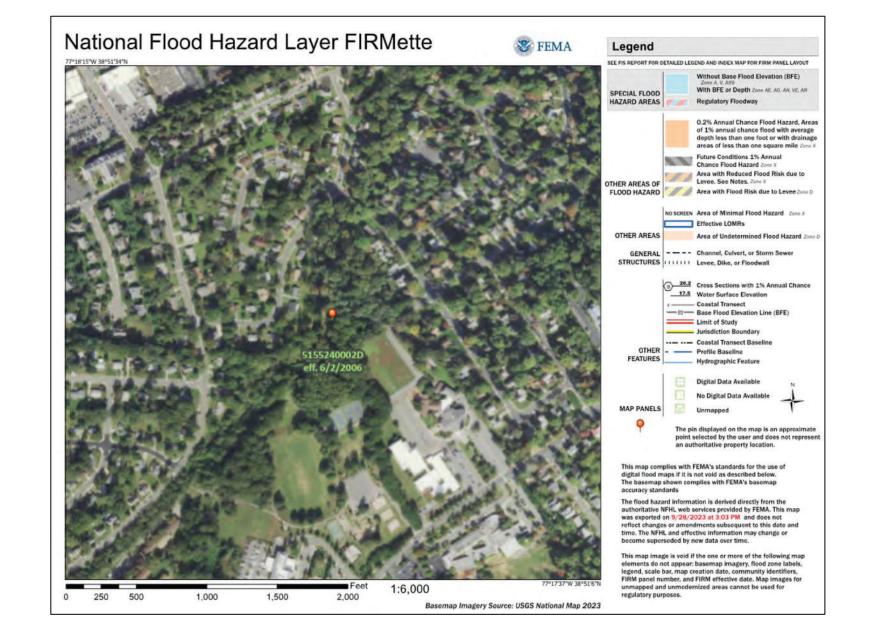
GENERAL NOTES:

- 1. THE SUBJECT PROPERTY OF THIS PROJECT IS THE FOLLOWING: TAX MAP NUMBER: 57 2 02 176 & 57 2 02 175 PARCEL AREA: 8.87 ACRES (386,380 SF) & 13.21 ACRES (575,430 SF)
- TOPOGRAPHIC INFORMATION SHOWN IS BASED ON THE READILY AVAILABLE GEOGRAPHIC INFORMATION SYSTEM (GIS) FOR THE PROJECT AREA. THE SITE IS INTENDED TO BE SURVEYED AS PART OF THE NEXT STAGE OF THE DESIGN PROCESS.
- 3. THE EXISTING UTILITIES, AS SHOWN HEREON, ARE APPROXIMATE ONLY. NO GUARANTEE IS HEREIN MADE OR IMPLIED THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT ALL UTILITY COMPANIES TO VERIFY THE TYPE, SIZE, AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO STARTING THE WORK. ANY DISCREPANCIES IN OR FROM THE INFORMATION SHOWN HEREON SHALL BE REPORTED TO KIMLEY-HORN.
- 4. THE AREA SHOWN HERON IS LOCATED ON THE FLOOD INSURANCE RATE MAP (FIRM), COMMUNITY PANEL NO. 5155240002D, WITH AN EFFECTIVE DATE OF JUNE 2, 2006. FIRM PANEL NO. 5155240002D INDICATES THAT THE PROJECT AREA IS NOT LOCATED IN A FEMA SPECIAL FLOOD HAZARD AREA (SFHA).

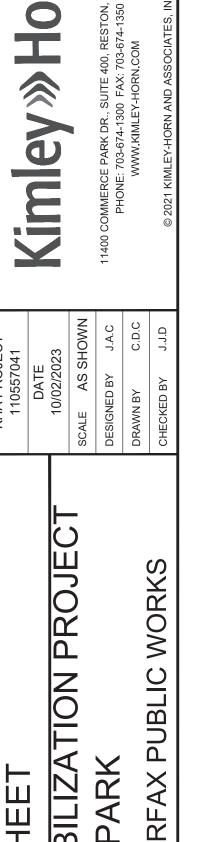


	OWNER	CLIENT	ENGINEER
NAME	CITY OF FAIRFAX	CITY OF FAIRFAX	KIMLEY-HORN
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589

	Sheet List Table		
Sheet Number	Sheet Title		
01	COVER SHEET		
02	GENERAL NOTES & DETAILS		
03	GENERAL NOTES & DETAILS		
04	PHOTO STATION MAP		
05	EXISTING CONDITIONS		
06	EXISTING HYDROLOGY		
07	PRELIMINARY POC CREDITING SUMMARY		







OUTF/

SHEET NUMBER



Pollution Reduction Calculation Methodology narrative

Preliminary crediting for the Van Dyck Park Outfall Restoration Projects was determined utilizing the crediting methodology outlined in the "Unified Guide for Crediting Stream and Floodplain Restoration Projects in the Chesapeake Bay Watershed" — specifically Protocol 5 (Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed). Calculation methodologies and crediting for the outfall restoration can be found in the Conceptual Plan Set Assembly located in the Section F Appendix. Table 1 outlines the Pollutant of Concern (POC) Reduction summary for the potential restoration of the outfall channel.

Table 1. Van Dyck Park – Outfall Restoration Project – Preliminary Pollutant of Concern Reduction Summary

Outfall-ID	Outfall Length (ft.)	Outfall Drainage Area (Ac.)	Estimated Phosphorous Reduction Provided (lbs./yr.)	Estimated Nitrogen Reduction Provided (lbs./yr.)	Estimated TSS Reduction Provided (Ibs./yr.)
Outfall 1	329.00	3.30	81.47	134.27	150,862.10

DEQ Virginia Runoff Reduction Method New Development Compliance Spreadsheet - Version 3.0

C 2011 BMP Standards and Specification

© 2013 Draft BMP Standards and Specification

Project Name:

Date:

9/20/2023

BMP Design Specifications List: 2013 Draft Stds & Specs

CLEAR ALL (Ctrl+Shift+R) data input cells
constant values
calculation cells
final results

Site Information

Post-Development Project (Treatment Volume and Loads)

Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) undisturbed,					1.04
protected forest/open space or reforested land	0.00	0.82	0.22	0.00	1.04
Managed Turf (acres) disturbed, graded for					1.30
yards or other turf to be mowed/managed	0.00	0.00	0.97	0.33	1.50
Impervious Cover (acres)	0.00	0.02	0.19	0.70	0.91
* Forest/Open Space areas must be protected in accordance with the Virginia Runoff Reduction Method				3.25	

Constants

Annual Rainfall (inches)	43
Target Rainfall Event (inches)	1.00
Total Phosphorus (TP) EMC (mg/L)	0.26
Total Nitrogen (TN) EMC (mg/L)	1.86
Target TP Load (lb/acre/yr)	0.41
Pj (unitless correction factor)	0.90

Runoff Coefficients (Rv)

	A Soils	B Soils	C Soils	D Soils
Forest/Open Space	0.02	0.03	0.04	0.05
Managed Turf	0.15	0.20	0.22	0.25
Impervious Cover	0.95	0.95	0.95	0.95

Post-Development Requirement for Site Area

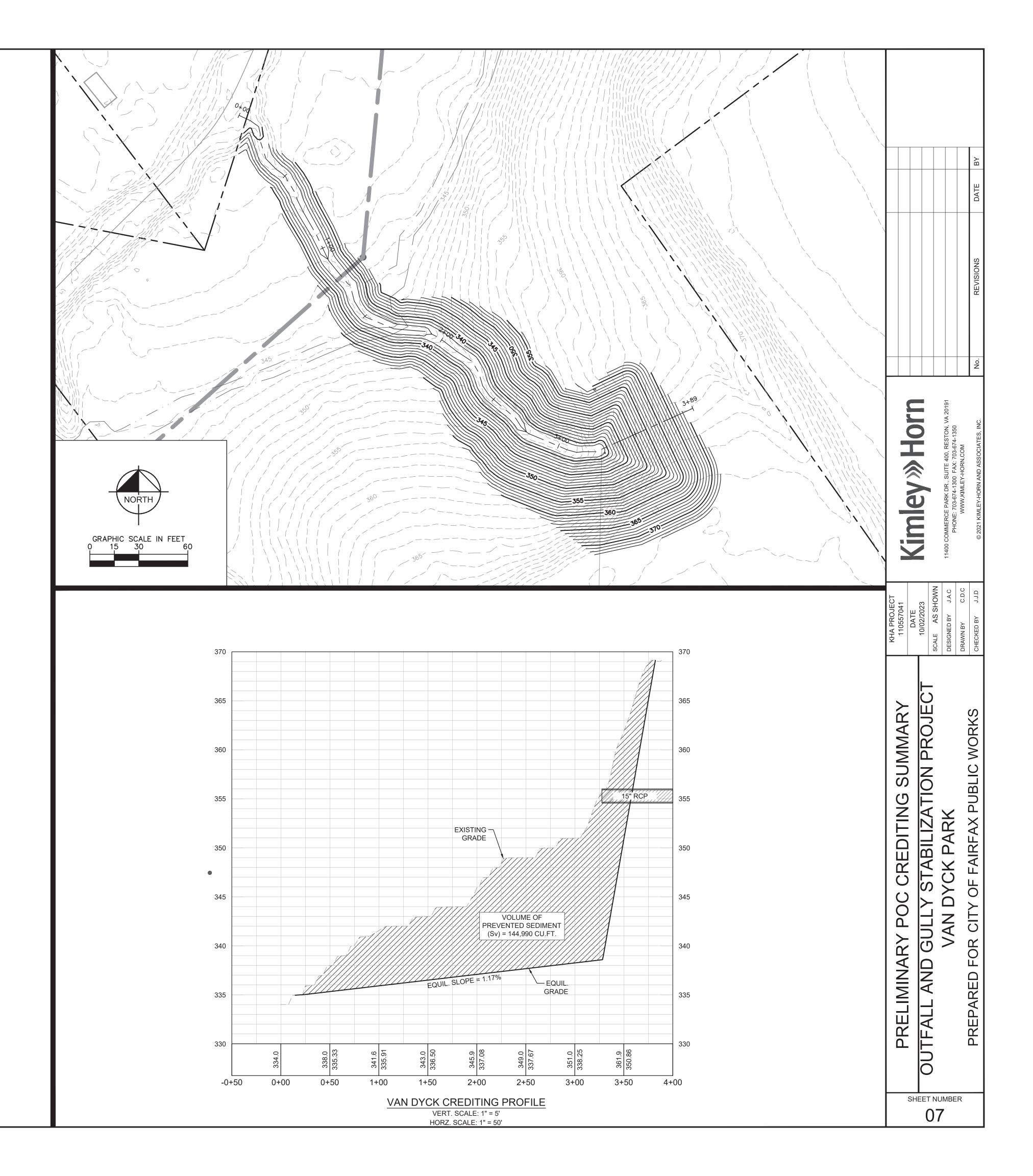
TP Load Reduction Required (lb/yr) 1.39

LAND COVER SUMMARY -- POST DEVELOPMENT

	OOTEROO		
Land Cover Summary			
Forest/Open Space Cover (acres)	1.04		
Weighted Rv (forest)	0.03		
% Forest	32%		
Managed Turf Cover (acres)	1.30		
Weighted Rv (turf)	0.23		
% Managed Turf	40%		
Impervious Cover (acres)	0.91		
Rv (impervious)	0.95		
% Impervious	28%		
Site Area (acres)	3.25		
Site Rv	0.37		
	<u> </u>		

Treatment Volume and Nutrien	t Loads
Treatment Volume (acre-ft)	0.0997
Treatment Volume (cubic feet)	4,341
TP Load (lb/yr)	2.73
TN Load (lb/yr)	19.51

Existing Outfall Char		
Drainage Area (A _d)=	3.28	ac
Drainage Area (A _d)=	0.0133	km ²
Mean Flow Depth =	0.433	ft
	existing Channel Conditions	
Length of Proposed Reach = Channel Slope =	328.640 0.063	ft ft/ft
Bank Height =	2.80	ft
Bottom Width =	5.57	ft
Top Width =	18.43	ft
Bulk Density (Estimate) =	70.00	lb./ft ³
	uilibrium Channel Conditions	,
Is there a pipe outfall or other defining infrastructure site?	e present upstream of the restoration	Yes
Ups	tream Limit	
L _{ma}	_{ax} = 153A _d ^{0.6}	
Maximum Upstream Channel Length (L _{max}) =	Not Applicable	ft
	rium Bed Slope	, , , , , , , , , , , , , , , , , , ,
Choose Bed Condition =	Bed Condition 1	
Bed Condition 1 =	Cohesive Bed	
Bed Condition 2 =	Sand and Fine Grave (0.1-5mm	particle size)
Bed Condition 3 =	Beds Coarser than Sand (>5mm	· · · · · · · · · · · · · · · · · · ·
Bed Conditi	on 1: Cohesive Bed	·
S _{PR} =	= 0.0028A ^{-0.33}	
Equilibrium Slope (S _{eq})=	0.0117	 ft/ft
1 1 1	2: Sand and Fine Gravel	3-73-
	.06 / (y * 62.43)	
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
	: Bed Coarser than Sand	7.771
Equilibrium Slope (S _{eq})=	Not Applicable	 ft/ft
	ium Bank Slopes	<i>Jt/Jt</i>
Bank Slopes =	ин винк эторез	_
·	ttom Width (est)	
Bottom Width =	, ,	
	5.5	ft
	5.5 e Total Prevented Sediment	ft
	e Total Prevented Sediment	
Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate	e Total Prevented Sediment hannel Condition - Equilibrium Channe	l Condition
Step 3: Calculate the Volume of Prevented Sediment = Existing Column of Prevented Sediment (S_v) =	e Total Prevented Sediment Channel Condition - Equilibrium Channe 5,370.00	I Condition Cu. Yd.
Step 3: Calculate the Volume of Prevented Sediment = Existing Column of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) =	E Total Prevented Sediment Channel Condition - Equilibrium Channe 5,370.00 144,990.00	I Condition Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Column of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V	E Total Prevented Sediment Shannel Condition - Equilibrium Channe 5,370.00 144,990.00 /olume to Annual Prevented Sediment L	I Condition Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate the Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Values of Reduction	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 Volume to Annual Prevented Sediment Lens in Efficiency and Timescale	I Condition Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Column of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction $S_p = S_p $	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Let in Efficiency and Timescale 0.5 (S v / 30)	Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate the Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = $Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ S_p = $	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50	Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate the Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = $Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ S_p = $	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Let in Efficiency and Timescale 0.5 (S v / 30)	Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate the Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = $Step \ 4: Convert \ the \ Total \ Sediment \ Volume \ S_p = $	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 Yolume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density	Cu. Yd. Cu. ft. Coad Cu. ft. / year
Step 3: Calculate the Volume of Prevented Sediment = Existing Convert to Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S_p) = Annual Volume of Prevented Sediment (S_p) = Adjust for Reduction (S_p)	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 Yolume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density	Cu. Yd. Cu. ft. Coad Cu. ft. / year
Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate the Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S_p) = Adjust for Reduction S_p = Adjust for Adjust for Annual Volume of Prevented Sediment Load = Annual	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density and Volume of Prevented Sediment * Bulk	Cu. Yd. Cu. ft. Cu. ft. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Calculate the Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S_p) = Annual Volume of Prevented Sediment (S_p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) =	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Cu. ft. Cu. ft. / year
Volume of Prevented Sediment = Existing Converted Sediment (S_v) = Volume of Prevented Sediment (S_v) = $Step 4$: Convert the Total Sediment Volume of Prevented Sediment (S_p) = $S_p = S_p = $	Shannel Condition - Equilibrium Channe 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Cu. ft. Cu. ft. / year
$Step \ 3: \ Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Calculate $	Shannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lentin Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment	Cu. Yd. Cu. ft. Coad Cu. ft. / year Ib./year Ib./year
$Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Step \ 4: \ Convert \ the \ Total \ Sediment \ V$ $Adjust \ for \ Reduction$ $S_p =$ $Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) =$ $Adjust \ for \ Sediment \ (S_p) =$ $Adjust \ for \ Sediment \ Se$	Shannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Letter in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Joad Cu. ft. / year k Density Ib./year Ib./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p) = Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Adjust for Adjust for Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Sediment Load (Policy Sediment Load (P	Shannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lettin in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Jean Cu. ft. / year Ib./year Ib./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p) = Adjust for Reduction (S _p) = Adjust for Adjust for Adjust for Adjust for Adjust for Sediment Load (Estimate) = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Sediment Columns) Estimated Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate =	Shannel Condition - Equilibrium Channe 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable Not Applicable	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Joad Cu. ft. / year k Density Ib./year Ib./year
$Volume\ of\ Prevented\ Sediment = Existing\ Colume of\ Prevented\ Sediment\ (S_v)=$ $Volume\ of\ Prevented\ Sediment\ (S_v)=$ $Step\ 4:\ Convert\ the\ Total\ Sediment\ V$ $Adjust\ for\ Reduction$ $S_p=$ $Annual\ Volume\ of\ Prevented\ Sediment\ (S_p)=$ $Adjust\ for\ Sediment\ (S_p)=$ $Adjust\ for\ Sediment\ (S_p)=$ $Annual\ Prevented\ Sediment\ Load\ (Estimate)=$ $Annual\ Prevented\ Sediment\ Load\ (Field\ Verified)=$ $Step\ 5:\ Determine\ the\ Sediment\ Sedim$	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Ital Adjusted Results	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Cu. ft./year Ib./year Ib./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p) = Adjust for Reduction (S	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 Yolume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Se Adjusted Results 62.43	Cu. Yd. Cu. ft. Cu. ft. Coad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p) = Adjust for Reduction (S _p) = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (N) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specifier (P) = 1 ton of sediment =	shannel Condition - Equilibrium Channe 5,370.00 144,990.00 /olume to Annual Prevented Sediment Letting in Efficiency and Timescale 0.5 (S , / 30) 2,416.50 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable ic Adjusted Results 62.43 1.08	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Cu. ft./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p)= Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated of Prevented Sediment Load (Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specifier Specifier Sediment = 1 ton of sediment =	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 Yolume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Se Adjusted Results 62.43	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Cu. ft./year Ib./year Ibs./year Ibs./year Ibs./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _ν) = Step 4: Convert the Total Sediment Volume of Prevented Sediment Volume of Prevented Sediment (S _ν) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _ν) = Adjust for Reduction S _ν = Annual Volume of Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specifier Specifier Site Adjusted Total Suspended Solids (TSS) Removal Site Adjusted Total Suspended Solids (TSS) Removal	shannel Condition - Equilibrium Channe 5,370.00 144,990.00 /olume to Annual Prevented Sediment Letting in Efficiency and Timescale 0.5 (S , / 30) 2,416.50 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable ic Adjusted Results 62.43 1.08	Cu. Yd. Cu. ft. Cu. ft. Cu. ft. Cu. ft./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p) = Adjust for Reduction (S _p) = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Total Sediment (P)) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification of Sediment = 1 ton of sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate =	Soils Bulk Density I ton of sediment On the Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable 150,862.10 100 Applicable 100 Applicable	Cu. Yd. Cu. ft. Cu. ft. coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment Volume of Prevented Sediment (S _p) = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Tield Verified) = Step 5: Determine the Estimated (Pield Verified) = Step 5: Determine the Estimate	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 62.43 1.08 1.78 150,862.10 81.47	Cu. Yd. Cu. ft. Cu. ft. coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment Volume of Prevented Sediment (S _p)= Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Pield Verified) = Step 5: Determine the Estimated of Sediment (N) = Estimated Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Site Specifi Bulk Density = 1 ton of sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate =	Shannel Condition - Equilibrium Channe 5,370.00 144,990.00 Volume to Annual Prevented Sediment II In in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Soils Adjusted Results 62.43 1.08 1.78 150,862.10 81.47 134.27	Cu. Yd. Cu. ft. Cu. ft. coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S _p) = Adjust for Reduction S _p = Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Coad (Prevented Sediment C	thannel Condition - Equilibrium Channel 5,370.00 144,990.00 /olume to Annual Prevented Sediment In in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable ic Adjusted Results 62.43 1.08 1.78 150,862.10 81.47 134.27 1 (POC) Crediting Summary	Cu. Yd. Cu. ft. Cu. ft. coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ib. of (P) Ib. of (N) Ibs./year Ibs./year Ibs./year
Step 3: Calculate the Volume of Prevented Sediment = Existing Color Volume of Prevented Sediment (S _v)= Volume of Prevented Sediment (S _v)= Step 4: Convert the Total Sediment Volume of Prevented Sediment Volume of Prevented Sediment (S _p)= Annual Volume of Prevented Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Field Verified) = Step 5: Determine the Estimated of Sediment Load (Pield Verified) = Step 5: Determine the Estimated of Sediment (N) = Estimated Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Site Specifi Bulk Density = 1 ton of sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate =	Shannel Condition - Equilibrium Channe 5,370.00 144,990.00 Volume to Annual Prevented Sediment II In in Efficiency and Timescale 0.5 (S v / 30) 2,416.50 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 150,862.10 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Soils Adjusted Results 62.43 1.08 1.78 150,862.10 81.47 134.27	Cu. Yd. Cu. ft. Cu. ft. coad Cu. ft. / year Ib./year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ib. of (P) Ib. of (N) Ibs./year





Appendix Q. Traveler Street Outfall Restoration Calculations

30% CONSTRUCTION PLANS **OLD ROBIN STREET** (FORMALLY TRAVELER STREET) OUTFALL AND GULLY STABILIZATION PROJECT

PIN#: 47 4 01 039 3157 FAIR WOODS PKWY CITY OF FAIRFAX, VIRGINIA

PROJECT NARRATIVE

THIS PROJECT CONSISTS OF THE STABILIZATION OF TWO ACTIVELY ERODING OUTFALL CHANNELS

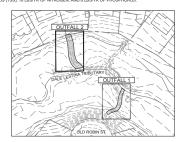
THE PROJECT LIMITS OF OUTFALL 1 BEGIN AT THE DISCHARGE OF A 15" RCP PIPE AND END AT THE CONFLUENCE OF THE OUTFALL CHANNEL WITH THE DUALE LESTINA TRIBUTARY: THE PROJECT LIMITS OF OUTFALL SEGN AT THE DISCHARGE OF A 21' RCP AND END AT THE CONFLUENCE OF THE OUTFALL CHANNEL WITH THE DISCHARGE OF A 21' LOCATED WITHIN DALE LESTINA PARK.

THE POLITANT OF CONCERN POC) CREDITING AND DESIGN FOR THE OUTFALL WAS DONE IN ACCIDENANCE WITH THE GUIDANCE MEMO FECOMENSATION FOR CREDITING OUTFALL AND GULF Y STRULEZATION PROJECTS IN THE CRESS-FEAR BAY WATERSHEET, DATED OCTOBER 15, 2019. REPRESENTATIVE SOIL FIELD SAMPLES WERE ORTANDED FROM THE PROJECT PROJECT OF THE OUTFALL OF THE PROJECT PROJECT OF THE PROJECT PROJE

THE SOIL SAMPLE RESULTS FOR OUTFALL 1 ARE AS FOLLOWS

- BULK DENSITY 64.3 LB/FT³
 0.88 LBS OF PHOSPHORUS PER 1 TON OF SEDIMENT
 2.11 LBS OF NITROGEN PER 1 TON OF SEDIMENT
- THE SOIL SAMPLE RESULTS FOR OUTFALL 2 ARE AS FOLLOWS

THE TOTAL POLLUTANT OF CONCERN CREDIT REDUCTION FROM BOTH OUTFALL LOCATIONS IS 14,300 LBS/YR OF TOTAL SUSPENDED SOLIDS (TSS), 16 LBS/YR OF NITROGEN, AND 6 LBS/YR OF PHOSPHORUS.



GENERAL NOTES

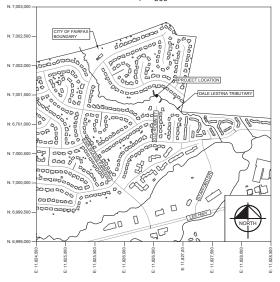
THE SUBJECT PROPERTY OF THIS PROJECT IS THE FOLLOWING

TAX MAP NUMBER: 47 4 01 039 PARCEL AREA: 7.78 ACRES (339.000 SF) ESTIMATED DISTURBED AREA: 0.66 ACRES

- TOPOGRAPHIC INFORMATION SHOWN IS BASED ON GROUND SURVEY PREPARED BY JOHNSON, MIRIAM, & THOMPSON (JMI ON OCTOBER 3, 2022. THE HORIZONTAL DATUM IS NADES WHILE THE VERTICAL DATUM IS NGVD29. THE GROUND SURVEYS (AVE BEEN SUPPLEMENTED WITH THE BEST AVAILABLE DATA FROM THE CITY'S OPEN GIS DATA HUB.
- THE DISTINGUITHERS, AS SHOWN HEREON, ARE APPROXIMATE ONLY NO GUARANTEE IS RESENTANCE OF INFILID THAT THE ALL ENSINGS UNDERGOAD UNTIL THAT ARE SHOWN OF HAVE BEEN AND FOR THAT THAT ALL ENSINGS UNDERGOAD UNTIL THAT ARE SHOWN OF THE AREA OF THE SHOWN OF THE SHOWN OF THE SHOWN OF THE SHOWN OF THE WORLD AND SHOWN OF THE S
- THE AREA SHOWN HERON IS LOCATED ON THE FLOOD INSURANCE RATE MAP (FIRM), COMMUNITY PANEL NO. 5155240002D WITH AN EFFECTIVE DATE OF JUNE 2, 2008. FIRM PANEL NO. 515524002D INDICATES THAT THE PROJECT AREA IS LOCATE! IN A FEMA SPECIAL FLOOD HAZARD AREA (SHAN) ZONE AE.

VICINITY MAP

1" = 500'



	OWNER	CLIENT	ENGINEER
NAME	CITY OF FAIRFAX	CITY OF FAIRFAX	KIMLEY-HORN
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589

Sheet List Table		
Sheet Number	Sheet Title	
01	COVER SHEET	
02	GENERAL NOTES & DETAILS	
03	GENERAL NOTES & DETAILS	
04	PHOTO LOCATION MAP - OUTFALL 1	
05	PHOTO LOCATION MAP - OUTFALL 2	
06	EXISTING CONDITIONS - OUTFALL 1	
07	EXISTING CONDITIONS - OUTFALL 2	
08	EXISTING HYDROLOGY	
09	POC CREDITING SUMMARY	



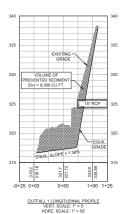


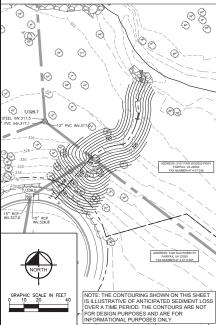
Kimley »Horn

Kimley≫Horn

) GULLY STABILIZATION PROJECT OLD ROBIN STREET SHEE

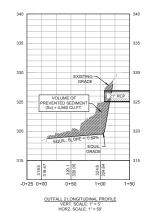
OUTFALL 1

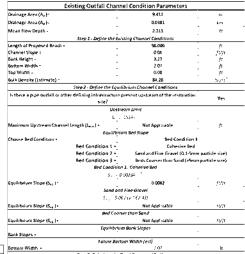


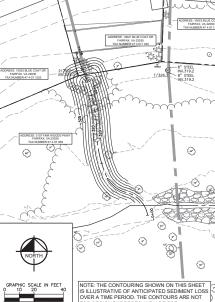


Existing Outfall	Channel	Condition Parameters	
Drainage Area (Aa)-		2.06	
Oralnage Area (A ₄)-	-	0.0063	·
Mean Flow Dench -	•	0.767	. "
	ha Eviesi		. "
Step 1 - Define Ength of Proposed Reach -	the even	ng Channel Conditions 69.110	· · · ·
ength of Proposed Reach - Channel Slope -	-	69.110	
hannel Slope - lank Height :	-	2.17	, f\(f \) t
sank Height : Softom Width -		2.21	· //
spreom sviens - rop Wichh ∸	-	6.53	. "
half Denvity (Extiracte) =		24.78	1570:
	t- Femilia	num Channel Candihons	E11.
is there a p-pe outlast or other detening intrastr			
is the relative policial or ocner deliming initiative		SOM MASCROAMS IN THE LESSON CONTRACTOR	Yes
	r Uptintos	_ 11	
	1 25		
العيناسيس Upstream Channel Length (لــــــ) - ا		Not Applicable	. tr
	guilibrium	Brd Slope	
Thorse Bed Condition :		Ged Condition L	
Bed Condition	n1=,	Cohesive Bed	
Bed Condition	n 2 = ,	Sand and Fine Gravel 10 1-5mm	
Bed Condition		Beds Coarser shan Sand I >Smr	particle site)
DFU LL		Cohesive Bed	
	5., 5.00		
qullibnym Slope (5 _H =	-	0.0136	f://r
	and and Fi		
5.	. 3,067	(v * 63 4))	
Equilibrium Slope (S _m) =	-	Not Applicable	ty/r
	ed Coarser	than Sond	
quilibrium Slope (5 _m) =		Not Applicable	ti/it
	eulibrium 6	lank Slopes	
Bank Slopes •	-		
	ure Bottom	Width (est)	'
Sorton Width -		7.79	16
Srep 3. Calcula	are the Fat	ol Prevented Sediment	
	_		
Volume of Prevented Sediment = Exist	log Chann	el Candilion - Equilibrium Channe	J Condition
		347 MI	Cu 54
Valume of Prevented Sedimon (S,)-		211.00	
followe of Prevented Sod-mam (S,)-		9,369.00	Ca B
		ne to Annual Prevented Sediment i	фрф
Adjust for Feet		(General and Tomorals	
	5 000		
Annual Volume of Prevented Sediment (5,) -		156.15	to ft Zwar
Adjo	of for Sails	Bulk Density	
Achyol Prevented Sediment Load (External) -	go phagaine	North Control of Strategy (1994) Mark Applicable	
Annual Prevented Sediment Load (Field Ventile)	di =	Not Applicable 10,040 45	9 Area
		roal Prevented Notinents	A 134.00
		ersvan Foetors	
LOS III. of Phospharus (P) -	Oleo co	Liter of Gistory at	
2.28 lb. of Narogen (N) -	-	Storiof reduces	
	-	Not Applicable	See Agree
	-	Nat Applicable	017,007
	oecific Adl	lusted Results	PI CESE
Esbinated Nirrogen (N) Removal Rate -		64.30	15 Apr. 1
Esbinated Nikrogen (N) Removal Rate - Site 5		0.26	0 of (P)
Estimated N-ringen (A) Removal Rane – Site 5, Bul's Density –			
Esbimated Historgen (M) Removal Rate – Site 5 Bulls Density – L'tim of sediment •		211	
Bulk Density – Litins of sediment + Litins of sediment =	-	2.31	10 of (A)
Estimated Hintegen (M) Removal Rate - Sile S Buts Density - Litimatis rediment - Litimatis rediment - Litimatis rediment - Siler Adjusted Total Suspended Solids (TSS) Rem	-	2.21.	io of INI in Arm
Estimated hisragen (M) Removal Rane - Site S But Density - Litina of vediment + Litina of sediment = Litina destinated Total Suspended Solids (TSS) Rem Rute =	-		to Aprile
Elbimated horragen (M) Removal Rare - SHE S, Buth Density - Ltins of Vadiment - Long of Vediment - Site Adjusted Tatal Surpended Solids (TSS) Rem Rate :	-	10,040.45	Sen Apenie Sen Apenie
Esbimated horizgen (M) Removal Rate – SHe S, But's Density – Ltons of vediment i – Ltons of vediment i – Like Adjusted Total Suspended Solids (TSS) Rem Like Adjusted Total Suspended Solids (TSS) Rem Like Adjusted Phosphonus (T) Removal Rate – Like Adjusted Phosphonus (T) Removal Rate –	noval	10,040.45 4.30 10.59	to Aprile
Esbimated heringen (M) Removal Raic - Sile 5 But's Density - Linius in Availiment = Linius in Availiment = Sile Adjusted Total Surjee aded Solids (TSS) Rem- Rote = Sile Adjusted Phosphonus (T) Permoval Raic = Diel Adjusted Microgen (M) Removal Raic = Poll Utant of Com	noval	10,040.45 4.30 10.59 DC) Crediting Summary	San Apena San Apena San Apena
Elbimated horizgen (M) Removal Ranc – Sité X, Bush Density – Line of sediment + Li	noval	10,040.45 4.30 10.59 DC) Crediting Summary 10,040.45	Sur Apenie Sur Apenie Sur Apenie
Esbimated heringen (M) Removal Raic - Sile 5 But's Density - Linius in Availiment = Linius in Availiment = Sile Adjusted Total Surjee aded Solids (TSS) Rem- Rote = Sile Adjusted Phosphonus (T) Permoval Raic = Diel Adjusted Microgen (M) Removal Raic = Poll Utant of Com	noval	10,040.45 4.30 10.59 DC) Crediting Summary	San Apena San Apena San Apena

OUTFALL 2







FOR DESIGN PURPOSES AND ARE FOR INFORMATIONAL PURPOSES ONLY.

1, 0	175,730)	
Annual Volume of Prevented Sediment (5,) •	76.05	(v.f: / rear
Adjust for So	lls Built Density	•
Acresa Principles Searchert (Cost. Acresa)	Victoria of Provented Sealment 1	Buy Density
Annual Prevented Sediment Load (Estimate) :	Not Applicable	5.7year
Annual Prevented Sed-more Load (Field Verified) -	4,273.25	5 Ayrılar
Step St Determine the A	naual Prevented Nutrients	
Et nimoned Co	eversion Fectors	
L.DS Ib. of Phosphorus (P) -	Lack of John	rent
2 281b, of Mitrogen (NI -	Liter of sedin	n, ni
Eso maned Phosphorus (P) Removal Race -	Not Applicable	10.7,001
Estimated Mitrogen NI Removal Rate =	Not Applicable	36) /year
Side Specific A	ldyusted Results	
But Density -	96 19	8.70
Ltan of sediment –	0.79	10 37 17,
Lton of sediment -	5.60	26 of (N)
Site Adjusted Tatal Suspended Solids (TSS) Removal Rate -	4,273.25	in Agene
Site Adjusted Phosphorus (P) Removal Race -	1.70	1017/401
Site Adjusted N trogen INI Removal Rate -	5 56	ien /year
Pollutant of Concern (POC) Crediting Summary	
Total Suspended Solids (TSS) Removal Rate -	4,273.25	3. Aprile
Phosphorus P -Removal Rate =	1.70	3.17000
ntragen (N Romoval Rate - 5.56		3a Zectic

Volume of Prevented Sediment - Existing Channel Condition - Equilibrium Channel Condition

Step 4: Convert the Total Sediment Volume to Annual Prevented Sediment Load
Adjust for Pediction in Efficiency and Timescale

164.00

4,963.00

Ca. Vd

Valume of Prevented Sed-mem [S].

Valume of Prevented Sediment [5,] -

	POC CREDITING SUMMARY	110557037	JECT 037	
SHI		DATE		
EE.	101.000.101.001.001.00	10/02/2023	023	
T NL	OUTFALL AND GULLY STABILIZATION PROJECT	SCALE AS	ASSHOWN	
JMBE	OLD ROBIN STREET	DESIGNED BY JJ.D	J.J.D	
R		DRAWN BY	MJM	
	PREPARED FOR CITY OF FAIRFAX PUBLIC WORKS	CHECKED BY	J.J.D	
ı			I	ı

09

Kimley»Horn



Appendix R. Providence Park Providence Park Outfall Restoration Calculations

30% CONSTRUCTION PLANS PROVIDENCE PARK OUTFALL AND GULLY STABILIZATION PROJECT

PIN#: 57 3 01 007 10715 WEST DR CITY OF FAIRFAX, VIRGINIA

VICINITY MAP

PROJECT NARRATIVE

THIS PROJECT CONSISTS OF THE STABILIZATION OF APPROXIMATELY AN ACTIVELY FRODING OUTFALL CHANNEL

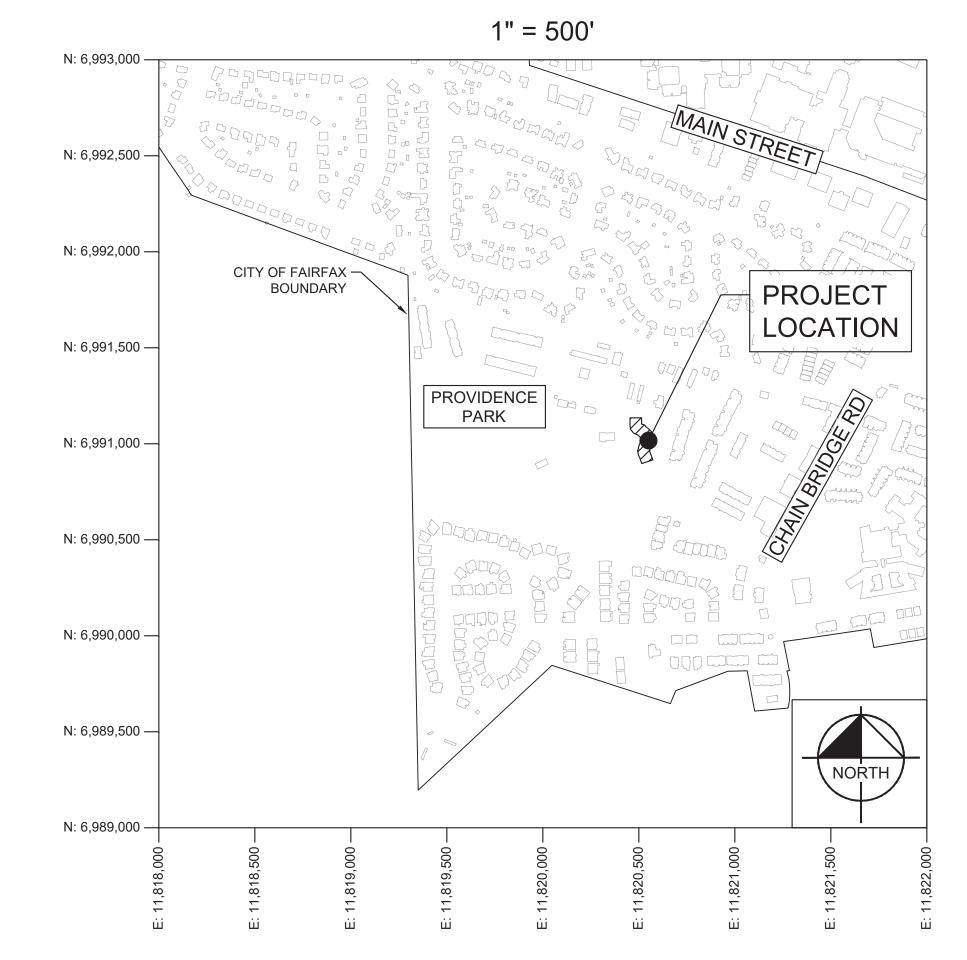
THE PROJECT LIMITS BEGIN AT THE DISCHARGE OF A 15" RCP PIPE AND END AT THE CONFLUENCE OF LOWER BULL RUN. THE PROJECT IS LOCATED IN PROVIDENCE PARK IN THE CITY OF FAIRFAX, VIRGINIA.

THE POLLUTANT OF CONCERN (POC) CREDITING AND DESIGN FOR THE OUTFALL WAS DONE IN ACCORDANCE WITH THE GUIDANCE MEMO "RECOMMENDATIONS FOR CREDITING OUTFALL AND GULLY STABILIZATION PROJECTS IN THE CHESAPEAKE BAY WATERSHED", DATED OCTOBER 15, 2019. REPRESENTATIVE SOIL FIELD SAMPLES WERE OBTAINED FROM THE PROJECT SITE AND PROCEED AT A LABORATORY TO OBTAIN THE SOILS BULK DENSITY, NITROGEN CONCENTRATION, AND PHOSPHORUS CONCENTRATION.

THE SOIL SAMPLE BULK DENSITY WAS 60.56 LB/FT³ AND THE CONCENTRATIONS WERE 0.60 LBS OF PHOSPHORUS PER 1 TON OF SEDIMENT AND 1.34 LBS OF NITROGEN PER 1 TON OF SEDIMENT. THE POLLUTANT OF CONCERN CREDIT REDUCTION FROM THIS PROJECT IS 36,054.40 LBS/YR OF TOTAL SUSPENDED SOLIDS (TSS), 24.16 LBS/YR OF NITROGEN AND 10.89 LBS/YR OF PHOSPHORUS.

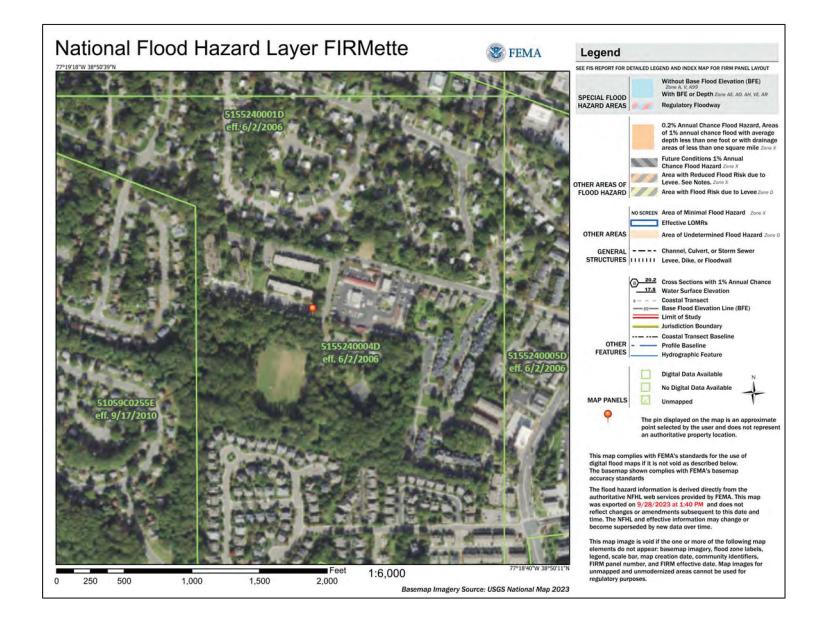
GENERAL NOTES

- THE SUBJECT PROPERTY OF THIS PROJECT IS THE FOLLOWING: TAX MAP NUMBER: 57 3 01 007 PARCEL AREA: 17 ACRES (740,520 SF) DEED BOOK AND NUMBER: UNKNOWN
- 2. TOPOGRAPHIC INFORMATION SHOWN IS BASED ON THE READILY AVAILABLE GEOGRAPHIC INFORMATION SYSTEM (GIS) FOR THE PROJECT AREA. THE SITE IS INTENDED TO BE SURVEYED AS PART OF THE NEXT STAGE OF THE DESIGN PROCESS.
- 3. THE EXISTING UTILITIES, AS SHOWN HEREON, ARE APPROXIMATE ONLY. NO GUARANTEE IS HEREIN MADE OR IMPLIED THAT ALL EXISTING UNDERGROUND UTILITIES ARE SHOWN. IT SHALL BE THE CONTRACTOR'S RESPONSIBILITY TO CONTACT ALL UTILITY COMPANIES TO VERIFY THE TYPE, SIZE, AND LOCATION OF ALL EXISTING UTILITIES PRIOR TO STARTING THE WORK. ANY DISCREPANCIES IN OR FROM THE INFORMATION SHOWN HEREON SHALL BE REPORTED TO KIMLEY-HORN.
- 4. THE AREA SHOWN HERON IS LOCATED ON THE FLOOD INSURANCE RATE MAP (FIRM), COMMUNITY PANEL NO. 5155240004D, WITH AN EFFECTIVE DATE OF JUNE 2, 2006. FIRM PANEL NO. 5155240004D INDICATES THAT THE PROJECT AREA IS NOT LOCATED IN A FEMA SPECIAL FLOOD HAZARD AREA (SFHA).

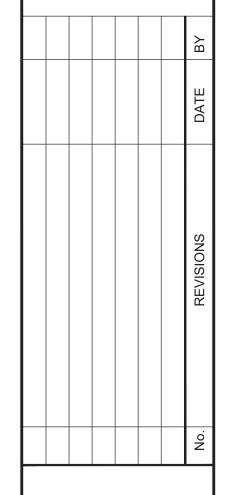


	OWNER	CLIENT	ENGINEER
NAME	CITY OF FAIRFAX	CITY OF FAIRFAX	KIMLEY-HORN
ADDRESS	10455 ARMSTRONG STREET FAIRFAX, VA	10455 ARMSTRONG STREET FAIRFAX, VA	11400 COMMERCE PARK DRIVE, SUITE 400 RESTON, VA
CONTACT	SATOSHI ETO	SATOSHI ETO	JON D'ALESSANDRO
PHONE	(703) 385-7810	(703) 385-7810	(703) 752-0589

	Sheet List Table
Sheet Number	Sheet Title
01	COVER SHEET
02	GENERAL NOTES & DETAILS
03	GENERAL NOTES & DETAILS
04	PHOTO LOCATION MAP
05	EXISTING CONDITIONS
06	EXISTING HYDROLOGY
07	POC CREDITING SUMMARY







400 COMMERCE PARK DR., SUITE 400, RESTON, VA 20191 PHONE: 703-674-1300 FAX: 703-674-1350 www.kimley-horn.com

DATE
10/02/2023
SCALE AS SHOWN
DESIGNED BY J.A.C

GULLY STABILIZATION PROJECTION PR

SHEET NUMBER

Kimley» Ho



Pollution Reduction Calculation Methodology narrative

Crediting for the Providence Park Outfall Restoration Project was performed utilizing the methodologies outlined in Protocol 5 of the "Unified Guide for Crediting Stream and Floodplain Restoration Projects in the Chesapeake Bay Watershed" (Recommendations for Crediting Outfall and Gully Stabilization Projects in the Chesapeake Bay Watershed). Calculation methodologies and crediting for the outfall restoration can be found in the Plan Set Assembly located in the Section F Appendix. Table 1 outlines the Pollutant of Concern (POC) Reduction summary for the restoration of the outfall.

Table 1. City of Fairfax – Providence Park Outfall Restoration Project - Pollutant of Concern Reduction Summary

Outfall-ID	Approximate Outfall Length (ft.)	Outfall Drainage Area (Ac.)	Estimated Phosphorous Reduction Provided (lbs./yr.)	Estimated Nitrogen Reduction Provided (lbs./yr.)	Estimated TSS Reduction Provided (lbs./yr.)
Providence Park Outfall	200	2.08	10.89	24.16	36,054.00

DEQ Virginia Runoff Reduction Method New Development Compliance Spreadsheet - Version 3.0

C 2011 BMP Standards and Specification

© 2013 Draft BMP Standards and Specification

Project Name: Providence Park OTFL #1
Date: 9/20/2023

BMP Design Specifications List: 2013 Draft Stds & Specs

CLEAR ALL (Ctrl+Shift+R) data input cells
constant values
calculation cells
final results

Site Information

Post-Development Project (Treatment Volume and Loads)

Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) undisturbed,					0.00
protected forest/open space or reforested land	0.00	0.00	0.00	0.00	0.00
Managed Turf (acres) disturbed, graded for					0.48
yards or other turf to be mowed/managed	0.00	0.25	0.00	0.23	0.48
Impervious Cover (acres)	0.00	0.06	0.00	1.52	1.57
					2.05

Constants

Annual Rainfall (inches)	43
Target Rainfall Event (inches)	1.00
Total Phosphorus (TP) EMC (mg/L)	0.26
Total Nitrogen (TN) EMC (mg/L)	1.86
Target TP Load (lb/acre/yr)	0.41
Pj (unitless correction factor)	0.90

Runoff Coefficients (Rv)

	A Soils	B Soils	C Soils	D Soils
Forest/Open Space	0.02	0.03	0.04	0.05
Managed Turf	0.15	0.20	0.22	0.25
Impervious Cover	0.95	0.95	0.95	0.95

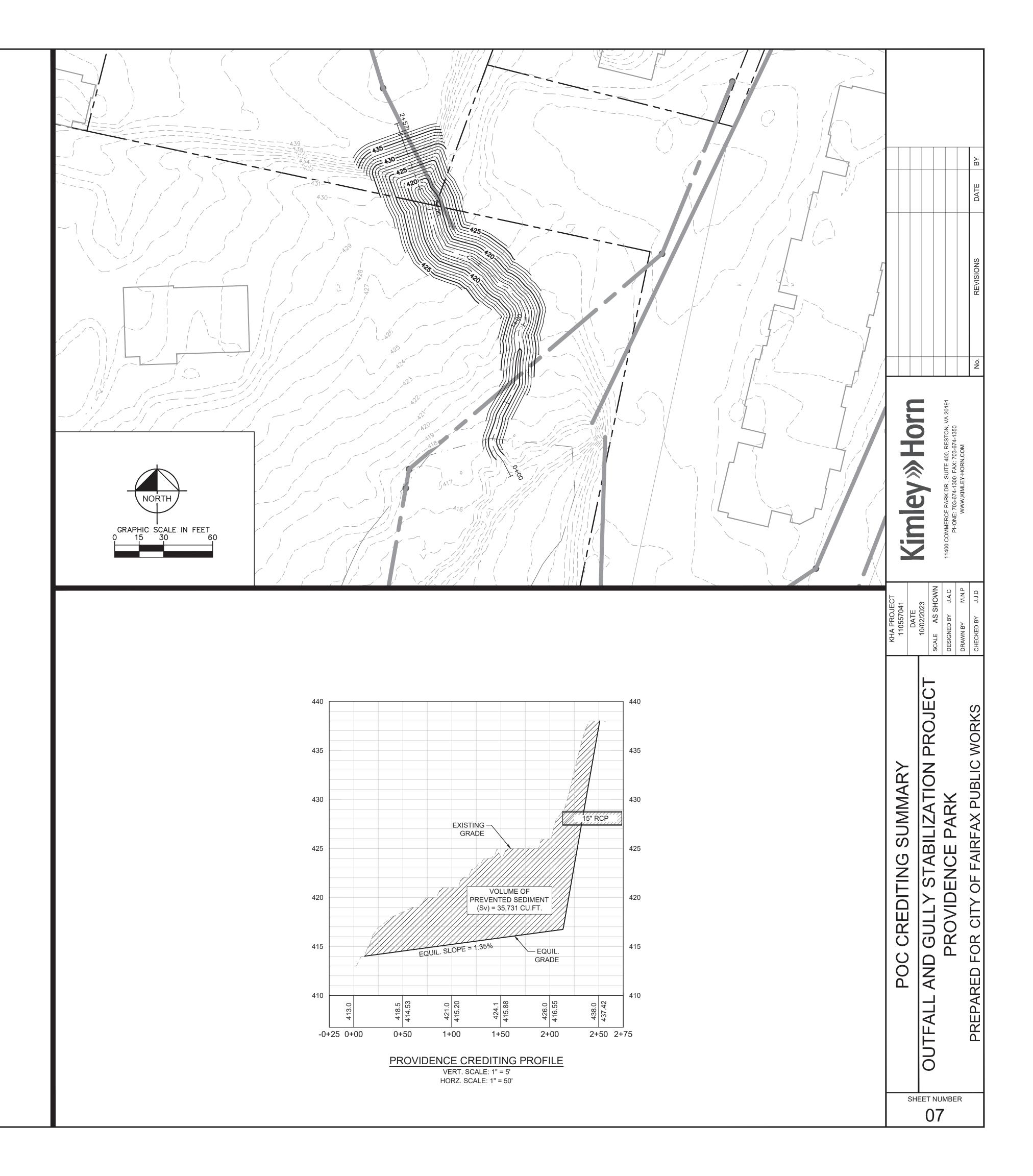
Post-Development Requirement for Site Area

TP Load Reduction Required (lb/yr) 2.81

LAN	J COVER SC
Land Cover Summary	
Forest/Open Space Cover (acres)	0.00
Weighted Rv (forest)	0.00
% Forest	0%
Managed Turf Cover (acres)	0.48
Weighted Rv (turf)	0.22
% Managed Turf	23%
Impervious Cover (acres)	1.57
Rv (impervious)	0.95
% Impervious	77%
Site Area (acres)	2.05
Site Rv	0.78

Treatment Volume and Nutrien	t Loads
Treatment Volume (acre-ft)	0.1335
Treatment Volume (cubic feet)	5,817
TP Load (lb/yr)	3.65
TN Load (lb/yr) (Informational Purposes Only)	26.15

Drainage Area (A _d)=	2.08	ас
Drainage Area (A _d)=	0.0084	km²
Mean Flow Depth = Sten 1 - Define the F	0.683 xisting Channel Conditions	ft
Length of Proposed Reach =	211.990	ft
Channel Slope =	0.066	ft/ft
Bank Height =	14.53	ft
Bottom Width =	2.20	ft
Top Width =	16.93	ft
Bulk Density (Estimate) =	70.00	lb./ft ³
	uilibrium Channel Conditions	,, ; :
Is there a pipe outfall or other defining infrastructure site?		Yes
•	tream Limit	
L _{ma}	$_{\rm ax} = 153 {\rm A_d}^{0.6}$	
Maximum Upstream Channel Length (L _{max}) =	Not Applicable	ft
Equilibi	rium Bed Slope	
Choose Bed Condition =	Bed Condition 1	
Bed Condition 1 =	Cohesive Bed	
Bed Condition 2 =	Sand and Fine Grave (0.1-5mm	particle size)
Bed Condition 3 =	Beds Coarser than Sand (>5mm	particle size)
	on 1: Cohesive Bed	
$S_{eq} =$: 0.0028A ^{-0.33}	
Equilibrium Slope (S _{eq})=	0.0135	ft/ft
Bed Condition 2	2: Sand and Fine Gravel	
$S_{ea} = 0.$	06 / (y * 62.43)	
Equilibrium Slope (S _{eq})=	Not Applicable	ft/ft
·	Bed Coarser than Sand) 4) 1
Equilibrium Slope (S_{eq}) =	Not Applicable	 ft/ft
	um Bank Slopes	
Bank Slopes =		-
Future Bo	ttom Width (est)	
Bottom Width = Step 3: Calculate the	2.2 e Total Prevented Sediment	ft
	e Total Prevented Sediment	
Step 3: Calculate the	e Total Prevented Sediment	
Step 3: Calculate the Volume of Prevented Sediment = Existing Cl	e Total Prevented Sediment hannel Condition - Equilibrium Channel	Condition Cu. Yd.
Step 3: Calculate the Volume of Prevented Sediment = Existing Classian Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) =	total Prevented Sediment hannel Condition - Equilibrium Channel 1,323.00 35,721.00	Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Clause Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Values of Reduction	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Learning Efficiency and Timescale	Cu. Yd. Cu. ft.
Step 3: Calculate the Volume of Prevented Sediment = Existing Clause Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Values of Reduction	total Prevented Sediment hannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lo	Condition Cu. Yd. Cu. ft. oad
Step 3: Calculate the Volume of Prevented Sediment = Existing Classification S_v = Volume of Prevented Sediment S_v = $S_$	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lens in Efficiency and Timescale 0.5 (S v / 30)	Condition Cu. Yd. Cu. ft. oad
$Step \ 3: \ Calculate \ the$ $Volume \ of \ Prevented \ Sediment \ (S_v)=$ $Volume \ of \ Prevented \ Sediment \ (S_v)=$ $Step \ 4: \ Convert \ the \ Total \ Sediment \ V$ $Adjust \ for \ Reduction$ $S_p =$ $Annual \ Volume \ of \ Prevented \ Sediment \ (S_p)=$ $Adjust \ for \ Adjust \ for \ Sediment \ (S_p)=$	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lance in Efficiency and Timescale 0.5 (S _v / 30) 595.35 Soils Bulk Density	Cu. Yd. Cu. ft. oad Cu. ft. / year
Volume of Prevented Sediment = Existing Column of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Sediment (S_p) =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lance in Efficiency and Timescale 0.5 (S , / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year
$Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Cloud \ Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Step \ 4: \ Convert \ the \ Total \ Sediment \ Volume \ of \ Prevented \ Sediment \ (S_p) =$ $Adjust \ for \ S_p =$ $Annual \ Volume \ of \ Prevented \ Sediment \ Load = Annual \ Prevented \ Sediment \ Load \ (Estimate) =$	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lance in Efficiency and Timescale 0.5 (S _v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year
$Step \ 3: \ Calculate \ the$ $Volume \ of \ Prevented \ Sediment = Existing \ Calculate $	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Leading in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 36,054.40	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Leadine Efficiency and Timescale 0.5 (S , / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year
$Step 3: Calculate the \\ Volume of Prevented Sediment = Existing Cloud Sediment (S_v) = \\ Volume of Prevented Sediment (S_v) = \\ Step 4: Convert the Total Sediment Volume of Prevented Sediment (S_p) = \\ Adjust for Reduction S_p = \\ Annual Volume of Prevented Sediment (S_p) = \\ Adjust for Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = \\ Annual Prevented Sediment Load (Field Verified) = \\ Step 5: Determine the \\ Estimated Sediment Load (Estimate) = \\ Step 5: Determine the \\ Step 5: Determine the \\ Step 5: Determine Sediment Load (Estimate) = \\ Step 5: Determine the \\ Step 5: Determine Sediment Load (Estimate) = \\ Step 5: Determine Sediment Load (Estimate) $	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Learning Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
Volume of Prevented Sediment = Existing Column of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment Volume of Prevented Sediment (S_p) = Annual Volume of Prevented Sediment (S_p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (1.05 lb. of Phosphorus (P) =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Leading in Efficiency and Timescale 0.5 (S _V / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for . Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lead in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Adjust for Adjust for Adjust for Sediment Load = Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (Continue) = 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Leadine Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for . Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (S_v) = 2.28 lb. of Phosphorus (S_v) = Estimated Phosphorus (S_v) Removal Rate = Estimated Nitrogen (S_v) Removal Rate =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lead in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year
$Step \ 3: Calculate \ the$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Volume \ of \ Prevented \ Sediment \ (S_v) =$ $Step \ 4: \ Convert \ the \ Total \ Sediment \ V$ $Adjust \ for \ Reduction$ $S_p =$ $Annual \ Volume \ of \ Prevented \ Sediment \ (S_p) =$ $Adjust \ for .$ $Annual \ Prevented \ Sediment \ Load \ (Estimate) =$ $Annual \ Prevented \ Sediment \ Load \ (Field \ Verified) =$ $Step \ 5: \ Determine \ the$ $Estimated \ O$ $1.05 \ lb. \ of \ Phosphorus \ (P) =$ $2.28 \ lb. \ of \ Nitrogen \ (N) =$ $Estimated \ Phosphorus \ (P) \ Removal \ Rate =$ $Estimated \ Nitrogen \ (N) \ Removal \ Rate =$ $Site \ Specification$	Annual Prevented Sediment 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Letter in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable Not Applicable Not Applicable	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S_v) = Volume of Prevented Sediment (S_v) = Step 4: Convert the Total Sediment V Adjust for Reduction S_p = Annual Volume of Prevented Sediment (S_p) = Adjust for . Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated (S_v) = 2.28 lb. of Phosphorus (S_v) = Estimated Phosphorus (S_v) Removal Rate = Estimated Nitrogen (S_v) Removal Rate =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lease in Efficiency and Timescale 0.5 (S , / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable C Adjusted Results	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment Volume for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Adjust for Reduction S _p = Adjust for Reductio	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Letter in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Ital Volume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable Not Applicable Not Applicable C Adjusted Results 60.56	Cu. Yd. Cu. ft. oad Cu. ft. / year Density Ib./year Ib./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Classific Substitute of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Classification of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification of Sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Letter in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable Not Applicable Conversion Factors 1 ton of sediment Applicable Not Applicable Conversion Factors 1 ton of sediment Ont Applicable Ont Applicable Conversion Factors 1 ton of sediment Ont Applicable Ont Applicable Ont Applicable Ont Adjusted Results 60.56 Ontice	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Classification 1.05 lb. of Phosphorus (P) = 2.28 lb. of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification Site Specification Site Specification Site Adjusted Total Suspended Solids (TSS) Removal Rate =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Letter in Efficiency and Timescale 0.5 (S _v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment Not Applicable Not Applicable C Adjusted Results 60.56 0.60 1.34 36,054.40	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Classification Estimated Classification Site Specification Bulk Density = 1 ton of sediment = 1 ton of sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Yolume to Annual Prevented Sediment Lean in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Yolume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable C Adjusted Results 60.56 0.60 1.34 36,054.40 10.89	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ib. of (P) Ib. of (N) Ibs./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Classification of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification of Sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Volume to Annual Prevented Sediment Land in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable C Adjusted Results 60.56 0.60 1.34 36,054.40 10.89 24.16	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Columns of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annu Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Of Sediment Load (Field Verified) = Step 5: Determine the Estimated Of Sediment Load (Results of Sediment Load (Results of Nitrogen (N)) = Estimated Phosphorus (P) = Site Mitrogen (N) Removal Rate = Site Specific Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate = Pollutant of Concern	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Volume to Annual Prevented Sediment Lease in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Val Volume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable C Adjusted Results 60.56 0.60 1.34 36,054.40 10.89 24.16 (POC) Crediting Summary	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year
Volume of Prevented Sediment = Existing Classification Volume of Prevented Sediment (S _v) = Volume of Prevented Sediment (S _v) = Step 4: Convert the Total Sediment V Adjust for Reduction S _p = Annual Volume of Prevented Sediment (S _p) = Annual Prevented Sediment Load = Annual Annual Prevented Sediment Load (Estimate) = Annual Prevented Sediment Load (Field Verified) = Step 5: Determine the Estimated Classification of Nitrogen (N) = Estimated Phosphorus (P) Removal Rate = Estimated Nitrogen (N) Removal Rate = Site Specification of Sediment = Site Adjusted Total Suspended Solids (TSS) Removal Rate = Site Adjusted Phosphorus (P) Removal Rate = Site Adjusted Nitrogen (N) Removal Rate =	thannel Condition - Equilibrium Channel 1,323.00 35,721.00 Volume to Annual Prevented Sediment Land in Efficiency and Timescale 0.5 (S v / 30) 595.35 Soils Bulk Density Volume of Prevented Sediment * Bulk Not Applicable 36,054.40 Annual Prevented Nutrients Conversion Factors 1 ton of sediment 1 ton of sediment Not Applicable Not Applicable C Adjusted Results 60.56 0.60 1.34 36,054.40 10.89 24.16	Condition Cu. Yd. Cu. ft. oad Cu. ft. / year Ib./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year Ibs./year





Appendix S. Mathy Park Retrofit Calculations



Memo

To: City of Fairfax

Attn: Mr. Satoshi Eto

From: Brice Kutch, PE Sean Mowery, PE

Date: March 31, 2023

Re: Mathy Park BMP Project – TMDL Pollutant Removal Calculations (GKY TO#21)

Project Information

GKY was tasked with performing an analysis regarding TMDL credits for the Mathy Park BMP (sheet flow to open space) project located at 10251 Main Street in Fairfax, Virginia. The goal of this analysis was to identify the total nitrogen (TN), total phosphorus (TP), and total suspended solids (TSS) reductions for three (3) sheet flow to open space drainage divides (Figure 1) as follows:

Area 1: Sheet flow area treated to the existing curb line along the museum building and parking parcels (red area).

Area 2: Sheet flow area treated from Ratcliffe Park (blue area).

Area 3: Sheet flow area treated through residential lots along Sager Avenue (yellow area).

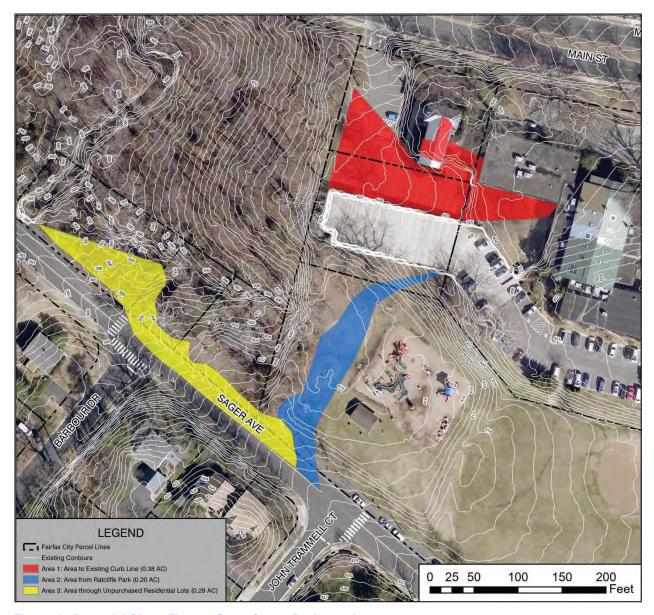


Figure 1. Potential Sheet Flow to Open Space Drainage Areas

GKY utilized the Chesapeake Bay TMDL Special Condition Guidance Memo No. GM20-2003 dated February 6, 2021 (DEQ Guidance) for the following analysis.

Area 1. Sheet Flow to Open Space: Existing Curb Line Analysis

GKY evaluated the TMDL pollutant reduction credit for diverting flow from the museum building and parking parcels (57-4-02-138B and 57-4-02-138C, respectively) as sheet flow to the Mathy Park open space parcel (57-4-02-142). GKY first determined the total loads for all pollutants of concern (TN, TP, and TSS) within the drainage divide for this area and found that approximately 0.25 impervious acres and 0.13 pervious acres make up the 0.38-acre drainage divide for the sheet flow area to existing curb line. It was assumed that all areas of the drainage divide were within MS4 service areas. This drainage divide is shown in red on Figure 1.

Using the DEQ Guidance, GKY determined the total load of TN, TP, and TSS for the sheet flow area to existing curb line drainage divide. These results are presented in Table 1.



Table 1. Total Pollutant Loads (TN, TP, and TSS) for the Sheet Flow Area to Existing Curb Line

Land Use Drainage		Loading Rate -	Total Load -	Loading Rate -	Total Load -	Loading Rate -	Total Load -
Land Ose	Area, ac	TN, lbs/ac/yr	TN, lbs/yr	TP, lbs/ac/yr	TP, lbs/yr	TSS, lbs/ac/yr	TSS, lbs/yr
Impervious	0.25	16.86	4.22	1.62	0.41	1,171.32	292.83
Pervious	0.13	10.07	1.31	0.41	0.05	175.80	22.85
		Total Load -	F F2	Total Load -	0.46	Total Load -	215 60
		TN, lbs/yr	5.52	TP, lbs/yr	0.46	TSS, lbs/yr	315.68

The baseline efficiency of all areas shown in Figure 1 is 0% for TN, TP, and TSS since the areas are currently not being treated by an existing BMP.

GKY then determined the efficiency of the proposed sheet flow to open space for all areas shown in Figure 1 using Table V.A.1 (Virginia Stormwater BMP Clearinghouse BMPs, Established Efficiencies Comparative Runoff Reduction and Nutrient Removal for Practices) in the DEQ Guidance. Using "Sheet Flow to Veg. Filter or Conserve Open Space" as the BMP and designed as flow to open space with C and D soils, the established efficiencies for TN and TP are shown in Table 2.

Table 2. Sheet Flow to Open Space Pollutant Efficiencies for the Area Treated to the Existing Curb Line

ВМР	TN	TP	TSS
Sheet Flow to Open Space (C/D Soils)	50%	50%	75%

TSS percent effectiveness was determined using the retrofit curves/equations found in Appendix V.B (Chesapeake Bay Program, Retrofit Curves/Equations) of the DEQ Guidance. The nutrient curves are divided into two categories: runoff reduction practices (RR) and stormwater treatment practices (ST). Sheet flow to open space was found to be an RR practice per Table V.B.1 (Chesapeake Bay Program, Established Efficiencies) in the DEQ Guidance; therefore, the RR curve shown in Figure 2 was used to determine the TSS efficiency for all sheet flow to open space areas as shown in Figure 1.

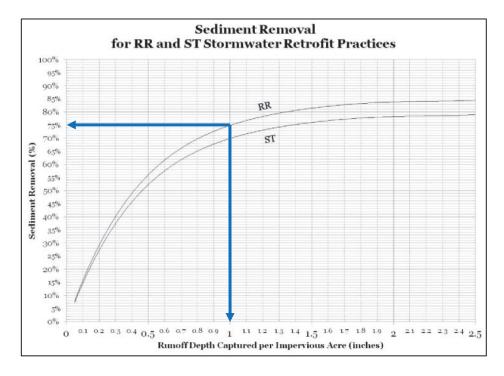


Figure 2. Sediment Removal Percent Effectiveness Based on Runoff Depth Captured Per Impervious Acre



For purposes of determining the sediment (TSS) removal efficiency, a runoff depth captured per impervious acre of 1" was used. Utilizing the RR curve shown in Figure 2, the sediment (TSS) removal efficiency for all sheet flow to open space areas entering Mathy Park (shown in Figure 1) was determined to be 75% as shown in Table 2.

See Table 3 for the resulting credits from converting the untreated area to the existing curb line to sheet flow to open space utilizing the efficiences shown in Table 2. The total credits gained for this conversion is 2.76 lbs/year of TN, 0.23 lbs/year of TP, and 236.76 lbs/year of TSS as shown in Table 3.

Table 3. Credits Gained: Converting Untreated Area to Sheet Flow to Open Space for the Area Treated to the Existing Curb Line

	Pollutants of Concern Credits Gained, lbs/year				
	TN TP TSS				
Total Credits Gained for Sheet Flow to Open Space	2.76	0.23	236.76		

Area 2. Sheet Flow to Open Space: Ratcliffe Park Analysis

GKY evaluated the TMDL pollutant reduction credit for converting flow from the Ratcliffe Park parcel (57-4-02-138A) to sheet flow to the Mathy Park open space parcel (57-4-02-142). GKY first determined the total loads for all pollutants of concern (TN, TP, and TSS) within the drainage divide for this area and found that approximately 0.02 impervious acres and 0.18 pervious acres make up the 0.20-acre drainage divide for the sheet flow area from Ratcliffe Park. It was assumed that all areas of the drainage divide were within MS4 service areas. This drainage divide is shown in blue on Figure 1.

Using the DEQ Guidance, GKY determined the total load of TN, TP, and TSS for the sheet flow area from the Ratcliffe Park drainage divide. These results are presented in Table 4.

Table 4. Total Pollutant Loads (TN, TP, and TSS) for the Sheet Flow Area from Ratcliffe Park

Landilla	Drainage	Loading Rate -	Total Load -	Loading Rate -	Total Load -	Loading Rate -	Total Load -
Land Use	Area, ac	TN, lbs/ac/yr	TN, lbs/yr	TP, lbs/ac/yr	TP, lbs/yr	TSS, lbs/ac/yr	TSS, lbs/yr
Impervious	0.02	16.86	0.34	1.62	0.03	1,171.32	23.43
Pervious	0.18	10.07	1.81	0.41	0.07	175.80	31.64
		Total Load -	2.15	Total Load -	0.11	Total Load -	55.07
		TN, lbs/yr	2.15	TP, lbs/yr	0.11	TSS, lbs/yr	55.07

See Table 5 for the resulting credits from converting the untreated area from Ratcliffe Park to sheet flow to open space utilizing the efficiences shown in Table 2. The total credits gained for this conversion is 1.07 lbs/year of TN, 0.05 lbs/year of TP, and 41.30 lbs/year of TSS as shown in Table 5.

Table 5. Credits Gained: Converting Untreated Area to Sheet Flow to Open Space for the Area Treated from Ratcliffe Park

	Pollutants of Concern Credits Gained, lbs/year					
	TN	TP	TSS			
Total Credits Gained for	1.07	0.05	41.30			
Sheet Flow to Open Space	1.07	0.05	41.30			



Area 3. Sheet Flow to Open Space: Sager Avenue Analysis

GKY evaluated the TMDL pollutant reduction credit for converting flow from the Sager Avenue parcels (57-4-02-139, 57-4-02-140, and 57-4-02-141) to sheet flow to the Mathy Park open space parcel (57-4-02-142). GKY first determined the total loads for all pollutants of concern (TN, TP, and TSS) within the drainage divide for this area and found that approximately 0.10 impervious acres and 0.19 pervious acres make up the 0.29-acre drainage divide for the sheet flow area from the Sager Avenue parcels. It was assumed that all areas of the drainage divide were within MS4 service areas. This drainage divide is shown in yellow on Figure 1.

Using the DEQ Guidance, GKY determined the total load of TN, TP, and TSS for the sheet flow area from the Sager Avenue drainage divide. These results are presented in Table 6.

Table 6. Total Pollutant Loads (TN, TP, and TSS) for the Sheet Flow Area from the Sager Avenue Parcels

Landillea	Drainage	Loading Rate -	Total Load -	Loading Rate -	Total Load -	Loading Rate -	Total Load -
Land Use	Area, ac	TN, lbs/ac/yr	TN, lbs/yr	TP, lbs/ac/yr	TP, lbs/yr	TSS, lbs/ac/yr	TSS, lbs/yr
Impervious	0.10	16.86	1.69	1.62	0.16	1,171.32	117.13
Pervious	0.19	10.07	1.91	0.41	0.08	175.80	33.40
		Total Load -	3.60	Total Load -	0.24	Total Load -	150.52
		TN, lbs/yr	3.60	TP, lbs/yr	0.24	TSS, lbs/yr	150.53

See Table 6 for the resulting credits from converting the untreated area from the Sager Avenue parcels to sheet flow to open space utilizing the efficiences shown in Table 2. The total credits gained for this conversion is 1.80 lbs/year of TN, 0.12 lbs/year of TP, and 112.90 lbs/year of TSS as shown in Table 7.

Table 7. Credits Gained: Converting Untreated Area to Sheet Flow to Open Space for the Area Treated from the Sager Avenue Parcels

	Pollutants of Concern Credits Gained, lbs/year				
	TN TP TSS				
Total Credits Gained for Sheet Flow to Open Space	1.80	0.12	112.90		

Conclusion

Table 8 identifies the total nitrogen (TN), total phosphorus (TP), and total suspended solids (TSS) reductions for the three (3) sheet flow to open space drainage divides (Figure 1).

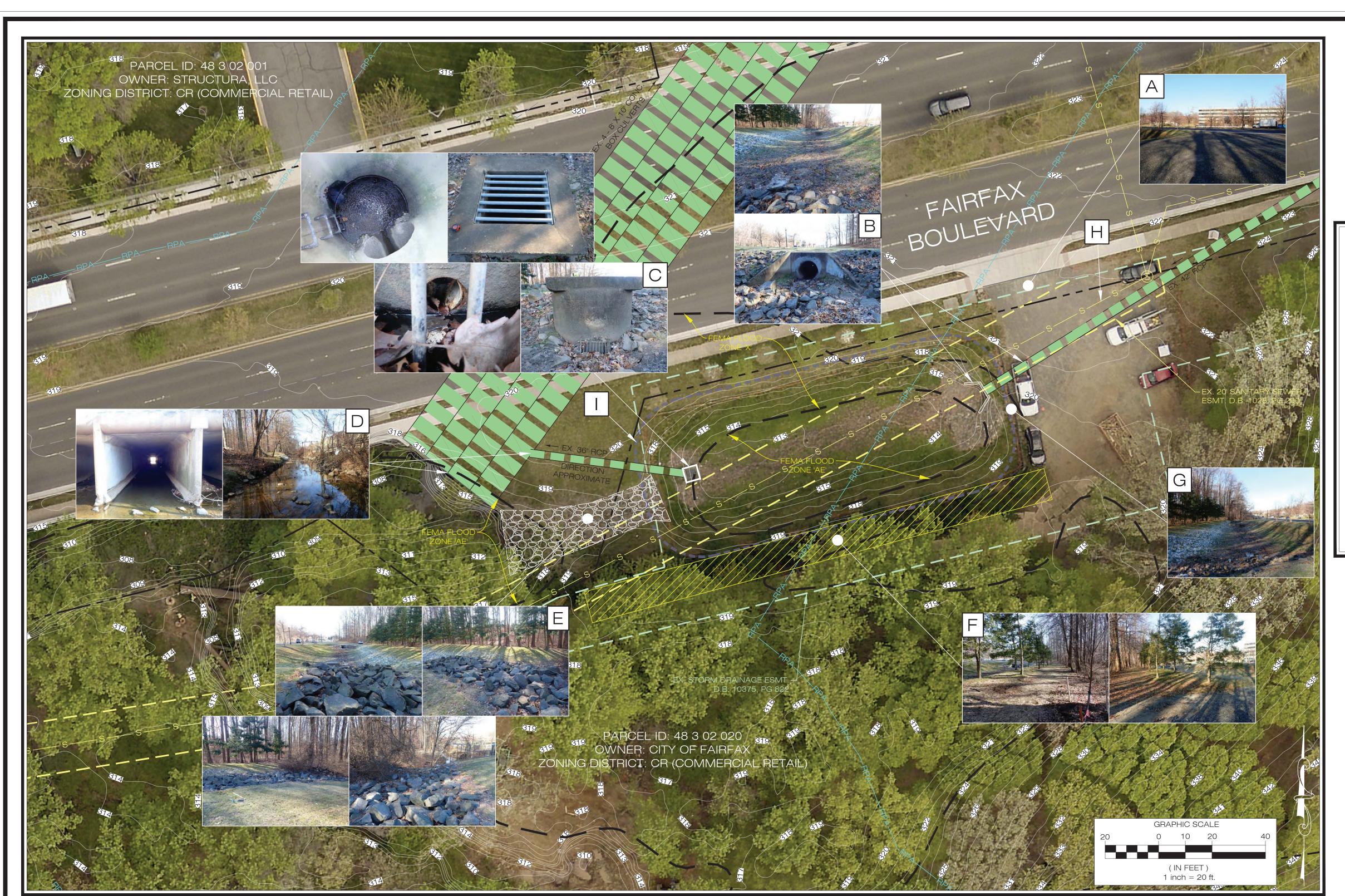
Table 8. Credits Gained: Converting Untreated Area to Sheet Flow to Open Space for All Areas

Mathy Park Drainage Divides	Impervious Area (Acres)	Pervious Area (Acres)	TN Credits Gained (lbs/year)	TP Credits Gained (lbs/year)	TSS Credits Gained (lbs/year)
Area 1	0.25	0.13	2.76	0.23	236.76
Area 2	0.02	0.18	1.07	0.05	41.3
Area 3	0.10	0.19	1.80	0.12	112.9
		Total:	5.63	0.40	390.96





Appendix T. Lions Run BMP Retrofit Concept Calculations



NOTE: ALL AERIAL IMAGERY, TOPOGRAPHIC, AND PIPE NETWORK DATA WAS RETRIEVED FROM THE FAIRFAX COUNTY AND CITY OF FAIRFAX GIS DATABASES. THE EASEMENT AND BOX CULVERT PIPE LINES WERE DIGITIZED FROM ATLA / ACSM LAND TITLE SURVEY OF THE PROPERTY OF MARGURITE O. PITTS, DATED DECEMBER 1987. SUPPLEMENTAL PHOTOGRAPHS WERE TAKEN BY GKY ENGINEERS DURING A SITE VISIT ON FEBRUARY 20TH, 2024.

PROJECT NARRATIVE

THE EXISTING FAIRFAX HIGH SCHOOL DRY POND FACILITY IS LOCATED AT 9985 FAIRFAX BOULEVARD, PARCEL ID 48 3 02 020, AND IS OWNED AND MAINTAINED BY THE CITY OF FAIRFAX. NO FACILITY DESIGN PLANS COULD BE LOCATED FOR THE POND. AN ATLA / ACSM LAND TITLE SURVEY OF THE PROPERTY OF MARGURITE O. PITTS, DATED DECEMBER 1987 SHOWS SOME PROPERTY, EASEMENT, AND UTILITY INFORMATION IN THE AREA OF THE EXISTING POND FACILITY. GKY PREVIOUSLY EVALUATED THIS POND AS A RETROFIT OPPORTUNITY TO PROVIDE EDUCATIONAL OUTREACH FOR THE COMMUNITY AND THE ADJACENT HIGH SCHOOL, AS WELL AS CLAIM SOME TMDL POLLUTANT REDUCTION CREDITS FOR THE CITY. THE EXISTING DELINEATED DRAINAGE AREA TO THE FACILITY IS 8.19 ACRES. THE OUTFALL OF THE FACILITY EXITS INTO EXISTING QUADRUPLE 8'X10' BOX CULVERTS CONVEYING ACCOTINK CREEK FROM SOUTHWEST TO NORTHEAST UNDERNEATH FAIRFAX BOULEVARD, AND ULTIMATELY EMPTIES INTO THE POTOMAC RIVER AT GUNSTON COVE.

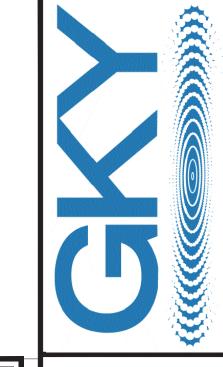
THE OBJECTIVE FOR THIS PROJECT IS TO RETROFIT THE EXISTING DRY POND FACILITY TO A LEVEL 1 EXTENDED DETENTION POND. PROPOSED IMPROVEMENTS FOR THIS FACILITY INCLUDE A SEDIMENT FOREBAY AT THE INFLOW, TWO MICROPOOLS ON THE POND FLOOR, AQUATIC BENCHES AROUND THE FOREBAY AND MICROPOOLS, INCREASED STORAGE VOLUME TO MEET TREATMENT VOLUME DESIGN REQUIREMENTS, MEANDERING FLOW PATH, AND MODIFICATIONS TO THE EXISTING RISER STRUCTURE TO MEET ALLOWABLE FLOWS. APPROXIMATELY 0.54 ACRES ARE PROPOSED TO BE DISTURBED WITH THIS PROJECT.

THE REQUIRED TREATMENT VOLUME BASED ON VRRM CALCULATIONS (SEE SHEET 3) IS 15,758 CF. A MINIMUM OF 15% OF THE REQUIRED TREATMENT VOLUME SHALL BE CONTAINED BELOW THE PERMANENT POOLS OF THE FOREBAY AND MICROPOOLS. THE TOTAL PROPOSED STORAGE BELOW PERMANENT POOL WITH THIS PLAN IS 4,573 CF (29%) AS SHOWN IN THE WET STAGE-STORAGE TABLES ON SHEET 4. THE TOTAL TREATMENT VOLUME BELOW 314.91' (THE 2-YR ORIFICE INVERT ELEVATION OF THE MODIFIED CONTROL STRUCTURE) IS 15,766 CF, WHICH IS GREATER THAN THE REQUIRED TREATMENT VOLUME OF 15,758 CF.

GKY PERFORMED AN ANALYSIS REGARDING TMDL CREDITS TO CALCULATE POLLUTANT CREDITS GAINED FOR RETROFITTING THE EXISTING DRY POND FACILITY TO A LEVEL 1 EXTENDED DETENTION POND FACILITY. SEE SHEET 3 FOR THE TMDL CREDIT ANALYSIS SUMMARY.

THE FACILITY'S PROPOSED DRY DETENTION VOLUME CAPACITY IS PROPOSED TO INCREASE. EXISTING AND PROPOSED STAGE-STORAGE TABLES ARE SHOWN ON SHEET 4. EXISTING POND STAGE-STORAGE WAS DEVELOPED USING 2018 FAIRFAX COUNTY 1-FT CONTOUR GIS DATA. AN ANALYSIS OF PEAK OUTFLOWS AND ROUTED PEAK WATER SURFACE ELEVATIONS WAS PERFORMED FOR THE EXISTING POND AND THE PROPOSED LEVEL 1 EXTENDED DETENTION POND FACILITY WITH RESULTS SHOWN ON SHEET 4.

FAIRFAX HIGH SCHOOL POND RETROFIT CONCEPT PLAN



LEGEND

EXISTING MAINTENANCE ACCESS ROAD ENTRANCE VIA FAIRFAX BOULEVARD

EXISTING 42" RCP INFLOW, WITH 60" H X 72" W HEADWALL, AND WINGWALLS. SEE EXISTING INFLOW HEADWALL AND WINGWALL DETAIL ON SHEET 5.

EXISTING 6' DIA. CONCRETE CONTROL STRUCTURE WITH 64" X 64" X 8" TOF SLAB, 3' X 3' GRATE DROP INLET, 3" LOW-FLOW ORIFICE, AND 36" PRINCIPAL SPILLWAY PIPE. SEE EXISTING CONTROL STRUCTURE DETAIL ON SHEET 5.

FACILITY OUTFALLS INTO EXISTING QUADRUPLE 8' X 10' BOX CULVERTS CONVEYING ACCOTINK CREEK.

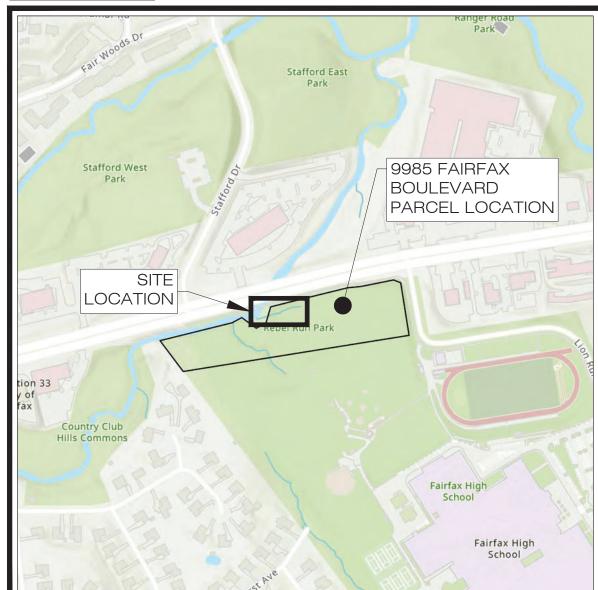
EXISTING EMERGENCY SPILLWAY CHANNEL; APPROXIMATE 10' BOTTOM WIDTH, 16' TOP WIDTH, AND 3:1 SIDE SLOPES. SEE EXISTING EMERGENCY SPILLWAY DETAIL ON SHEET 5.

EXISTING AREA OF LANDSCAPING ADJACENT TO POND; 19 TREES AND 2 SHRUBS TO BE REMOVED FOR POND EXPANSION.

EXISTING DRY POND FACILITY, OVERALL, LOOKING SOUTHWEST.

EXISTING 14" SANITARY SEWER LINE FROM CITY GIS DATA. THE EXISTING SANITARY SEWER LINE RUNS UNDERNEATH THE EXISTING POND AT AN APPROXIMATE ELEVATION BETWEN 302' AND 305' AS SHOWN ON ATLA / ACSM LAND TITLE SURVEY OF THE PROPERTY OF MARGURITE O. PITTS, DATED DECEMBER 1987.

EXISTING POND FOOTPRINT.



SOURCE: NATIONAL GEOGRAPHIC ESRI

SHEET INDEX

- 1 EXISTING CONDITIONS
- 2 PROPOSED CONDITIONS
- 3 SWM ANALYSIS (1 OF 2)
- 4 SWM ANALYSIS (2 OF 2)
- 5 SWM STRUCTURE DETAILS

(5 TOTAL SHEETS)

H SCALE: H DATUM: NAD83 V SCALE: N/A V DATUM: NGVD29

DATE | DESCRIPTIO

4/3/2024 | 1ST SUB.

DESIGNED: DRAFTED: CHECKED:

PROJECT#: 2023-002 CONTRACT#: TO#11

SHEET:

ALL INFORMATION HEREIN, INCLUDING THE PLAN AND COST ESTIMATE, IS IN PRELIMINARY FORM AT A CONCEPTUAL LEVEL OF DESIGN, PRODUCED AS AN INTERIM PRODUCT. INFORMATION WILL CHANGE AS SUBSEQUENT LEVELS OF DESIGN ARE COMPLETED.

VICINITY MAP

SCALE 1" = 400'

From: Brian Wilson, EIT Sean Mowery, PE

Date: April 3, 2024

QUANTITY UNIT UNIT COST COST

1 EA \$5,000 / EA \$5,000

40 LF \$130 / LF \$5,200

19 EA \$1,050 / EA \$19,950

2 EA \$500 / EA \$1,000

15 EA \$1,000 / EA \$15,000

80 TN \$150 / TN \$12,000

1 LS \$150,000 / LS \$150,000

1 LS \$10,000 / LS \$10,000

1,350 CY \$77 / CY \$103,950

1 LS \$20,000 / LS \$20,000

1 EA \$15,000 / EA \$15,000

120 TN \$150 / TN \$18,000 350 SY \$12 / SY \$4,200

50 CY \$80 / CY \$4,000

1 LS \$8,000 / LS \$8,000

1 LS \$5,000 / LS \$5,000 1 LS \$100,000 / LS \$100,000

MISCELLANEOUS SUBTOTAL: \$105,000

PROJECT SUB TOTAL: \$531,300

PROJECT TOTAL: \$725,225

Level 1 Design Criteria Per VA Stormwater BMP

Clearinghouse

Required Treatment Volume (T_V) is equal to the calculated

Treatment Volume.

A minimum of 15% of the Treatment Volume (T_V) is required

below permanent pool of forebay and micropool(s).

Length/width ratio or flow path = 2:1 or more. Length of

multiple inflows, the flow path is measured from the dominant

inflows (that comprise 80% or more of the total pond inflow).

Average Treatment Volume (T_V) extended detention time is

required to be 24 hours.

cannot extend more than 5 ft above the pond floor. Turf cover is required on the floor of the pond.

At least one (1) forebay and one (1) micropool are required in

the design of the extended detention pond.

shortest flow path/overall length = 0.4 or more. In the case of

TOTAL: \$557,865

PROPOSED IMPROVEMENTS SUB TOTAL: \$218,150

MOBILIZATION (5% of PROJECT SUB TOTAL): \$26,565

CONTINGENCY (30% of PROJECT SUB TOTAL): \$167,360

1,750 SY \$20 / SY \$35,000

EROSION & SEDIMENT CONTROL SUB TOTAL: \$150,000

DEMOLITION SUB TOTAL: \$58,150

Project: Fairfax High School Pond Retrofit

Estimate Type: Conceptual Plan Estimate

2 Removal of Existing Inflow Endwall and Wing Walls

7 Removal of Emergency Spillway Riprap and Store on Site

4 Relocation of Trees Along South Side of Pond

5 Relocation of Shrubs Along South Side of Pond

6 Removal of Existing Trees (6"-12" diameter)

14 Excavation and Hauling Excess Soil Off-Site

18 Riprap for Inflow and Emergency Spillway

20 Widening the Emergency Spillway Channel

21 Landscaping and Miscellaneous Restoration

9 EROSION & SEDIMENT CONTROL

10 Erosion and Sediment Controls

12 PROPOSED IMPROVEMENTS

17 Inflow Headwall and Wing Walls

15 Fine Grading of Pond

16 Aquatic Bench Plantings

19 Gravel for Access Road

25 Survey, Design, & Permitting

23 MISCELLANEOUS 24 Maintenance of Traffic

3 Removal of Existing Portion of 42" RCP Inflow and Disposal Offsite

13 Riser Modifications (low-flow trash rack, BMP orifice plate, new orifice)

Prepared by: GKY & Associates, Inc.

Date: Arpil 3, 2024

ITEM

1 DEMOLITION

Re: Fairfax High School Pond Retrofit – TMDL Credit Analysis (GKY TO#11)

Project Information

ALL INFORMATION HEREIN, INCLUDING THE PLAN AND COST ESTIMATE, IS IN PRELIMINARY

LEVEL 1 EXTENDED DETENTION POND DESIGN GUIDANCE MATRIX

FORM AT A CONCEPTUAL LEVEL OF DESIGN, PRODUCED AS AN INTERIM PRODUCT.

INFORMATION WILL CHANGE AS SUBSEQUENT LEVELS OF DESIGN ARE COMPLETED

Vertical Treatment Volume (T_V) extended detention fluctuation | The maximum head corresponding to the required water quality

GKY was tasked with performing an analysis regarding TMDL credits for the retrofit project of the existing Fairfax High School dry pond facility located at 9985 Fairfax Boulevard, in Fairfax, Virginia. The goal of this analysis was to identify the total nitrogen (TN), total phosphorus (TP), and total suspended solids (TSS) reductions for the following retrofit:

1. Converting the existing dry pond to a Level 1 extended detention pond.

GKY utilized the Chesapeake Bay TMDL Special Condition Guidance Memo No. GM20-2003 dated February 6, 2021 (DEQ Guidance).

1. Existing Fairfax High School Dry Pond to Level 1 Extended Detention Pond

GKY evaluated the conversion of the existing Fairfax High School dry pond to a Level 1 Extended Detention Pond. GKY first determined the total loads for all pollutants of concern (TN, TP, and TSS) within the existing dry pond's drainage shed. GKY delineated the drainage shed for this facility under TO#11 and found that approximately 4.02 impervious acres and 4.17 pervious acres make up the 8.19-acre drainage shed for the existing dry pond. It was assumed that all areas of the drainage shed for the dry pond were within MS4 service areas.

Using the DEQ Guidance, GKY determined the total load of TN, TP, and TSS for the existing dry pond drainage shed. These results are presented in Table 1.

Table 1. Total Pollutant Loads (TN, TP, and TSS) for the Existing Dry Pond

Land Use	Drainage Area, ac	Loading Rate - TN, lbs/ac/yr	Total Load - TN, lbs/yr	Loading Rate - TP, lbs/ac/yr	Total Load - TP, lbs/yr	Loading Rate - TSS, lbs/ac/yr	Total Load - TSS, lbs/yr
Impervious	4.02	16.86	67.78	1.62	6.51	1,171.32	4,708.71
Pervious	4.17	10.07	41.99	0.41	1.71	175.80	733.09
		Total Load - TN, lbs/yr	109.77	Total Load - TP, lbs/yr	8.22	Total Load - TSS, lbs/vr	5,441.79

GKY then determined the baseline efficiency of the existing dry pond using Table V.C.1 (Chesapeake Bay Program BMPs, Established Efficiencies) in the DEQ Guidance. Using "Dry Detention Ponds and Hydrodynamic Structures" as the BMP, the established efficiencies are presented in Table 2.

Proposed Level 1 Extended Detention Pond Design Per
Criteria Met

This Planset

Required Treatment Volume is 15,758 ft³ per the VRRM

spreadsheet calculations shown on this sheet. The Treatment olume proposed with this design, below elevation 314.91' (crest of

BMP pool at modified riser), is 15,766 ft³. One (1) forebay is proposed with 1,621 ft³ of storage below permanent pool (313'). Two (2) micropools are proposed; one (1) with 2,595 ft³ of storage below permanent pool (313') and one (1)

with 357 ft³ of storage below permanent pool (313'). The

combined storage below permanent pool for the forebay and

micropools is 4,573 ft³, which is 29.0% of the required treament volume of 15,758 ft³.

The flow path length of the proposed extended detention pond is

approximately 227 ft and the width of the proposed extended

of approximately 2.8:1. There is one (1) piped inflow to the facility.

The piped inflow comprises more than 80% of the total pond inflow.

The extended detention drawdown time is proposed to be 24

volume is proposed to be 1.91 ft'.

Turf cover is proposed on the pond floor. One (1) forebay and two (2) micropools are proposed with this

detention pond is approximately 80 ft, which is a length/width ratio

(P)703 642 5080 (F)703 642 5367 WWW.GKY.COM 4229 LAFAYETTE CENTER DRIVE | SHITE 1850 | CHANTILLY VA 20151 WATER RESOURCES & ENVIRONMENTAL SOLUTIONS Fairfax High School Pond Retrofit - TMDL Credit Analysis (GKY TO#11)

Table 2. Existing Dry Pond Pollutant Efficiencies

BMP TN TP TSS Dry Pond 5% 10% 10%

GKY also looked for missing design criteria for the existing dry pond to determine if the BMP efficiency should be modified downward. Specifically, 10% downward reductions in efficiency were applied for two missing water quality features as presented in Table 3. These included a missing sediment forebay and no micro pool near the outlet. No reduction in efficiency was applied for an undersized practice based on the existing water quality storage volume of 0.49 acre-feet (based on Fairfax County 1-ft contours), which is more than 2*WQ_V, where WQ_V = 0.5" x impervious area draining to the pond or 0.17 acre-feet. Based on an impervious area of 4.02 acres, 2*WQ_V = 0.34 acre-feet. Furthermore, no additional reduction in efficiency was applied as the existing 3" low-flow orifice has a calculated drawdown of 12.1 hours.

Table 3. Existing Dry Pond Efficiency Adjustment

Dry Extended Detention Pond Efficiency Adjustments (Place a Y Existing Dry Pond Criteria	Applicable	
	Applicable	
Absence of sediment forebay	Υ	10%
Absence of micropool or other form of riser outlet protection	Y	10%
Short circuting due to initial inlet placement (design flaw only)	N	0%
Drainage Area <5 acres and drainage orifice > 3 inches or	N	0%
Less than 12-hour draw down time	N	0%
Undersized practice based on the existing water quality storage volume	N	0%
Ţ	atal Adjustment	209/

GKY modified the BMP efficiencies downward by 20% to obtain the adjusted existing dry pond pollutant efficiencies, as presented in Table 4.

Table 4. Adjusted Existing Dry Pond Pollutant Efficiencies

BMP TN TP TSS

Dry Pond	4%	8%	8%	
GKY then determ	ined the tot	al loads for	all pollutants of c	oncern (TN, TP, and TSS) within
				ed. GKY delineated the drainage

e shed for this facility under TO#11 and found that approximately 4.02 impervious acres and 5.08 pervious acres make up the 9.20-acre drainage shed for the proposed level 1 extended detention pond. It was assumed that all areas of the drainage shed for the extended detention pond were within MS4 service

Using the DEQ Guidance, GKY determined the total load of TN, TP, and TSS for the proposed level 1 extended detention pond drainage shed. These results are presented in Table 5.

Table 5. Total Pollutant Loads (TN, TP, and TSS) for the Proposed Level 1 Extended Detention Pond

Land Use	Drainage Area, ac	Loading Rate - TN, lbs/ac/yr	Total Load - TN, lbs/yr	Loading Rate - TP, lbs/ac/yr	Total Load - TP, lbs/yr	Loading Rate - TSS, lbs/ac/yr	Total Load - TSS, lbs/yr
Impervious	4.02	16.86	67.78	1.62	6.51	1,171.32	4,708.71
Pervious	5.18	10.07	52.16	0.41	2.12	175.80	910.64
		Total Load - TN, lbs/yr	119.94	Total Load - TP, lbs/yr	8.64	Total Load - TSS, Ibs/yr	5,619.35

Fairfax High School Pond Retrofit - TMDL Credit Analysis (GKY TO#11)

GKY then determined the efficiency of the proposed level 1 extended detention pond using Table V.A.1 (Virginia Stormwater BMP Clearinghouse BMPs, Established Efficiencies Comparative Runoff Reduction and Nutrient Removal for Practices) in the DEQ Guidance. Using "Ext. Det. Ponds" as the BMP and design level 1, the established efficiencies for TN and TP are shown in Table 5.

TSS percent effectiveness was determined using Table V.C.1 (Chesapeake Bay Program BMPs, Established Efficiencies) in the DEQ Guidance. Using "Dry Extended Detention Ponds" as the BMP.

Table 6. Level 1 Extended Detention Pond Pollutant Efficiencies:

the established efficiency for TSS is shown in Table 6.

BMP	TN	TP	TSS
-----	----	----	-----

Pollutant load reductions from converting the existing Fairfax High School dry pond to a level 1 extended detention pond were determined by taking the difference between the exsiting dry pond pollutant load efficiencies and level 1 extended detention pond pollutant load efficiencies. See Table 7 for the resulting credits for the level 1 extended detention pond retrofit.

Table 7. Credits Gained: Converting Existing Dry Pond to Level 1 Extended Detention Pond (Runoff Depth Captured Per Impervious Acre = 1.0")

	Pollutants of Concern Credits Gained, lbs/year				
	TN	TP	TSS		
Proposed Level 1 Extended Detention Pond	11.99	1.30	3,371.61		
Existing Dry Pond	(4.39)	(0.66)	(435.34)		
MS4 Area Credits Gained	7.60	0.64	2,936.27		

Therefore, the total credits gained for converting the existing Fairfax High School dry pond to a level 1 extended detention pond is 7.60 lbs/year of TN, 0.64 lbs/year of TP, and 2,936.27 lbs/year of TSS as

GKY

2.89

0.03

31%

2.29

0.23

25%

4.02

0.95

9.20

0.48

Land Cover Summary

Forest/Open Space Cover (acres)

Weighted Rv (forest)

% Forest

Managed Turf Cover (acres)

Weighted Rv (turf)

% Managed Turf

Impervious Cover (acres)

Rv (impervious)

% Impervious

Site Area (acres)

Site Rv

FAIRFAX HIGH SCHOOL POND RETROFIT VRRM CALCULATIONS FOR TREATMENT VOLUME

GKY

Site Information

Post-Development Project (Treatment Volume and Loads)

0.90

Land Cover Jacres

	A Soils	B Soils	C Soils	D Soils	Totals
Forest/Open Space (acres) undisturbed, protected forest/open space or reforested		2.69	0.15	0.06	2.89
Managed Turf (acres) disturbed, graded for yards or other turf to be		0.23	1.30	0.76	2.29
Impervious Cover (acres)		0.51	1.49	2.02	4.02
* Forest/Open Space areas must be protect	ted in accordance	with the Virginia R	unoff Reduction Meth	od	9.20

Constants	
Annual Rainfall (inches)	43
Target Rainfall Event (inches)	1.00
Total Phosphorus (TP) EMC (mg/L)	0.26
Total Nitrogen (TN) EMC (mg/L)	1.86
Target TP Load (lb/acre/yr)	0.41

	A Soils	B Soils	C Soils	D Soils
Forest/Open Space	0.02	0.03	0.04	0.05
Managed Turf	0.15	0.20	0.22	0.25
Impervious Cover	0.95	0.95	0.95	0.95

Drainage Area A

Pj (unitless correction factor)

Drainage Area A Land Cover (acres)

	A Soils	B Soils	C Soils	D Soils	Totals	Land Cover R
Forest/Open Space (acres)		2.69	0.15	0.06	2.89	0.03
Managed Turf (acres)		0.23	1.30	0.76	2.29	0.23
Impervious Cover (acres)		0.51	1.49	2.02	4.02	0.95
				Total	9.20	

Post Development Treatment Volume in D.A. A (ft³) 15,758

DATE DESCRIPTIO 4/3/2024 | 1ST SUB.

H SCALE: H DATUM: NAD83 V SCALE: N/A V DATUM: NGVD29 DESIGNED: DRAFTED: BW CHECKED: BK PROJECT#: 2023-002

CONTRACT#: TO#11

3 OF 5

SHEET:

AIRE,

 \widehat{S} \circ YSIS



Appendix U. Storm Drain Cleaning Assessment and Procedures

City of Fairfax Department of Public Works Stormwater Management

STORM DRAIN CLEANING ASSESSMENT AND PROCEDURES

Draft - Version 1 - August 4, 2021

Prepared for:



City of Fairfax, Virginia
Public Works - Stormwater
10455 Armstrong Street
Room 200
Fairfax, VA 22030

Updated by:



4229 Lafayette Center Drive, Suite 1850 Chantilly, Virginia 20151 703-870-7000



Acronyms

BMP Best Management Practice

CBP U.S. EPA Chesapeake Bay Program

DEQ Virginia Department of Environmental Quality

EPA U.S. Environmental Protection Agency

GM DEQ Guidance Memo

MS4 Municipal Separate Storm Sewer System

N Total Nitrogen

P Total Phosphorus

POC Pollutants of Concern – Nitrogen, Phosphorus and Sediment

SDC Storm Drain Cleaning

SOP Standard Operating Procedure

TMDL Total Maximum Daily Load

TSS Total Suspended Solids



1.0 Background and Purpose

With the February 6, 2021 publication of Guidance Memo No. 20-2003 (GM #20-2003),¹ the Virginia Department of Environmental Quality (DEQ) adopted the United States Environmental Protection Agency (EPA) Chesapeake Bay Program's (CBP) "Recommendations of the Expert Panel to Define Removal Rates for Street and Storm Drain Cleaning (SDC) Practices, Final Report, May 19, 2016, (CBP Final Report) as the sole acceptable methodology to quantify associated Chesapeake Bay Total Maximum Daily Load (TMDL) Pollutants of Concern (POC) reduction credits in Virginia after June 30, 2022. GM #20-2003 defines the requirements and expectations SDC programs must implement for associated POC reductions to be credited towards meeting VPDES General Permit for the Discharge of Stormwater from Small MS4s Chesapeake Bay TMDL requirements.

The purpose of this document is to determine the applicability for the City to utilize SDC as a means to meet POC reduction requirements, assess potential POC load reductions, and provide a draft SDC Credit Tracking and Documentation Standard Operating Procedure (SOP) (Attachment 1) for consideration.

2.0 SDC POC Reduction Credit Applicability

The use of credits associated with SDC is an annual non-traditional BMP available to the City for meeting its Chesapeake Bay TMDL POC load reductions. The acceptable SDC BMP described in the CBP Final Report can be characterized as a systematic, well-defined, documented, and verifiable program rather than just quantification of the POC removed from stormwater infrastructure associated with response-oriented maintenance programs. To be applied towards meeting Chesapeake Bay TMDL POC reduction requirements, credits from SDC must meet the following requirements and expectations:

1. The SDC program should target catch basins that trap the greatest organic matter loads, streets with the greatest overhead tree capacity, and/or outfalls with high sediment or debris loads.

The City targets stormwater infrastructure that is located within the MS4 service area and which the City conducts storm sewer maintenance as a result of historical knowledge or citizen complaints regarding drainage, flooding, or water quality issues caused by sediment, debris, or leaf litter.

2. POC loads collected as part of the SDC must be tracked and verified using a field protocol to measure the mass or volume of solids collected within the storm drainage system.

The Tracking and Documenting SDC Activities and Quantifying Associated POC Reduction Credits SOP provides the direction for tracking and documenting POC load removal by volume for stormwater infrastructure cleaned for sediment removal and direction for tracking and documenting POC removal by weight for stormwater infrastructure cleaned as part of organic material removal activities.

Volume has been selected as the means of estimating sediment removal loads as a means of program efficiency. Given City maintenance crews' daily workloads, it is not feasible or effective to keep sediment collected as part of the SDC program from sediment collected as part of other non-qualifying stormwater maintenance activities for the purposes of weighing.

3. An SOP must be developed and implemented to keep track of the mass of sediments and/or organic matter that is removed.

The Tracking and Documenting SDC Activities and Quantifying Associated POC Reduction Credits SOP has been developed for implementation in conjunction with the City SOP for Storm Sewer System Cleaning and

¹ Official copies of DEQ GM #20-2003 - Chesapeake Bay TMDL Special Condition Guidance are available from the Virginia Regulatory Town Hall (https://townhall.virginia.gov/L/GDocs.cfm)



Maintenance to assure collection and disposal requirements are met and that tracking, documentation, and verification of records are properly recorded.

4. Credits can only be generated from the cleaning of certain types of stormwater infrastructure.

POC load reductions associated with City SDC cleaning of the following types of stormwater infrastructure can be utilized to generate credits:

- a. Sediment and/or organic matter removed from catch basins, culverts, pipes, and concrete-lined channels by hand or use of equipment.
- b. Organic matter collected at the ends of stormwater outfalls within the stormwater system using nets or traps.

The collection and removal of materials from road segments with open channel ditches during ditch maintenance are not applicable for SDC crediting and must not be included in the annual calculations. Similarly, materials collected and removed from stormwater facilities as part of routine maintenance are not applicable for credit as part of the SDC as the pollutant reductions are included as part of the stormwater facilities' pollutant removal efficiencies.

5. POC loads must be characterized as either sediment or organic matter.

For City implementation of a SDC program and calculation of associated POC removal credits:

- a. Sediment is defined as material consisting primarily of solids that are collected and removed directly from catch basins, culverts, pipes, and concrete-lined channels.
- b. Organic matter is defined as material consisting primarily of organic materials (leaf litter, grass clippings collected and removed directly from catch basins, culverts, pipes, and concrete-lined channels or collected at the ends of stormwater outfalls within the stormwater system using nets or traps.

6. POC loads removed from stormwater infrastructure must be disposed of in a manner that prevents their migration back into the Chesapeake Bay watershed.

The City SOP for Storm Sewer System Cleaning and Maintenance requires:

- a. Liquid collected during cleaning activities be disposed of at the dewatering facility at the City's fleet maintenance facility so that it is not discharged back into the storm sewer system or water bodies.
- b. Solids collected during cleaning activities are properly disposed of in such a manner as to prevent reentry into the environment.

7. The aggregate load captured over the course of a year must be reported in terms of pounds of sediment and nutrients.

The use of the City of Fairfax SDC POC Credit Tracking Log (Attachment 2), developed in conjunction with the Tracking and Documenting SDC Activities and Quantifying Associated POC Reduction Credits, automatically tracks and documents applicable SDC activities and allows for annual summation of credits for reporting to DEQ as part of the MS4 Annual Report and DEQ BMP Warehouse spreadsheet.



3.0 Relative Merits Associated with the Use of SDC to meet Chesapeake Bay TMDL POC Reductions

3.1 Advantages

The utilization of SDC as a means to address required Chesapeake Bay TMDL POC reductions is advantageous to the City in the following respects:

1. SDC adds another tool to the City's compliance toolbox.

SDC provides the City a compliance tool that is different than traditional "in-the-ground" BMPs; thus, potentially relieving strain on existing capital improvement resources.

2. The City can obtain credits for services already provided.

The City already provides storm sewer system maintenance as a general service. This maintenance is a valuable community service concerning drainage and flooding prevention. Implementation of a standardized SOP associated with this maintenance provides the ability to gain additional credit for its efforts.

3. SDC can be implemented using existing City and/or contracted resources.

SDC is creditable based on its implementation process. As such, SDC can be implemented simply through modification of existing maintenance activities and integration of a comprehensive tracking and documentation process using the same City resources.

4. SDC credits are quantifiable.

GM # 20-2003 and the CBP Expert Panel Report provide direction on how to quantify and report SDC credits. As such, they are a recognized BMP for meeting the Chesapeake Bay TMDL reduction requirements.

3.2 Disadvantages

Although there are advantages associated with the utilization of SDC to meet Chesapeake Bay TMDL POC reduction requirements, there are also disadvantages. These disadvantages include the following:

1. SDC credits have a one-year life span.

Unlike traditional "in-the-ground" BMPs such as constructed wetlands, infiltration trenches, or wet ponds, SDC credits must be calculated and reported annually based upon the efforts completed during the reporting period.

2. SDC credits are based on the quantity of material collected, not the level of effort employed.

SDC credits are based upon the quantity of material collected during each annual reporting period and not upon percent effectiveness associated with the level of effort employed. As such, the number of SDC credits available to the City will likely vary from year to year and cannot be accurately anticipated for future planning.

3. Field crew efficiency may decrease.

Implementation of a creditable SDC is dependent upon significant tracking and documentation of the quantity of POC removed from qualifying stormwater infrastructure. The additional documentation effort may extend the amount of time required to complete individual cleaning events. Additionally, additional time and effort may be required to ensure that POC loads removed from non-qualifying stormwater infrastructure, such as sediment removal from grass-lined channels, are not inadvertently included in SDC verification efforts. This may require schedule modification and additional trips to dispose of SDC POC loads.



4. Regulatory requirements and expectations associated with SDC credit calculations are unclear and incomplete.

GM #20-2003 provides a mechanism to quantify nutrients through the use of both conversion and enrichment factors. However, the guidance does not provide a mechanism for quantifying sediments credits for application against Chesapeake Bay TMDL sediment reduction requirements. The CBP Expert Panel Report refers to large-, medium- and fine-grained particle sizes that are different than the TSS particle size of less than 250 microns generally associated with the Chesapeake Bay TMDL (Figure 1).

As it stands, GM #20-2003 requires the City to report the aggregate load captured over the course of a year expressed in pounds of sediment and that the loads be tracked and verified using field protocol to measure the mass or volume of solids collected within the storm drain while demonstrating the implementation of an SOP to keep track of the mass of the sediments and/or organic matter that is removed.

It is recommended that the City routinely, preferably quarterly, sample both the solids collected as part of

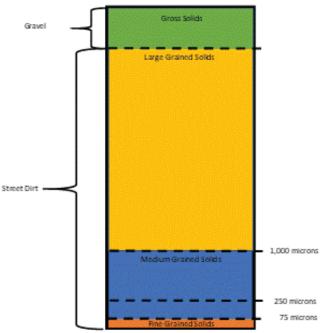


Figure 1: Differences Between CBO Expert Panel Particle Sizes and Corresponding Chesapeake Bay Sediment Particle Size of Concern (250 microns).

the SDC program and the liquid decant collected as part of SDC implementation using a vacuum truck. Samples should be analyzed to determine the percentage of organic matter and sediment particle size.

5. Verification of actual POC load reductions may be difficult.

To be of legitimate value to the City, SDC must be implemented in a manner that is both effective and efficient. It is not logistically possible to weigh the POC removal from individual SDC activities. Additionally, materials collected as part of SDC include other non-related Chesapeake Bay TMDL-related materials, such as trash and gravel, and, based upon the equipment used, may be comprised of different size particles. For example, the composition of wet materials collected by hand may differ from that collected by vacuum trucks as fine-grain materials may be removed from the composite and disposed of as part of the vacuum truck decant.

It is for these reasons that the City SOP is based on the City of Baltimore Public Work's default values provided in the CBP Expert Panel Report. The Expert Panel Report found that the accumulation rate, particle size distribution, and that POC content follow a relatively consistent uniform pattern across the nation and that these relationships provide a strong empirical basis for modeling how solids are transported from the street to the storm drain.



4.0 Use of the City of Fairfax SOP for Tracking and Documenting SDC Activities and Quantifying Associated POC Credits

GM #20-2003 states that the POC loads must be tracked and verified using a field protocol to measure the mass or volume of solids collected within the storm drain system and that the City must have instituted an SOP to track the mass of the sediments and organic matter that is removed. The City of Fairfax SOP for Tracking and Documenting SDC Activities and Quantifying Associated POC Credits is designed to be used in conjunction with the City SOP for Storm Sewer System Cleaning and Maintenance (Attachment 1) and the City of Fairfax SDC POC Credit Tracking Log (Attachment 2) to meet these requirements. SDC implemented as directed by the SOP ensure the following:

- 1. City priorities are targeted towards catch basins that trap the greatest organic matter loads, streets with the greatest overhead tree canopy, and/or outfalls with high sediment or debris loads.
- 2. Only applicable stormwater infrastructure cleaning is credited.
- 3. Loads collected as part of SDC implementation are tracked and verified using a field measure:
 - a. For sediment matter material loads, the SOP calls for tracking and verification by volume.
 - b. For organic matter loads, the SOP calls for tracking and verification by weight.
- 4. The mass of sediment and organic matter is tracked by the use of an SOP that relies upon default values. The default values incorporated into the City of Fairfax SDC POC Credit Tracking Log (Attachment 2) calculations are:
 - a. The bulk density of sediment-laden wet materials is 331 lbs./cubic yard.
 - b. Wet materials are comprised of 8.9% trash.
 - c. Sediment matter and organic matter comprise 301.54 lbs. per cubic yard of sediment-laden wet materials. This corresponds to credits totaling the following:
 - i. 3.78 lbs. N/ton of collected wet material, not including trash.
 - ii. 0.84 lbs. P/ton of collected wet material, not including trash.
 - iii. 420 lbs. TSS/ton of collected wet material, not including trash.
 - d. Nutrient credits associated with organic material collection incorporated as part of SDC are as follows:
 - i. 4.44 lbs. N/ton of collected wet material.
 - ii. 0.48 lbs. P/ton of collected wet material.
 - iii. TSS is not credited as part of organic material collection.
- 5. The material collected and measured for credit is disposed of so that it cannot migrate back into the Chesapeake Bay watershed.
- 6. The use of the City of Fairfax SDC POC Credit Tracking Log requires verification of the date, location, and estimated volume of material collected for individual SDC activities as well as an acknowledgment that the appropriate SOPs have been adhered to.



Attachment 1. Pollution Prevention/Good Housekeeping Standard Operating Procedure for Tracking and Documenting Storm Drain Cleaning (SDC) Activities and Quantifying Associated POC Credits



CITY OF FAIRFAX

POLLUTION PREVENTION/GOOD HOUSEKEEPING STANDARD OPERATING PROCEDURE (SOP) FOR

TRACKING AND DOCUMENTING STORM DRAIN CLEANING (SDC) ACTIVITIES

AND QUANTIFYING ASSOCIATED POC CREDITS

OBJECTIVE

POC reductions associated with specific City SDC activities can be used as a compliance method for meeting its MS4 Chesapeake Bay TMDL requirements. This SOP is intended to be used in conjunction with the City's Storm Sewer System Cleaning and Maintenance SOP to identify the applicable SDC activities and quantify, document, and verify the associated load reductions.

RESPONSIBILITIES

City employees conducting SDC activities are responsible for executing the activities in this operating procedure.

PROCEDURE

SDC Activities Applicable for Chesapeake Bay TMDL POC Reduction Compliance Credits

POC reductions from SDC activities are applicable for use in calculating Chesapeake Bay TMDL credits provided:

- SDC occurs within the City's MS4 service area without a formal agreement with adjoining MS4 operator allowing for the City to take credit for the POC removal.
- SDC occurs in an area prioritized by the City as having either a high sediment/debris load or a significant tree canopy. For the implementation of this SOP, prioritized areas are hereby identified as any area located within the MS4 service area in which the City conducts storm sewer maintenance as a result of historical knowledge or citizen complaints regarding drainage, flooding, or water quality issues caused by sediment, debris, or leaf litter.
- The SDC primarily collects either solid materials or organic materials.
 - For the purposes of SDC to collect solid materials, cleaning of the following stormwater infrastructure is applicable for quantification under this SOP:
 - Catch basins and associated sumps.
 - » Pipes and culverts.
 - » Concrete-lined conveyance channels.
 - » Outfall aprons.
 - For the purposes of SDC to collect organic materials, the following are applicable for quantification under this SOP:
 - » Netting or traps utilized to trap organic materials within stormwater infrastructure system or at the MS4 outfall.
 - Hand or equipment removal of accumulated leaf litter from catch basins, pipes and culverts, and concrete drainage conveyances provided the materials are disposed of in such a manner as to prevent entry back into the watershed (e.g., recycled into compost).
- POC reductions associated with the following are not eligible for credit consideration under this SOP:

Version 1 - August 4, 2021 Page 1-1



- Cleaning activities that occur outside of the City's MS4 service area without a formal agreement allowing for the City to take credit for the POC removal.
- Cleaning of street gutters by hand or street sweepers.
- Cleaning of, including sediment removal, grass-lined channels, and swales.
- Routine or required maintenance activities of stormwater management facilities in which the City has identified
 as part of its Chesapeake Bay TMDL compliance initiative.

Materials collected as part of SDC are disposed of in accordance with the Storm Sewer System Cleaning and Maintenance SOP to prevent mitigation back into the Chesapeake Bay watershed.

Tracking and Documenting SDC Field Efforts for Credit Generation

Accurate and complete documentation is imperative to generate and verify POC load reduction credits. The following data must be collected and maintained for each individual SDC activity:

- The cleaning date
- The type of stormwater infrastructure cleaned
- The primary POC type collected:
 - Solid materials
 - Organic materials
- When cleaning solid materials from storm drains where the estimated volume of the material is removed.²

Note: Volume is dependent upon the geometry of the infrastructure being cleaned and the estimate should be based on the overall length, width, and depth of the debris field. Large debris, such as tree branches and trash, should not be included in the estimated volume. The estimated volumes must be as accurate as possible as they will be the basis for Chesapeake Bay TMDL credit calculations.

When cleaning storm drains where the primary reasoning is for the collection of organic materials, the weight of the material collected.³

Note: TSS credits are not calculated for crediting as a result of collecting organic materials as part of this SOP.

 Certification that the Storm Sewer System Cleaning and Maintenance and SOP for Tracking and Documenting SDC Activities and Quantifying Associated POC Credits SOPs were followed.

Tracking and Documenting SDC Material Disposal

All materials collected under this SOP must be disposed of per the Storm Sewer System Cleaning and Maintenance SOP. The following data must be recorded, documented, and tracked for report verification:

- The total tonnage of solid debris disposed.
- Do not include large debris or tree branches when weighing the tonnage disposed.

Version 1 - August 4, 2021 Page 1-2

² The volume is estimated as a matter of efficiency. There is not an efficient way to weigh solid materials in the field.

³ Organic materials collected using netting or traps or collected by hand or equipment from applicable stormwater infrastructure should not be mixed with other materials but should be weighed independently prior to disposal.



- Debris for collection and disposal as part of the City's credited SDC protocol should be weighed independent of debris
 collected from non-qualifying City activities.
- Organic matter collected through the use of netting or traps should be weighed independent of all other forms of debris.
- Landfill and transfer station tipping receipts must be retained for verification with the distinction made between sediment-based and organic material-based collections. Receipts documenting disposal of organic material must remain separate from solid-based disposal receipts and should be identified as organic materials.

If a vacuum truck is utilized in the cleaning process, an estimated volume of the liquid vacuum truck decant disposed of via sanitary sewer should be recorded.

Calculating Chesapeake Bay TMDL POC Reduction Annual Credits

The collected field data from qualifying SDC activities must be entered into the City of Fairfax SDC POC Credit Tracking Log. The City of Fairfax SDC POC Credit Tracking Log will automatically calculate individual N, P, and TSS load reduction credits for individual activities. The total annual Chesapeake Bay TMDL POC reduction credits are aggregate for all activities completed between the first day of the MS4 permit reporting period and the last day of the annual MS4 permit reporting period (currently July 1 – June 30). Annual summations of the City's efforts and Chesapeake Bay TMDL POC load reduction credits should be reported to DEQ.

Verifying SDC Annual Credits

To verify the annual local reduction credits, field data for individual cleaning activities must be collected and entered into the City of Fairfax SDC POC Credit Tracking Log. Credits shall be generated using only the City of Fairfax SDC POC Credit Tracking Log entries in which all required data is entered (date, location, structure type, estimated volume collected). Associated work orders, landfill, and transfer station tipping fees must be maintained and made available during regulatory agency auditing.

Reporting of SDC Annual Credits

The credits and associated calculations should be included in the MS4 Annual Report:

- Wet load collected, lbs. during SDC
 - Solid material
 - Organic material
- Dry load calculated, lbs.
 - Solid material
 - Organic material
- TSS credits calculated, lbs.
- Total nitrogen credits calculated, lbs.
- Total phosphorus credits calculated, lbs.

Additionally, the City should report the TSS, TN, and TP credits to DEQ using the most recent Urban-Suburban BMP Template provided by DEQ.

Version 1 - August 4, 2021 Page 1-3



Attachment 2. City of Fairfax SDC POC Credit Tracking Log (Electronic)

City of Fairfax SDC Pollutant Credit Tracking Log Solid Material

Date Cleaned -		dentification (STRUC Address/Structure T		SOP for Disposal Followed	SOP for Tracking Followed	Estimated Volume of Wet	Calculated Wet	Calculated Sediment	Calculated Dry	Calculated Nitrogen Credits,	Calculated Phosphorus
	Structurel	Parcel Address	Structure Type	(Yes/No)	(Yes/No)	Material Collected, cf	Sediment, lbs.	Credit, lbs.	Sediment, lbs.	Lbs.	Credits, lbs.
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00 0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00 0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
<u> </u>							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00 0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
							0.00	0.00	0.00	0.0000	0.0000
1	<u>-</u>				<u></u>						
							0.00 0.00	0.00	0.00 0.00	0.0000 0.0000	0.0000 0.0000



Appendix V. Chesapeake Bay POC Reduction and Crediting Associated with Leaf Litter Collection and Disposal Discussion

City of Fairfax Department of Public Works Stormwater Management

CHESAPEAKE BAY POC REDUCTION AND CREDITING ASSOCIATED WITH LEAF LITTER COLLECTION AND DISPOSAL DISCUSSION

Version 1 – Effective Date August 31, 2021 (DRAFT)

Prepared for:



City of Fairfax, Virginia
Public Works - Stormwater
10455 Armstrong Street
Room 200
Fairfax, VA 22030

Updated by:



4229 Lafayette Center Drive, Suite 1850 Chantilly, Virginia 20151 703-870-7000



Acronyms

C Carbon

CBP U.S. EPA Chesapeake Bay Program

DEQ Virginia Department of Environmental Quality

GM Guidance Memo
Mg/L Milligrams/Liter

MS4 Municipal Separate Storm Sewer System

N Nitrogen

P Phosphorus

POC Pollutants of Concern (Nitrogen, Phosphorus, Total Suspended Sediment)

TN Total Nitrogen

TP Total Phosphorus

SOP Standard Operating Procedure

TMDL Total Maximum Daily Load

TSS Total Suspended Solids

VPDES Virginia Pollutant Discharge Elimination System



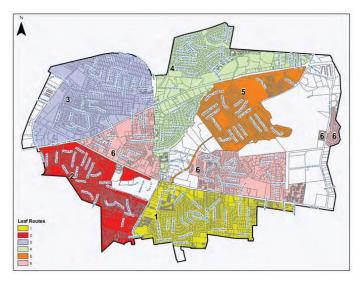
1.0 Background and Purpose

Discharges from the City of Fairfax's Municipal Separate Storm Sewer System (MS4) are authorized under the Virginia Pollutant Discharge Elimination System (VPDES) General Permit for Discharges of Stormwater from Small MS4s (MS4 General Permit). The MS4 General Permit includes conditions specific to MS4 discharges as well as standardized conditions applicable to all VPDES permits The MS4 General Permit also includes special conditions applicable to discharges identified in by a Total Maximum Daily Load (TMDL) study as contributing to a water quality impairment, including City MS4 discharges to the Chesapeake Bay. It is the City's regulatory responsibility to comply with the MS4 General Permit Chesapeake Bay TMDL Special Condition including the reduction of Pollutants of Concern (POC) from Existing Sources.

In determining the overall progress in addressing the Bay impairments, City implementation is documented in MS4 Annual Reports and provided to the Virginia Department of Environmental Quality (DEQ) for inclusion in the federal Environmental Protection Agency's (EPA) bay-wide watershed computer modeling efforts. While EPA's modeling efforts play a significant role in evaluating the overall watershed progress, it lacks the precision assess water quality impacts from relatively de minimus POC loads and associated POC load reductions such as those associated with the City's compliance efforts. As such, the City's compliance with meeting the required POC reductions is determined using calculation tables included in the MS4 General Permit Chesapeake Bay TMDL Special Condition. The MS4 General Permit Chesapeake Bay Special Condition dictates the acceptable POC reduction strategies and includes the use of those strategies approved by DEQ. DEQ Guidance Memo GM2-2003 provides further direction for the submission of strategies not previously DEQ-approved for the regulatory agencies review and approval. It is the City's responsibility to develop acceptable strategies that include means and methods for implementation of verifiable practices and accurately quantify the associated POC load reductions. The document lays out the rationale and potential direction for the City regarding receiving POC load reductions credits associated with its leaf litter collection and disposal programs for submission to DEQ for their consideration.

2.0 City Loose Leaf Collection and Disposal Program

The City operates a seasonal leaf collection and disposal program during the fall and spring months in which City crews collect loose leaves that are raked to the edge of the roadway from properties within the City. The loose leaves are collected on an approximate two-week rotational basis from six leaf collection routes (Figure 1). The collected loose leaves are then delivered to Loudoun Composting (44150 Wade Dr, Chantilly, VA 20152) where they are composted and converted into a marketable product for use in the Mid-Atlantic region, including the Chesapeake Bay Watershed. The Loudoun Composting operation, including leachate management, is regulated under a DEQ Solid Waste Permit By Rule (PBR141). In FY2021, the City transported 1,056 tons of loose leaf litter to Loudoun Composting.





3.0 Rationale for Consideration of Nutrient Reduction Credits from the City's Leaf Litter Collection and Disposal Program

The City's Leaf Collection and Disposal program is an exit ramp for nutrients entering the Chesapeake Bay. The difficulty is determining just how much actual nutrient reduction credit is attained and how it can be credited towards the City meeting its MS4 POC reduction requirements. The Chesapeake Bay Program Management Board Expert Panel included in its 2016 publication, 'Recommendations of the Expert Panel to Define Removal Rates for Street and Storm Drain Cleaning Practices,' that studies in the City of Baltimore, MD found that the average nutrient load associated with leaf drop was estimated to be 28.8 lbs./ac/yr. for nitrogen and 2.95 lbs./ac/yr. for phosphorus. The potential for leaf litter to represent a significant nutrient source, and in turn, a potentially significant source control available to the City, was further reenforced by a 2020 U.S. Geological Survey (USGS) Scientific Investigations Report titled 'Reducing Leaf Litter Contributions of Phosphorus and Nitrogen to Urban Stormwater through Municipal Leaf Collection and Street Cleaning Practices.' The USGS report found that

- "At its peak, fall leaf litter can rapidly accumulate on a street surface over a short period of time. Because the
 amount of leachable phosphorus in runoff is a function of the amount of time a leaf is exposed to stormwater,
 the timing of leaf collection and street cleaning is an important factor when maximizing phosphorus and
 nitrogen load reduction."
- [Municipal] "collection of leaf piles remains an important part of managing phosphorus and nitrogen loads, because most homeowners have come to rely on that service to dispose of excess yard waste."
- "The link between concentrations of phosphorus and nitrogen measured in storm drains and street tree canopy support stormwater management practices that are designed to limit accumulation of leaf litter on streets or encourage their removal before a storm event."
- "The majority of nutrient concentrations were in the dissolved fraction making source control through leaf collection and street cleaning more effective at reducing the amount of dissolved nutrients in stormwater runoff."

A City-specific example of the potential POC concentrations associated with leaf litter collection and disposal can be drawn from the CFP discussions regarding bulk collection of organic matter as part of storm drain cleaning. If, during FY2021, the City were to collect the 1,056 tons of leaves from within the storm drainage system rather than before they enter it, the City could potentially gain significant POC reduction credits based on the potential nutrients (Table 1).

Table 1. POC Nutrient Credit Example Using City FY2021 Leaf Collections and Calculations for Determining Credits if Leaf Litter Had Been Removed from the MS4.

Bulk Leaves Collected and Disposed, lbs. (tons)	Wet Load to Dry Load Conversion Factor	Nutrient	Nutrient Enrichment Factor (Organic Matter / Leaf Litter	Nutrient Credit, lbs.		
2,112,000 (1,056)	0.2	Nitrogen	itrogen 0.12%			
	0.2	Phosphorus	1.11%	6,243		

There are numerous factors that make the values calculated in Table 1 inappropriate to apply to towards the City's leaf collection and disposal program. These include:

¹ Selbig, W.R., Buer, N.H., Bannerman, R.T., and Gaebler, P., 2020, Reducing Leaf Litter Contributions of Phosphorus and Nitrogen to Urban Stormwater Through Municipal Leaf Collection and Street Cleaning Practices: U.S. Geological Survey Scientific Investigations Report 5109, 17 p.



1. There is a re-introduction of an unknown percentage of nutrients into the delivery pathway leading to the Chesapeake Bay.

Collected leaf litter, such as the City's, is often composted and returned to the community in the form of mulch. The reuse of the leaf litter as mulch represents a pathway for some nutrients to re-enter the Chesapeake Bay watershed and, ultimately, reach the Bay. While limited research has shown that nutrients tend to leach from composting leaves rather quickly, the leaching rate depends on numerous physical factors such as amount of time the leaves are submersed in water. Any procedure designed to quantify the reduction of nutrients as a result of leaf litter collection must account for this reintroduction process.

- 2. The nutrients in leachate collected during composting that are properly disposed (prevented from re-entering the Chesapeake Bay watershed) represent a POC reduction as it pertains to MS4 POC reductions.
 - Nutrients leach out of composting leaf litter when it comes into contact with precipitation. If this leachate is collected and prevented from discharge into the environment, there is a reduction in the quantity of nutrients being discharged to the Chesapeake Bay; however, difficulty lies with how to quantify the applicable nutrient load. Quantification of the applicable nutrient load for consideration must consider the following:
 - a. The nutrient concentration in the leachate will vary throughout the season based on the chemical and physical factors associated with composting.
 - b. Leaves are collected from mixed land uses consisting of both pervious and impervious surfaces. A percentage of the nutrients would infiltrate into the pervious lands and would not be discharged. Although it is technically removed from the environment, the fraction is an artificial 'load' enhancement that would not be released unless the City directed leaf litter to be raked to the edge of the property and collected. As such, it's removal should not count towards the City's overall POC reduction.
- 3. The Nutrient Enrichment Factor included in the CFP publication, "Recommendations of the Expert Panel to Define Removal Rates for Street and Storm Drain Cleaning Practices" is not appropriate for use in calculating the nutrient loads.
 - The Nutrient Enrichment Factor assumes that the nutrients are permanently prevented from re-entry into the Chesapeake Bay watershed. The reintroduction of mulch prevents this assumption from being fulfilled.
- 4.0 Recommendations for Proposing City Leaf Litter Collection as a Chesapeake Bay TMDL POC Reduction Credit

As discussed in this document's background and purpose, DEQ has the authority to approve other POC reduction methods outside of those included in GM20-2003; however, it is the City's responsibility to develop a verifiable process in which to quantify the POC reductions from a proposed alternative POC reduction method. The following actions are recommended if the City wishes to pursue the potential opportunity to utilize leaf litter collection as a means to meet Chesapeake Bay TMDL POC reduction requirements:

- Confirm that Loudoun Compost prevents its leachate from re-entry into the Chesapeake Bay watershed.
 There is no applicable credit opportunity if the nutrients in the leachate are permitted to re-enter the Chesapeake Bay watershed.
- 2. Obtain DEQ's acknowledgement, preferably in writing, that they will consider leaf litter collection as an alternative means of reducing POC loads.
 - If DEQ refuses to consider POC reductions associated with leaf litter collection, there is no sensible reason to pursue it any further.
- Develop a runoff coefficient for the portions of the City in which leaves are collected.
 - The development of a runoff coefficient will allow the City to adjust the volume of runoff to what would be expected from the portions of the City where leaf litter is collected. This will enable the City to account for areas of forest in which leaves would not be collected and for nutrients in stormwater runoff that would normally infiltrate into the ground and be discharged.



4. Implement a pilot monitoring program to determine the seasonal nutrient concentration and overall load associated with the leachate.

The City should implement a monitoring program that runs concurrent with its leaf litter collection program and extends through the warmer spring months. The pilot monitoring program would consist of setting a known quantity of leaves on an impervious surface with exposure to the environment. The quantity of leachate should be measured throughout the pilot program and flow-based monitoring of nitrogen and phosphorus concentrations in the leachate should be monitored.

5. Calculate the proposed POC reduction credits

Use the annual average nutrient concentration and the quantity of leachate to determine the POC load captured as part of the pilot project. Apply the results to the total amount of leaf litter collected and adjust downward using the collection area runoff coefficient. The results of this calculation project would represent the potential POC reduction credit for the City to submit to DEQ for review and approval.



Appendix W. Summary of Public Comments Received During the Public Comment Period and City Responses